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## CONTRACT REPORT ARBRL-CR-00382

# A LITERATURE REVIEW OF MILLIMETER AND SUBMILLIMETER RADIATION ABSORPTION AND SCATTERING IN THE ATMOSPHERE

Prepared by

Radiation Research Associates, Inc. 3550 Hulen Street Fort Worth, Texas 76107

October 1978



## US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND BALLISTIC RESEARCH LABORATORY ABERDEEN PROVING GROUND, MARYLAND

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Ozone Absorption Rain Index of Refraction for Water
Oxygen Absorption Snow Index of Refraction for Dusts
Aerosols Mm and Submm radiation Atmospheric Index of Refraction
Battlefield Dusts

#### 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The presence on the electronic battlefield of smoke, dust, aerosols and exotic gases may seriously interfere with the effectiveness of battlefield radars in the millimeter and submillimeter wavelength range that have to operate in such an environment. This report describes a literature review that was performed on the absorption and scattering processes undergone by 100  $\mu m$  to 1 cm wavelength radiation as it propagates through the atmosphere. Recommendations are given for further experimental and theoretical work that is needed to better define

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| the absorption by atmospheric and battlefield generated gases and the scattering and absorption by atmospheric and battlefield generated aerosols and smokes. The Appendix contains a bibliography of the unclassified unlimited and limited distribution documents included in the literature review. The bibliography of the classified documents included in the literature review is |                             |         |      |   |  |  |
| given in Volume                                                                                                                                                                                                                                                                                                                                                                          | II of this report.          |         |      |   |  |  |
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#### I. INTRODUCTION

The presence of smoke, dust, aerosol and exotic gases on the battlefield may impair the effectiveness of battlefield radar in such an environment. The object of the work described in this report was to review the unclassified and classified literature on the absorption and scattering processes undergone by  $100~\mu m$  to 1 cm wavelength radiation as it propagates through the atmosphere. The literature reviewed includes those papers that describe calculations and measurements of  $100~\mu m$  to 1 cm wavelength radiation and absorption by normal atmospheric gases and by water vapor, rain, ozone, atmospheric aerosols, clouds, fogs, battlefield dust and smoke and the exotic gases produced by motorized equipment and weapons during battle.

The government report literature surveyed during this study is listed in Appendix A of this report. An NTIS literature survey was obtained for use in this study. The NTIS survey was entitled "Submillimeter Wavelength Radiation Absorption and Scattering by Atmospheric Gases, Water Vapor, Ozone, Aerosols, Clouds, Fog, Battlefield Dust and Smoke." A total of 51 reports listed in the NTIS survey was ordered for use in this study. A number of the reports listed in the NTIS survey were already available in the RRA document files. A total of 190 unclassified, 34 limited, and 14 classified government sponsored research, reports were reviewed for this study. In addition, a number of books were reviewed and articles on millimeter radiation interactions in the atmosphere from the following journals were reviewed:

IEEE Transactions on Microwave Theory and Techniques, 1970-1977 IEEE Transactions on Antenna and Propagation, 1970-1977 Journal of the Optical Society of America, 1970-1977 Applied Optics Infrared Physics, 1963-1977 Journal of Geophysical Research, 1963-1977

Journal of the Atmospheric Sciences, 1974-1976
Optics and Spectroscopy, (Russian Translation) 1970-1977
Radio Physics and Electronics (Russian Translation), 1969-1977
Nature and Nature/Physical Sciences, 1970-1977
Journal of the Faraday Society, 1970-1977 (and selected 1960's)
Optical Engineering, 1973-1978
Physical Review (selected articles), 1965-1975
Review of Modern Physics (selected articles), 1973-1978
Journal of Molecular Spectroscopy, 1967-1977

Section II gives a summary of the unclassified documents in the open literature on: 1) attenuation by atmospheric water vapor and oxygen, 2) atmospheric index of refraction, 3) attenuation and scattering by fog. rain and clouds, 4) attenuation and scattering by snow, 5) attenuation by Ozone, 6) attenuation and scattering by aerosols and dust and 7) attenuation and scattering by battlefield generated dusts and smokes. Section III gives a summary of the limited distribution, unclassified literature on attenuation and scattering by rain and hail, attenuation by water vapor and the refractive indices for sea spray. Section IV discusses the results of the review of the classified literature.

A bibliography of the unclassified literature is given in Appendix A. Section V describes the methods used to index the contents of the articles reviewed. Recommendations for further work that is needed to further the understanding of the interaction processes undergone by mm and sub mm radiation as it propagates in the atmosphere are given in Section VI.

#### II. SUMMARY OF LITERATURE SURVEYED

The following sections present data taken from the reviewed literature which describe the current state of knowledge on the interaction cross sections for millimeter and submillimeter radiation when it is propagated through the atmosphere.

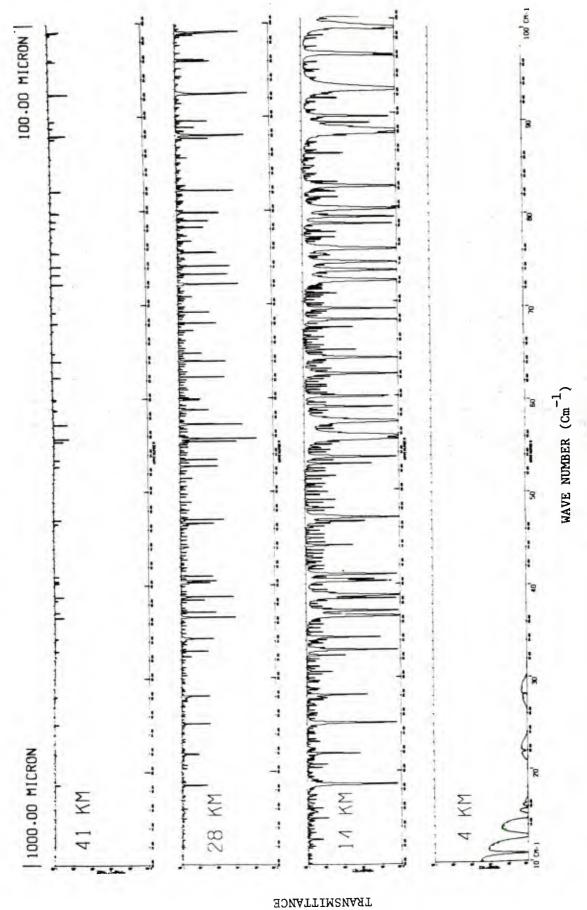
## 2.1 Attenuation by Water Vapor and Oxygen

Corcoran has presented a table (shown here as Table I) of the atmosphere "Windows" and bounding absorption peaks, from 3.2 cm to 156  $\mu m$  for absorption due to water vapor and oxygen for a zenith path through a cloudless Maritime Polar atmosphere. The absorption is given for water vapor, oxygen, and combined gaseous attenuation for these chief atmospheric constituants.

Traub and  $\operatorname{Stier}^2$  has presented an atmospheric calculation for mid and far IR at 4 observing altitudes, 4.2 km (Mauna Kea), 14 km (aircraft), 28 km (balloon), and 41 km (balloon). Molecular abundances, effective pressures and temperatures used in the Curtis-Godson approximation as shown here in Table II (from Traub and Steier, Ref. 2). They used the AFCRL atmospheric absorption line parameter tape  $^3$  to obtain the wavenumber, line strength, pressure broadening coefficient, and energy level of the lower state for over 109,000 known transitions of  $H_2^0$ ,  $O_3$ ,  $\rm O_2$  , CO,  $\rm N_2O$  , and CH  $_4$  between .76  $\rm \mu m$  and 3.26 mm. Figure 1 presents the results of their calculations of atmospheric transmission from 100  $\mu\text{m}$ to 1000  $\mu\text{m}$  using the initial conditions shown in Table II. The "4 km" labeled curve is really for the 4.2 km altitude of Mauna Kea. The vertical ordinate, the transmission, unreadable in the curves of Fig. 1 is linear from 0 to 1. A Lorentz line profile was used for simplicity, though a Van Vleck-Weiskopf line profile would have been more accurate in the wings of each line.

Table I. Candidate "Windows" in the Submillimeter and Microwave Bands, Arising from Absorption Spectra of Water Vapor and Oxygen, with Attenuation in Decibels Calculated for a Zenith Path through a Cloudless Maritime Polar Atmosphere (from Ref. 1)

|        | -                                                          | Bounding Absor                           | ption Peaks              | Attenuation    | (in decibels) | along zenith path              |
|--------|------------------------------------------------------------|------------------------------------------|--------------------------|----------------|---------------|--------------------------------|
| Window | Wavelength (approx.) of window at least gaseous absorption | Wavelength.of<br>peak absorption         | Primary<br>absorbing gas | By water vapor | By oxygen     | Combined<br>gaseous absorption |
|        |                                                            | No absorption of o<br>wavelengths greate |                          | ,              | f             |                                |
| I      | 3.2cm                                                      |                                          |                          | 0.005          | 0.140         | 0.145                          |
|        |                                                            | 1.3cm                                    | Water vapor              | 0.408          | 0.200         | 0.608                          |
| 11     | 9mm                                                        | -                                        |                          | 0.074          | 0.340         | . 0.414                        |
|        |                                                            | 5mm                                      | Oxygen                   | 0.100          | 135.          | 135.1                          |
| 111    | 3mm                                                        |                                          |                          | 0.253          | 1.00          | 4. 1.253                       |
|        | *                                                          | 2.52mm                                   | Oxygen                   | 0.447          | 30.0          | 30.447                         |
| IV     | 2.3mm                                                      |                                          | . 5                      | , = 0.506      | . 0.40°       | 57 - 20.906                    |
|        |                                                            | 1.6mm                                    | Water vapor              | 65.8           | 0.18          | 65.98                          |
| V      | 1.3mm -                                                    |                                          |                          | 1.80           | 0.31          | 2.11                           |
|        |                                                            | 920µ                                     | Water vapor              | 90.9           | 0.68          | ,91.5B                         |
| VI     | 880u                                                       |                                          | 1.4                      | 9,12           | 0.75          | 9.87                           |
|        | *                                                          | 780u                                     | Water vapor              | 621.           | 0,-95         | 621.95                         |
| VII    | 720u                                                       | ·                                        | ,                        | 20.9           | 1.10          | 22.00                          |
|        |                                                            | 660 <sub>µ</sub>                         | Water vapor              | ₹ 874.         | 1.30 👬        | 875.30                         |
| VIII   | 650u                                                       |                                          |                          | 64.8           | 1.40          | 66.20                          |
|        |                                                            | 630ш                                     | Water vapor              | 184.           | 1.50          | 185.50                         |
| IX     | 620u                                                       | *                                        |                          | 55.5           | 1.55          | 57.05                          |
|        |                                                            | 5 30u                                    | Water vapor              | 37,100.        | 2.10          | 37,102.                        |
| X      | 490µ                                                       |                                          |                          | 189.           | 2.40          | 191,40                         |
|        |                                                            | 475µ                                     | Water <sup>3</sup> vapor | enn.           | 2.60          | 692.60                         |
| XI     | ∂50µ                                                       |                                          | ,                        | 12.0           | 2.90          | 74.90                          |
|        |                                                            | 397u                                     | Water vapor              | 27,000.        | 3.80          | 27,003.8                       |
| XII    | 345µ                                                       |                                          |                          | -72.0          | - 5.0         | 3 70 77,0                      |
|        |                                                            | 325u                                     | Water vapor              | 1,450.         | 5.6           | 1,455.6                        |
| XIII   | 320u                                                       | · · · · · · · · · · · · · · · · · · ·    | =3                       | 189.           | 5.8           | 194.8                          |
|        |                                                            | , 30 3u                                  | Water vapor              | 176,000.       | 6.5           | 176,006.5                      |
| XIV    | 290u                                                       |                                          |                          | 360.           | 7.            | 367.                           |
|        |                                                            | . 256u                                   | Water vapor              | 187,000.       | , 9، س        | 187,009.                       |
| χV     | 237µ                                                       |                                          |                          | 540.           | 11.           | 551.                           |
|        |                                                            | 215u                                     | · Water vapor            | 176;000        | 13.           | 176,013.                       |
| XVI    | 200u                                                       |                                          |                          | 486.           | 15.           | 501.                           |
|        |                                                            | 174u                                     | Water vapor              | 6,900.         | (20.)         | 6,920.                         |
| XVII   | - 164u                                                     |                                          | . 1                      | 1,230.         | (22.)         | 1,252.                         |
|        |                                                            | 156u                                     | Water vapor              | 6,900.         | (25.)         | 6,925.                         |



Atmospheric Transmission at Four Altitudes with an Air Mass of 2.0 and a Rectangular Bandpass of 0.05 cm<sup>-1</sup> width. (From Data in Ref. 2) Fig. 1.

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Table II. Molecular Abundances, Effective Pressures, and Temperatures Used in the Curtis-Godson Approximation<sup>a</sup>, b

|           | 4.2 km<br>(Mauna Kea)     | 14 km<br>(Aircraft) | 28 km<br>(Balloon) | 41 km<br>(Balloon) |
|-----------|---------------------------|---------------------|--------------------|--------------------|
| 0,        | 209460.0 ppmv             | 209460.0            | 209460.0           | 209460.0           |
| CO,       | 325.0 ppmv                | <b>325</b> 0        | 325.0              | 325.0              |
| CH,       | 1.5 ppm <b>v</b>          | 1.1                 | 0.8                | 0.4                |
| N₁Õ<br>CO | 0.25 p <b>pm</b> v        | 0.20                | 0.20               | 0.20               |
| CO        | 0.07 ppmv                 | 0.06                | 0.06               | 0.06               |
| H,O       | 1200 μm                   | 2.5 ppmv            | 2.5 ppmv           | 2.5 ppm            |
| Ο,        | 7.28 E18 cm <sup>-2</sup> | 6.37 E18            | 1.85 E18           | 1.70 E17           |
| p         | 600.0 mbar                | 141.6               | 16.2               | 2,52               |
| p(eff)    | 300.0 mbar                | 70.8                | 8.10               | 1.26               |
| $p(H_2O)$ | 506.0 mbar                | 70.8                | 8.10               | 1.26               |
| $p(O_3)$  | 36.4 mbar                 | 30.2                | 7.09               | 1.84               |
| T(eff)    | 228.0 K                   | 217.0               | 230 0              | 268.0              |
| T(H,O)    | 252.0 K                   | 217.0               | 230.0              | 268.0              |
| $T(O_3)$  | 219.0 K                   | 221.0               | 233.0              | 260.0              |

<sup>a</sup>The H<sub>2</sub>O abundances in the last three columns correspond to 2.25, 0.26, and 0.040 precipitable  $\mu$ m, respectively; the H<sub>2</sub>O at 4.2 km is assumed to have a scale height of 1.85 km. The abundances listed are for unit air mass; an additional factor of 2 is included in the actual calculations corresponding to a zenith angle of 60°. The base pressure at each altitude is given by p, and the effective pressure for collisional line broadening is indicated by p(eff),  $p(H_2O)$ , and  $p(O_3)$  for the first five species, H<sub>2</sub>O, and O<sub>3</sub>, respectively; the temperatures at the corresponding pressure levels are also listed.

b<sub>Data from Ref. 2.</sub>

Archie Straiton  $^4$ , in a tutorial article, presents the results of a calculation of the attenuation in the 10-400 GHz wave bands (3.33 cm - .75 mm) due to oxygen and water vapor in a vertical path from sea level for a standard atmosphere. His results are shown in Fig. 2. We see graphically the major absorption lines and windows of the microwave-mm wave region; below 100 GHz, the absorption spectrum is dominated by the "22" GHz water vapor line, and the "60" GHz molecular oxygen line. Attention has been placed on communication systems operating in the 35 GHz and 93 GHz regions of transmission maximum for long range requirements, and in the 60 GHz region, for short range, secure communications. Some authors have utilized the water vapor lines (in emission) at 22 GHz and 183 GHz to measure the atmospheric water vapor content. In his calculation, Straiton used the Gross  $^5$ / Zhevakin-Naumov  $^6$  attenuations  $\Gamma(\nu)$  at a frequency  $\nu$  for a single line with center frequency  $\nu$ 

$$\Gamma(v) = \frac{S}{\pi} \frac{4\pi v_{\alpha}^{2}}{(v_{ij}^{2} - v_{\alpha}^{2})^{2} + 4v_{\alpha}^{2}^{2}}$$

- S = a measure of the strength of a line
- $\alpha$  = approximately the change in frequency from  $\nu_{ij}$  at which the attenuation has dropped to 1/2 (line breadth parameter =  $\simeq \Delta \nu$ )

Values of  $v_i$ , S, and  $\alpha$ , which are given by Burch for water vapor from 0.5 to 36 cm are presented here as Table III. The water vapor line breadth parameter is given by (after Straiton, Ref. 4)

$$\Delta v = 2.62 (1 + 0.01 \frac{\rho T}{p}) \frac{(P/760)}{(T/3.18)^{0.625}}$$

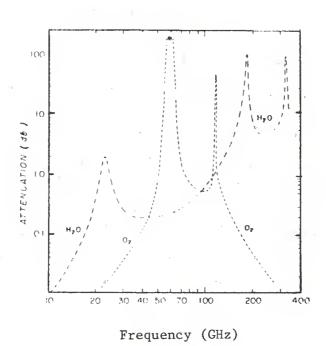


Fig. 2. Oxygen and Water Vapor Attenuation
Vertically from Sea Level (Data from Ref. 2)

Table III. Parameters for  $H_2^0$  lines below 38.8 cm<sup>-1</sup>. (Data from Ref. 7)

| Pa .              | J'      | τ'             |         | 20027                    | 200041              | Tempera           |                         | 2.400.5             | ****           |
|-------------------|---------|----------------|---------|--------------------------|---------------------|-------------------|-------------------------|---------------------|----------------|
| tm 1              | J''     | τ''            | Isotope | 320°K                    | 300°K               | 280°K             | 260°K                   | 240°K               | 220°K          |
| 0.74              | 6       | -5             |         | S = 1.35 - 2             | 1.39 - 2            | 1.42 - 2          | 1.43 - 2                | 1.42 - 2            | 1.38-          |
| 2.27              | 5<br>4  | $-1 \\ -3$     |         | $\alpha^{\circ} = 0.087$ | 0.090               | 0.094             | 0.090                   | 0.104               | 0.110          |
| 2.21              | 3       | -3             |         | 6.95—4<br>0.091          | 4.73 - 4 $0.095$    | 3.01 - 4 $0.099$  | 1.77 - 4 $0.10$         | 9.30 – 5<br>0.11    | 4.28-:<br>0.12 |
| 2.69              | ĭ       | î              | D       | 6.47 - 4                 | 7.53 - 4            | 8.85 - 4          | 1.05 - 3                | 1,26-3              | 1.54-          |
|                   | 1       | 0              |         | 0.098                    | 0.102               | 0.106             | 0.111                   | 0.117               | 0.123          |
| 4.03              | 5       | 4              | 1)      | 6.75 - 4                 | 7.42 - 4            | 8.16 - 4          | 8.98 - 4                | 9.89 - 4            | 1.09-          |
| 4.62              | 4<br>6  | -5             | D       | 0.089<br>5,154           | 0.093 $5.52 - 4$    | 0.097 $5.91 - 4$  | 0.10 $6.30-4$           | 0.11<br>0.67 - 4    | 0.11<br>7.01—  |
| 7.02              | 5       | - 3<br>- 1     | 1)      | 0.086                    | 0.090               | 0.094             | 0.098                   | 0.10                | 0.11           |
| 4.80              | 4       | Ô              | D       | 9.86 - 4                 | 1.09 - 3            | 1.20-3            | 1.32 - 3                | 1.45 - 3            | 1.60-          |
|                   | 4       | -1             |         | 0.088                    | 0.091               | 0.095             | 0.099                   | 0.10                | 0.11           |
| 6.11              | 3       | $-\frac{2}{3}$ |         | 2.26                     | 2.55                | 2.88              | 3.28                    | 3.76                | 4.32           |
| 5.79              | 2<br>3  | $-\frac{2}{2}$ | 18      | 0.092<br>5.75-3          | 0.096 $6.48 - 3$    | 0.100 $7.34 - 3$  | $0.105 \\ 8.36 - 3$     | 0.111 $9.58 - 3$    | 0.117<br>1.10- |
| 0.17              | 2       | 2              | 10      | 0.092                    | 0.096               | 0.10              | 0.11                    | 0.11                | 0.12           |
| 3.06              | 2       | ō              | D       | 2.79 - 3                 | 3.22 - 3            | 3.75 - 3          | 4.40 - 3                | 5.21 - 3            | 6.26-          |
|                   | 2       | -1             |         | 0.096                    | 0.10                | 0.10              | 0.11                    | 0.12                | 0.12           |
| 3.50              | 5       | 1              | D       | 3.05 - 3                 | 3.28 - 3            | 3.51 - 3          | 3.75 - 3                | 3.99-3              | 4.20-          |
| 3.90              | 4<br>2  | 1 2            | D       | $0.085 \\ 3.11 - 3$      | 0.089 - 3.54 - 3    | 0.093<br>4.06-3   | 0.098 $4.68 - 3$        | $0.10 \\ 5.44 - 3$  | 0.11<br>6.38 – |
| s. <del>9</del> 0 | 3       | -2             | 10      | 0.092                    | 0.096               | 0.10              | 0.11                    | 0.11                | 0.12           |
| ).74              | 10      | $-\frac{5}{7}$ |         | 9.57 - 2                 | 7.64 - 2            | 5.84 - 2          | $\frac{3.11}{4.22} - 2$ | 2.84 - 2            | 1.75-          |
| _                 | 9       | -3             |         | 0.074                    | 0.077               | 0.079             | 0.081                   | 0.084               | 0.087          |
| ).85              | 5       | -4             |         | 2.77                     | 2.95                | 3.14              | 3.33                    | 3.51                | 3.65           |
| .89               | 4<br>10 | 0<br>-7        | 18      | 0.089 $2.44-4$           | 0.093 $1.95 - 4$    | 0.097<br>1.49 – 4 | $0.102 \\ 1.08 - 4$     | 0.107<br>7.28-5     | 0.113<br>4.48- |
| .09               | 9       | $-\frac{7}{3}$ | 10      | 0.075                    | 0.077               | 0.079             | 0.082                   | 0.085               | 0.088          |
| .68               | 4       | -3             |         | 2.47 + 1                 | 2.72 + 1            | 2.99 + 1          | 3.30+1                  | 3.64 + 1            | 4.02+          |
|                   | 3       | 1              |         | 0.091                    | 0.095               | 0.099             | 0.104                   | 0.109               | 0.115          |
| 3.05              | 4       | -3             | 18      | 5.38 - 2                 | 5.93 - 2            | 6.54 - 2          | 7.21 - 2                | 7.96 - 2            | 8.78-          |
| .10               | 3<br>10 | 1<br>-4        |         | 0.091 $1.14-2$           | 0.095<br>8.43 – 3   | 0.099<br>5.92—3   | $0.10 \\ 3.89 - 3$      | 0.11 $2.34-3$       | 0.12<br>1.26-  |
| .10               | 11      | -8             |         | 0.069                    | 0.070               | 0.072             | 0.074                   | 0.076               | 0.078          |
| .58               | 7       | 2              |         | 1.77 - 1                 | 1.52 - 1            | 1.25 - 1          | 9.96 - 2                | 7.48 - 2            | 5.23-          |
|                   | 6       | 6              |         | 0.049                    | 0.050               | 0.051             | 0.052                   | 0.053               | 0.055          |
| .65               | 6       | 1              |         | 2.43                     | 2.28                | 2.10              | 1.88                    | 1.62                | 1.34           |
| .78               | 5<br>7  | 5<br>3         |         | 0.064<br>5.45 — 1        | 0.065<br>4.67 — 1   | 0.067 $3.87 - 1$  | 0.068 $3.07 - 1$        | 0.070<br>2.31—1     | 0.073<br>1.61— |
| .,,0              | 6       | 5              |         | 0.049                    | 0.050               | 0.051             | 0.053                   | 0.054               | 0.056          |
| .92               | 4       | -1             |         | 2.62 + 1                 | 2.82 + 1            | 3.03 + 1          | 3.25 + 1                | 3.46 + 1            | 3.66+          |
|                   | 3       | 3              |         | 0.080                    | 0.082               | 0.085             | 0.089                   | 0.092               | 0.097          |
| .68               | 6       | 2              |         | 9.29 1                   | 8.72 - 1            | 8.01-1            | 7.16 - 1                | 6.18-1              | 5.10-          |
| 5.87              | 5<br>5  | 4              |         | 0.061<br>3.51            | 0.063<br>3.55       | 0.065<br>3.56     | 0.066<br>3.52           | 0.069<br>3.42       | 0.071 $3.24$   |
| .07               | 4       | 4              |         | 0.067                    | 0.069               | 0.071             | 0.073                   | 0.075               | 0.078          |
| .29               | 6       | -2             |         | 7.05 - 1                 | 6.93 - 1            | 6.72 - 1          | 6.39 - 1                | 5.93 - 1            | 5.32-          |
|                   | 7       | -6             |         | 0.083                    | 0.086               | 0.090             | 0,093                   | 0.098               | 0.103          |
| 5.30              | 4       | - 1            | 18      | 6.49 - 2                 | 6.99 - 2            | 7.51 - 2          | 8.06-2                  | 8.60 - 2            | 9.12-          |
| .79               | 3<br>8  | 3              |         | 0.079 $1.27 - 1$         | $0.082 \\ 9.82 - 2$ | 0.085 $7.21-2$    | $0.088 \\ 4.98 - 2$     | 0.089 $3.18 - 2$    | 0.096<br>1.84- |
| 1.19              | 7       | 7              |         | 0.042                    | 0.042               | 0.043             | 0.044                   | 0.046               | 0.047          |
| .82               | 8       | 4              |         | 4.26 - 2                 | 3.28 - 2            | 2.41 - 2          | 1.67 - 2                | 1.06 - 2            | 6.15-          |
|                   | 8<br>7  | 6              |         | 0.042                    | 0.042               | 0.043             | 0.045                   | 0.046               | 0.047          |
| .96               | 1       | 1              | D       | 1.85 - 1                 | 2.16 - 1            | 2.54 - 1          | 3.03 - 1                | 3.66 - 1            | 4.48-          |
| 3.26              | 1<br>1  | -1<br>1        | 18      | 0.107<br>2.95            | 0.111<br>3.43       | 0.116<br>4.03     | $\frac{0.122}{4.78}$    | 0.128<br>5.75       | 0.135<br>7.01  |
| 1.20              | 1       | - i            | 10      | 0.107                    | 0.111               | 0.116             | 0.122                   | 0.128               | 0.135          |
| 3.58              | ĩ       | ī              |         | $1.49 \pm 3$             | 1.73 + 3            | 2.04 + 3          | 2.42 + 3                | 2.91 + 3            | 3.54+          |
|                   | 1       | -1             | **      | 0.107                    | 0.111               | 0.116             | 0.122                   | 0.128               | 0.136          |
| .99               | 2       | 0              | D       | 3.38-1                   | 3.90 - 1            | 4.55-1            | 5.35 - 1                | 6.36 - 1            | 7.66-          |
| 0.71              | 2<br>5  | - 2<br>1       |         | $0.100 \\ 1.82 + 1$      | 0.104               | 0.109             | 0.115                   | 0.121<br>1.76+1     | 0.129<br>1.67+ |
| ./1               | 4       | 3              |         | 0.073                    | 1.84 + 1 $0.076$    | 1.84 + 1 $0.079$  | 1.82+1<br>0.083         | 0.087               | 0.092          |
| .96               | i       | 1              |         | 1.59                     | 1.15                | 7.78 - 1          | 4.92 - 1                | 2.83 - 1            | 1.45-          |
|                   | 1       | 1              |         | 0.107                    | 0.111               | 0.116             | 0.122                   | 0.128               | 0.135          |
| 1.84              | 2       | 0              | 18      | 2.02                     | 2.31                | 2.67              | 3.11                    | 3.66                | 4.34           |
| 5.09              | 2<br>2  | $-\frac{2}{0}$ |         | $0.100 \\ 1.00 + 3$      | $0.104 \\ 1.15 + 3$ | 0.109 $1.33+3$    | 0.115<br>1.55+3         | $0.121 \\ 1.82 + 3$ | 0.129<br>2.16+ |
|                   |         |                |         |                          |                     |                   |                         |                     |                |

The table is to be read as indicated by the following example for the 0.74 cm<sup>-1</sup> line, J'=0, J''=5,  $\tau'=-5$ ,  $\tau''=-1$ ,  $S=1.35\times 10^{-1}$  g<sup>-1</sup> cm<sup>-1</sup>, C=0.087 cm<sup>-1</sup>. The isotope is  $H_2O^{14}$  unless indicated otherwise; D corresponds to  $H_2O$ , C=0.087 cm<sup>-1</sup>.

Table III. (Continued)

|           | A T There again |                     |         |                            |                            |                       |                        |                  |          |
|-----------|-----------------|---------------------|---------|----------------------------|----------------------------|-----------------------|------------------------|------------------|----------|
| $cm^{-1}$ | J' = J''        | $rac{	au'}{	au''}$ |         |                            |                            | Temperat              | ure                    |                  |          |
|           |                 | τ ·                 | Isotope | 320°K                      | 300 K                      | 280°K                 | 260°K                  | 240°K            | 220°K    |
| 28.07     | 10<br>11        | $-\frac{1}{7}$      |         | 9.15 - 2                   | 6.45 - 2                   | 4.27 - 2              | 2.62 - 2               | 1.46-2           | 7.14-3   |
| 28.31     | 11              | - i                 | 7.      | 0.052                      | 0.053                      | 0.053                 | 0.054                  | 0.055            | 0.056    |
| 20.01     | 1               | — t                 | 1)      | 6.84 2                     | 7.93 - 2                   | 9.28 - 2              | 1.10 - 1               | 1.31 - 1         | 1.59-1   |
| 28.68     | 2               | 0                   |         | 0.095                      | 0.000                      | 0.10                  | 0.11                   | 0.12             | 0.12     |
| 20.00     | $\frac{2}{2}$   | 2                   |         | 1.03                       | 7.29 - 1                   | 4.87 - 1              | 3.02 - 1               | 1.70 - 1         | 8.44 - 2 |
| 29.77     | ī               | - 2                 | D       | 0.100 $3.99 - 1$           | 0.104                      | 0.109                 | 0.115                  | 0.121            | 0.129    |
|           | ò               | ő                   | 17      | 0.096                      | 4.67 - 1                   | 5.52 - 1              | 6.60 - 1               | 8.00 - 1         | 9.85 - 1 |
| 30,00     | 2               | <b>–</b> 2          |         | 4.34 - 1                   | 0.100                      | 0.105                 | 0.110                  | 0.117            | 0.124    |
|           | ī               | Õ                   |         | 0.000                      | 3.11 - 1                   | 2.10 - 1              | 1.32 - 1               | 7.50 - 2         | 3.79 - 2 |
| 30.13     | 3               | - 1                 |         | 3.13 - 1                   | 0.103                      | 0.108                 | 0.113                  | 0.119            | 0.126    |
|           | 2               | i                   |         | 0.092                      | 2.17 - 1 $0.095$           | 1.41 - 1              | 8.49 - 2               | 4.61 - 2         | 2.20 - 2 |
| 30.23     | 9               | -6                  |         | 1.03                       | 8.79 ~ 1                   | 0.098<br>7.25—1       | 0.10                   | 0.11             | 0.11     |
|           | 8               | -2                  |         | 0.077                      | 0.080                      |                       | 5.72 - 1               | 4.28 - 1         | 2.97 - 1 |
| 30.56     | 4               | ō                   |         | 4.34 + 1                   | $4.66 \pm 1$               | $0.083 \\ 4.99 \pm 1$ | 0.086                  | 0.089            | 0.094    |
|           | 3               | 2                   |         | 0.083                      | 0.086                      | 0.091                 | $\frac{5.33+1}{0.095}$ | 5.67 + 1         | 5.97 + 1 |
| 32.37     | .5              | <b>-</b> 2          |         | 5.07 + 1                   | 5.28+1                     | 5.47 + 1              | 5.62 + 1               | 0.100            | 0.107    |
|           | 4               | 2                   |         | 0.080                      | 0.083                      | 0.086                 | 0.090                  | 5.70 + 1 $0.094$ | 5.70 + 1 |
| 32.91     | 2               | <b>-</b> 2          |         | 7.17 + 2                   | 8.29+2                     | 9.67 + 2              | 1.14+3                 | 1.36+3           | 0.098    |
| 22.24     | 1               | 0                   |         | 0.009                      | 0.103                      | 0.108                 | 0.113                  | 0.120            | 0.127    |
| 33.21     | 3               | -3                  | Ð       | 5.30 - 1                   | 6.20-1                     | 7.17 - 1              | 8.38-1                 | 9.88-1           | 1.18     |
| 22.45     | 2<br>5          | <b>-1</b>           |         | 0.095                      | 0.099                      | 0.10                  | 0.11                   | 0.11             | 0.12     |
| 33.47     | 5               | -2                  | 18      | 6.88 - 2                   | 7.18 - 2                   | 7.44 - 2              | 7.65 - 2               | 7.77 — 2         | 7.78-2   |
| 33.68     | 4               | 2                   | _       | 0.080                      | 0.083                      | 0.086                 | 0.090                  | 0.094            | 0.099    |
| 55.08     | 2               | 0                   | D       | 9.45 - 2                   | 1.09 - 1                   | 1.281                 | 1.51 - 1               | 1.80 - 1         | 2.17-1   |
| 36,59     | 1<br>3          | 1                   |         | 0.100                      | 0.104                      | 0.108                 | 0.113                  | 0.119            | 0.125    |
| *1119     | 3               | 1                   |         | 4.87 + 3                   | $5.46 \pm 3$               | 6.15 + 3              | 6.96 + 3               | 7.91 + 3         | 9.02 + 3 |
| 36.74     | 1               | -3                  | 4.0     | 0.095                      | 0.099                      | 0.104                 | 0.110                  | 0.116            | 0.124    |
| 30.74     | 0               | 0                   | 18      | 2.83                       | 3.31                       | 3.91                  | 4.67                   | 5.65             | 6.95     |
| 37.14     | 1               | 0                   |         | 0.096                      | 0.100                      | 0.105                 | 0.110                  | 0.117            | 0.124    |
| 07.17     | ò               | 0                   |         | 1.41+3                     | $1.65 \pm 3$               | 1.95 + 3              | 2.33 + 3               | 2.82 + 3         | 3.47 + 3 |
| 37.90     | 3               | 1                   | 18      | 0.096                      | 0.100                      | 0.105                 | 0.111                  | 0.117            | 0.124    |
|           | 3               | <b>—</b> 1          | 18      | 1.05 + 1                   | 1.17+1                     | 1.30 + 1              | 1.45 + 1               | 1.62 + 1         | 1.81 + 1 |
| 38.24     | 7               | -3                  |         | 0 001<br>3 74              | 0.095                      | 0,100                 | 0.10                   | 0.11             | 0.12     |
|           | 8               | -7                  |         | 0.078                      | 3.49                       | 3.19                  | 2.84                   | 2.44             | 2.00     |
| 38 45     | 3               | -1                  |         | 7.41 + 2                   | 0.080                      | 0.083                 | 0.086                  | 0.089            | 0.093    |
|           | 2               | i                   |         | 0.001                      | 8.32 + 2 $0.095$           | 9.37+2                | 1.06+3                 | 1.21 + 3         | 1.38 + 3 |
| 38.62     | 6               | – î                 |         | $8.18 \pm 1$               | $7.96 \pm 1$               | 0.099                 | 0.104                  | 0.109            | 0.115    |
|           | 5               | .3                  |         | $\frac{6.18 \pm 1}{0.070}$ | $\frac{7.96 \pm 1}{0.071}$ | 7.62 + 1              | 7.15 + 1               | 6.53 + 1         | 5.75 + 1 |
| 38.79     | 3               | ï                   |         | 5.37 + 3                   | $5.96 \pm 3$               | 0.073<br>6.63+3       | 0.076                  | 0.078            | 0.081    |
|           | 3               | - i                 |         | 0.091                      | 0.095                      | 0.03+3<br>0.099       | 7.39 + 3               | 8.25 + 3         | 9.23 + 3 |
|           |                 | -                   |         | 0,1771                     | 0,090                      | 0.099                 | 0.105                  | 0.111            | 0.117    |

where  $\rho$  = water vapor density in gm/cm<sup>3</sup>

T = absolute temperature, °K

P = pressure in mm mercury.

For water vapor, in the Gross equation for the attenuation, the strength function S is

$$S \sim \rho T^{-5/2} \exp(-a/T)$$
,

where a varies from line to line.

The line breadth depends on the collisions of the polar molecules with like molecules and other molecules in the atmosphere. For oxygen, Meeks and Lilley  $^8$  give the line breadth  $\Delta\nu(P_1T)$  by the equation

$$\Delta v(P_1T) = A P \left[0.21 + 0.78B\right] \begin{bmatrix} T \\ O \end{bmatrix} 0.85$$

where A specifies the line broadening at unit pressure (= 1.95MHZ(mmHgl))

and B specifies the relative effectiveness of the N $_2$  - O $_2$  collisions as compared to the O $_2$  - O $_2$  collisions (= .25 for pressures less than 267mmHg).

In a report by Richard Longbothum  $^9$ , the water vapor resonant scattering cross sections  $\sigma$  (for high altitudes, 30 -80 km) at 22 GHz (22.235 GHz, or 1.35 cm) and at 183 GHz (183.31 GHz or 1.64mm) are given by

$$\sigma(v,T,N,v_o) = \frac{K_a(v.T,N,v_o)}{N(h)},$$

where

N(h) = number of water vapor molecules/cm<sup>3</sup> for a path length h.

At 22.235 GHz, the absorption coefficient  $K_a$ , for a pressure broadened line  $^{10}$ , is given by

$$K_{a} = 1.05 \times 10^{-28} \frac{\text{Nv}^{2}}{\text{T}^{5/2}} \exp(-644/\text{T}) \qquad \frac{\Delta v}{(v - v_{0})^{2} + \Delta v^{2}} + \frac{\Delta v}{(v + v_{0})^{2} + \Delta v^{2}} + \frac{\Delta v}{(v + v_{0})^{2} + \Delta v^{2}}$$

$$+ 1.52 \times 10^{-52} \frac{\text{Nv}^{2} \Delta v}{\text{T}^{3/2}} \text{ cm}^{-1}$$

where

N = Number density of water vapor molecules in a cm<sup>3</sup>

v = frequency in Hertz

T - Kinetic temperature in °K.

At 183.31 GHz, the absorption coefficient for a pressure broadened line is (after Croom, Ref. 11)

$$K_{a} = 6.46 \times 10^{-29} \frac{Nv^{2}}{T^{5/2}} \exp(-200/T) \qquad \left[ \frac{\Delta v}{(v - v_{0})^{2} + \Delta v^{2}} + \frac{\Delta v}{(v + v_{0})^{2} + \Delta v^{2}} \right]$$

$$+ 1.8 \times 10^{-52} \frac{Nv^{2} \Delta v}{T^{3/2}} \text{ cm}^{-1}.$$

When both doppler and pressure broadening are applicable (altitude above 70 km) the 1/2 width  $\Delta v$  is given by

$$\Delta v \simeq (\Delta v_p^2 + \Delta v_D^2)^{-1/2}$$
.

The pressure broadening  $\Delta\nu_{p}$  is given by (Croom, Ref. 11) as

$$\Delta v_p = 2.62 \times 10^9 \frac{\left(\frac{P}{1013.25}\right)}{\left(\frac{T}{318}\right)^{0.625}} \cdot (1 + 0.0046\rho) \text{ Hz},$$

where

P = total atmospheric pressure in mb

 $\rho$  = density of water vapor in gm m<sup>-3</sup>

 $T = kinetic temperature in {}^{\circ}K.$ 

The doppler broadening  $\Delta\nu_{\mbox{\scriptsize D}}$  is given by (Croom, Ref. 11) as

$$\Delta v_{\rm D} = 8.45 \times 10^{-7} v_{\rm Q} \sqrt{\rm T} \text{ Hz}.$$

A plot of the absorption cross sections for the two main lines, at 22 and 183 GHz, is shown in Fig. 3. Data for this plot is tabulated in Table IV. These data were abstracted from Longbothum, Ref. 9. Persual of this table (which includes line widths) shows the broadening of line widths of the absorption cross sections as the altitude decreases from 120 km to 30 km.

One variable that is often elusive in a set of atmospheric transmission measurements is that of the water vapor pressure and atmospheric water content. These two parameters are presented next as Fig. 4, atmospheric water vapor content and Fig. 5, water vapor pressure as a function of temperature and relative humidity. Both of these curves are from A. R. Downs 12.

Before leaving the discussion of basic atmospheric attenuation of mm and sub mm wavelengths, mention should be made of two papers on the physical properties of the oxygen molecule. Welch and Mizushima  $^{13}$  have given a table of observed and calculated frequencies of the  $\mathrm{O}_2$  molecule, from 53.066 GHz to 3865.81 GHz (given here as Table V). A result of a nonlinear least squares fit to 25 microwave and 3 sub mm and IR wavelengths is a set of molecular parameters for  $\mathrm{O}_2$ , given here as Table VI.

Ott and Thomson  $^{14}$  discussed the index of refraction of air (oxygen) in the 55-65 GHz region in their article "Characteristics of a Radio Link in the 55-65 GHz range." They give the path averaged refractive index  $n(\nu)$  as a sum of frequency dependent and independent parts,

$$n(v) = 1 + \frac{77.63}{T} \left(P + \frac{4810e}{T}\right) \cdot 10^{-6}$$

$$+\frac{(S/\gamma)\cdot 10^{-4}}{(-i+Z)}\cdot \frac{300}{T}^{2}\left(\frac{P}{1013.25}\right)$$

with 
$$Z = (v_0 - v)/\gamma$$

T = absolute temperature °K

P and e are in millibars (1 mb = 0.75006376 Torr).

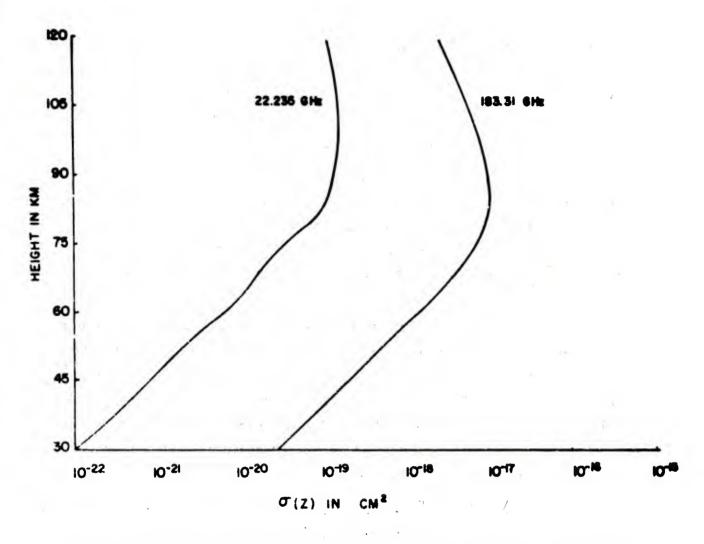


Fig. 3. Absorption Cross Sections for Water Vapor at 22.235 and 183.31 GHz vs. Height (Data from Ref. 9)

Table IV. Absorption Cross Sections for Water Vapor

(Data from Ref. 9)

| σ <sub>183</sub> (h) | $2.6 \times 10^{-20} \text{ cm}^2$   | $9.5 \times 10^{-20} \text{ cm}^2$ | $3.1 \times 10^{-19} \text{ cm}^2$ | $1.3 \times 10^{-18} \text{ cm}^2$ | $3.9 \times 10^{-18}  \mathrm{cm}^2$ | $8.3 \times 10^{-18} \text{ cm}^2$ | $7.8 \times 10^{-18}  \mathrm{cm}^2$ | $5.8 \times 10^{-18} \text{ cm}^2$   | $3.7 \times 10^{-18} \text{ cm}^2$   | 1.9 x 10 <sup>-18</sup> cm <sup>2</sup> |
|----------------------|--------------------------------------|------------------------------------|------------------------------------|------------------------------------|--------------------------------------|------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-----------------------------------------|
| σ <sub>22</sub> (h)  | $1.0 \times 10^{-22}  \mathrm{cm}^2$ | $4.0 \times 10^{-22} \text{ cm}^2$ | $1.5 \times 10^{-21} \text{ cm}^2$ | $6.1 \times 10^{-21} \text{ cm}^2$ | $1.7 \times 10^{-20}  \mathrm{cm}^2$ | $6.6 \times 10^{-20}  \text{cm}^2$ | $1.3 \times 10^{-19}  \mathrm{cm}^2$ | $1.4 \times 10^{-19}  \mathrm{cm}^2$ | $1.3 \times 10^{-19}  \mathrm{cm}^2$ | $1.0 \times 10^{-19}  \mathrm{cm}^2$    |
| Δν <sub>183</sub>    | $4.0 \times 10^7 \text{ Hz}$         | $9.7 \times 10^6 \text{ Hz}$       | $2.7 \times 10^6 \text{ Hz}$       | $7.1 \times 10^5 \text{ Hz}$       | $3.3 \times 10^5 \text{ Hz}$         | $2.1 \times 10^5 \text{ Hz}$       | $1 \times 10^5 \text{ Hz}$           | $2.2 \times 10^5 \text{ Hz}$         | $2.5 \times 10^5 \text{ Hz}$         | $2.9 \times 10^5 \text{ Hz}$            |
| * Δν 22              | 4.0 x 10 <sup>7</sup> FIz            | 9.7 × 10 <sup>6</sup> Hz           | $2.7 \times 10^6 \text{ Hz}$       | $6.6 \times 10^5 \text{ Hz}$       | $2.3 \times 10^5 \text{ Hz}$         | $5.0 \times 10^4 \text{ Hz}$       | $2.6 \times 10^4 \text{ Hz}$         | $2.8 \times 10^4 \text{ Hz}$         | 3.0 x 10 <sup>4</sup> Hz             | $3.5 \times 10^4 \text{ Hz}$            |
| L L                  | 30 km                                | 40 km                              | 50 km                              | 60 km                              | 70 km                                | 80 km                              | 90 km                                | 100 km                               | 110 km                               | 120 km                                  |

\* (See Appendix A of Ref. 9)

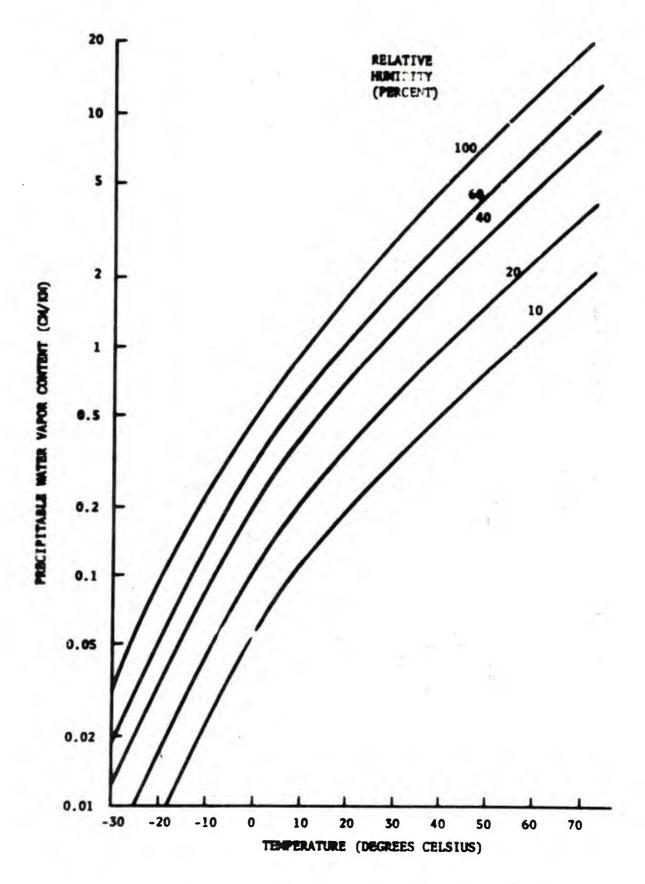


Fig. 4. Atmospheric Water Vapor Content (Data from Ref. 12)

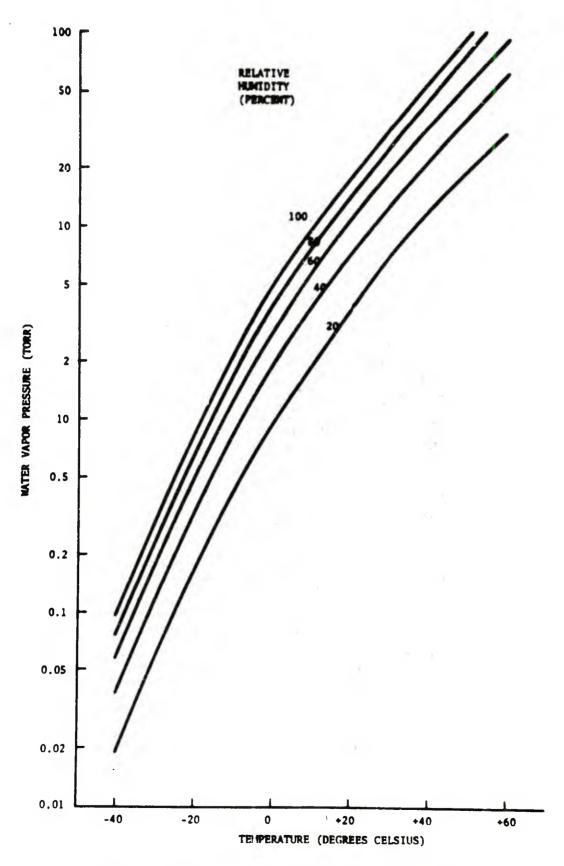


Fig. 5. Water Vapor Pressure as a Function of Temperature and Relative Humidity (Data from Ref. 12)

Table V. Observed and Calculated Frequencies of Oxygen Lines (GHz).

| Transition |          | Observed                             | Calculated  |  |
|------------|----------|--------------------------------------|-------------|--|
| n,J[-      | -]n', J' | frequency <sup>a</sup>               | frequency   |  |
| 1,2        | 1,1      | 56,264778(M)<br>56,264766(W)         | 56, 264 758 |  |
| 3,4        | 3,3 -    | 58,446 600 (M)<br>58,446 580 (Z)     | 58,446580   |  |
| 5,6        | 5,5      | 59.590 978(Z)                        | 59.590 979  |  |
| 7,8        | 7,7      | 60.434776(Z)                         | 60.434778   |  |
| 9,10       | 9,9      | 61.150 570(Z)                        | 61.150 567  |  |
| 11,12      | 11,11    | 61,800 169 (W)<br>61,800 155 (Z)     | 61,800 167  |  |
| 13,14      | 13,13    | 62.411 223(Z)                        | 62.411234   |  |
| 15,16      | 15, 15   | 62.996 G(H)b                         | 62, 997 999 |  |
| 17,18      | 17, 17   | 63,568520(Z)                         | 63,568542   |  |
| 19,20      | 19, 19   | 64.127777(W)                         | 64.127790   |  |
| 21,22      | 21, 21   | 64.6782(II)b                         | 64,678 920  |  |
| 23,24      | 23,23    | 65,22412(Z)                          | 65, 224 076 |  |
| 25, 26     | 25, 25   | 65.764744(W)                         | 65,764760   |  |
| 1,0        | 1,1      | 118,750 343(M)                       | 118.750 330 |  |
| 3,2        | 3,3      | [62, 486 255 (Z)<br>[62, 486 255 (M) | 62, 486 267 |  |
| 5,4        | 55, 5    | 60,306044(Z)                         | 60,306065   |  |
| 7,6        | 7,7      | 59, 164 215 (Z)                      | 59, 164 211 |  |
| 9,8        | 9,9      | 58,323885(Z)                         | 58,323883   |  |
| 11,10      | 11, 11   | 57, 611 4 a n h                      | 57,612 492  |  |
| 13,12      | 13,13    | 56, 965 T40 <i>0</i> (3)             | 56,968214   |  |
| 15,14      | 15, 15   | 56,363393(W)                         | 56, 363 397 |  |
| 17,16      | 17,17    | 55,733 819(W)                        | 55.783 805  |  |
| 19,18      | 19,19    | 55.221372(W)                         | 55.221362   |  |
| 21,20      | 21, 21   | 54,671145(W)                         | 54.671141   |  |
| 23,22      | 23, 23   | 54.1294(H) <sup>b</sup>              | 54, 129 962 |  |
| 25,24      | 25, 25   | 53.5994(H) <sup>b</sup>              | 53,595 682  |  |
| 27,26      | 27,27    | 53.066 8 (Wa)                        | 53,066 802  |  |
| 1, 1       | 3, 3     | 430,985277(M)                        | 430.985 276 |  |
| 13, 13     | 15, 15   | 2496.283 (E)                         | 2496.283    |  |
| 21, 21     | 23, 23   | 3865,81(E)                           | 3865.810    |  |

<sup>a</sup>(E) See Ref. 12, (II) see Ref. 7, (M) see Ref. 11, (W) see Ref. 6, (Wa) see Ref. 10, (Z) see Ref. 5.

Note: The references indicated above are references in Ref. 13 of this report.

Line not included in fit.

Table VI. Molecular Parameters of Oxygen Molecule
(GHz)

| (Data from Ref. 13 | ) |
|--------------------|---|
|--------------------|---|

| Parameter              | Wilheit and<br>Barrett  | Butcher, et al.          | Present Work                  |
|------------------------|-------------------------|--------------------------|-------------------------------|
| Во                     | 43.100589               | 43.10059 (27)            | 43.100518 (3) <sup>a</sup>    |
| · B <sub>1</sub>       | $-1.4 \times 10^{-4}$   | $-1.454$ (4) x $10^{-4}$ | $-1.449629$ (9) x $10^{-4}$   |
| <sup>B</sup> 2         |                         |                          | $-1.57$ (11) x $10^{-10}$     |
| $\lambda_{\mathbf{o}}$ | 59.501346               |                          | 59.501342 (7)                 |
| $^{\lambda}$ 1         | $5.845 \times 10^{-5}$  |                          | $5.847$ (3) x $10^{-5}$       |
| ho                     | -0.2525917              |                          | -0.2525865 (10)               |
| $^{	extstyle{\mu}}1$   | $-2.455 \times 10^{-7}$ |                          | $-0.2464 (20) \times 10^{-7}$ |
|                        | £                       |                          |                               |

Note: The statistical uncertainties quoted are approximately two standard deviation limits and do not include explicitly experimental uncertainties of the frequencies measurements. The standard deviations were estimated from the last iteration of the nonlinear fitting procedure based upon Taylorseries expansion about the estimated values.

These authors choose to use a "Lorentzian" line shape:

S = 5220 Hz

 $\gamma$  = 3.92 GHz = line width

 $v_0$  = center frequency in GHz

Different authors seemed to have "favorite" collision broadened reasonant line width functions (equivalent reasonant cross sections); from data by Burch (7), the experimental values favor (for  $\nu$ < 15.5 cm<sup>-1</sup>,  $\lambda$ >.645 mm) the Van Vleck-Weiskopf function. Above that frequency ( $\lambda$ <.645mm) Burch feels that the Gross/Zhevakin-Naumov form fits the data on water vapor best.

The general data coverage on atmospheric transmission is heavier on the microwave - mm wave end than it is on the 100  $\mu m$  end. A rough estimate is that there are 3 - 5 times the experimental and theoretical article coverage at the 30-300 GHz end (1 cm - 1 mm) than there is from 1 mm to 100  $\mu m$ .

As a final note on general atmosphere transmission, we would like to mention the following five papers which have attenuation calculations and measurements, line width functions, etc:

- a) "Atmospheric Absorption of Radio Waves Between 150 and 350 GHz" by F. T. Ulaby and Archie Straiton  $^{16}$
- b) "Calculations of Antenna Temperature, Horizontal Path Attenuation and Zenith Attenuation due to Water Vapor in the Frequency Band 150 700 GHz" by R. W. McMillan, J. J. Gallagher, and A. M. Cook 17
- c) "Water Vapor Absorption Spectra of the Upper Atmosphere" (45-185 cm), by G. C. Auguson, A. J. Mord et al. 18
- d) "Method of Calculating the Atmospheric Water Vapor Absorption of MM and Sub MM Waves" by A. Yu.  $Zrazkevskiy^{19}$
- e) "Temperature Dependence of the Absorption of Radio Waves by Atmospheric Water Vapor at the 10 cm 0.27 mm Wavelengths," by K. A. Aganbekyan, A. Yu. Zrazkevskiy and V. G. Malinkin.<sup>20</sup>

Two curves from McMillan et al<sup>17</sup> serve to summarize much of the atmospheric attenuation data in the mm - sub mm range. Fig. 6 presents horizontal-path attenuation vs. frequency at sea level, and Fig. 7 presents the total zenith attenuation from sea level.

#### 2.2 Atmospheric Index of Refraction

The atmospheric index of refraction is an important parameter which has received much less attention in the literature than atmospheric propagation. An illustration of the problem is from Davis and Cogdell to who measured the "differential refractive index" with their 16 foot antenna on Mt. Locke. This is a measure of the difference in pointing direction between optical and radio frequency waves and for some high resolution antennae, this difference (antenna point angle error) can be on the order of the beam width of the antennae. Davis and Cogdell's analysis of their data suggests that the refractive index is fairly well known up to 100 GHz and is given by

$$N = (77.6P/T) [1 + (4810/T) (e/p)].$$

where

T = temperature <sup>O</sup>K

P = pressure in mbar

e = water vapor partial pressure in mbar.

Above  $100~\mathrm{GHz}$  and below the  $140~\mathrm{GHz}$  atmospheric window there is a downward break in the index of refraction as a function of frequency.

In retrospect, one would expect a set of "sag effects" in the antenna pointing error each time the frequency crosses a main atmosphere resonance line. The main absorption lines, below 200 GHz, are at 22 and 183 GHz (water vapor) and at 60 and 118 GHz ( $^{0}_{2}$ ). Davis and Cogdell saw their "sag effect" in the antenna point angle error on either side (97 and 140 GHz) of the 118 GHz  $^{0}_{2}$  resonance line. It is suspected that

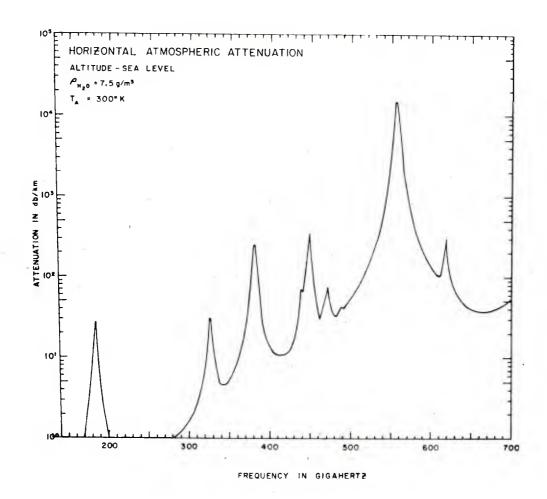


Fig. 6. Horizontal-path Attenuation Versus Frequency at Sea Level (Data from Ref. 17)

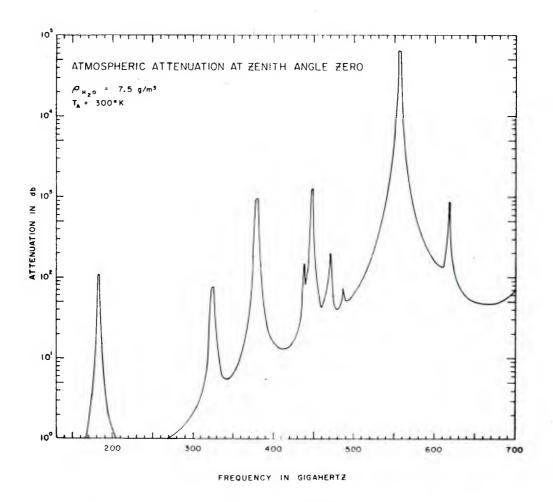


Fig. 7. Total Zenith Attenuation from Sea Level (Data from Ref. 17)

this sort of thing will happen on each side of major atmospheric reasonances, at the frequencies noted just previously, and at higher frequencies, as per the tables of resonances by Corcoran (Table 1) and by Burch (Table III). Also, as the atmospheric attenuation is a function of the relative humidity, so is the index of refraction; one might question if the "sag effect" is more pronounced about either side of the water vapor resonance/absorption lines than about the 60 and 110 GHz oxygen line.

## 2.3 Attenuation and Scattering by Fog, Rain and Clouds

If one knew the size distribution of the water droplets contained in fog, rain or clouds and the complex index of refraction for water as a function of wavelength and temperature, then it is possible to determine the scattering, absorption and extinction cross sections and the phase function with the application of Mie theory. The data available on the complex index of refraction is not very complete and there is not very good agreement in the various published values as a function of wavelength and temperature. For 20°C water, Deirmendjian  $^{21,22}$  has compiled a set of measured data from 12  $\mu m$  to 1000  $\mu m$ . For wavelengths between 2 mm and 33 mm Deirmendjian used the Debye equation to compute the complex index of refraction for water.

Table VII presents Deirmendjian's collection of complex index of refraction data for water. Dorothy Stewart 23 has tabulated a set of indexes of refraction at 4 wavelengths, .55  $\mu$ m, 10.6  $\mu$ m, 870  $\mu$ m, and 1250 µm. Table VIII lists the data she used in her very comprehensive article on infrared and submillimeter extinction by fog. She mentions in her article about recent sources of complex index of refraction data on water. Table IX, from the 1971 Chemical Rubber Company Handbook of Chemistry and Physics, is a listing of data from two different groups on how the static dielectric constant of water varies with temperature. The static dielectric constant is not a constant, as usually assumed, but varies with temperature. Hale and Querry did a very extensive survey of the optical constants of water with 59 reference listings; they computed the real part of the index of refraction doing a Cauchy principle value integration of smooth curve fits of all available data on the imaginary parts of the index of refraction,  $k(\lambda)$ , of water, from 200 nm to 1 meter wavelength. They produced a table for the complex index of refraction of water from 20 nm to 200  $\mu m$  (just the 100  $\mu m$  - 200  $\mu m$  section is reproduced here as Table X.) R. K. Crane in his article "Microwave Scattering Parameters for New England Rain" presented two sets of calculations of the microwave index of refraction: one set was based on Debye's formula of the index of refraction of water using Kerr Coefficients and the other set is attributed by Crane to Grant et al. The results of these calculations

Table VII. Complex Indices of Refraction vs Wavelength for Water (From Refs. 21, 22)

| λ            | Index of Refraction | λ       | Index of Refraction |
|--------------|---------------------|---------|---------------------|
| 12.µm        | 1.111 - 0.199i      | 500.μm  | 2.22 - 0.740i       |
| 17. $\mu m$  | 1.376 - 0.429i      | 700.µm  | 2.32 - 0.890i       |
| 28.µm        | 1.549 - 0.338i      | 1000.µm | 2.50 - 1.09i        |
| 40.μm        | 1.519 - 0.385i      |         |                     |
| 60.μm        | 1.703 - 0.587i      | 2.mm    | 2.5604 - 0.8947i    |
| 100. $\mu m$ | 2.06 - 0.551i       | 5.mm    | 3.1918 - 1.7657i    |
| 140.μm       | 2.07 - 0.470i       | 10.mm   | 4.2214 - 2.5259i    |
| 200.µm       | 2.08 - 0.509i       | 20.mm   | 5.8368 - 3.0046i    |
| 337.μm       | 2.20 - 0.600i       | 33.mm   | 7.1755 - 2.8642i    |
|              |                     |         |                     |

Table VIII. Indices of Refraction for Water (From Ref. 23)

| (µm) | Index of Refraction                |
|------|------------------------------------|
| 0.55 | 1.333 - 1.96 (10 <sup>-9</sup> ) i |
| 10.5 | 1.185 - 0.0662 i                   |
| 870  | 2.422 - 0.9667 i                   |
| 1250 | 2.630 - 1.1407 i                   |
|      | 0.55<br>10.5<br>870                |

<sup>\*</sup>The index of refraction for 870  $\mu\text{m}$  is an interpolated value.

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| t°C | ε*    | ٤†    | t°C | £ <b>*</b> | ε†    |
|-----|-------|-------|-----|------------|-------|
| 0   | 87.74 | 87.90 | 50  | 69.91      | 69.88 |
| 5   | 85.76 | 85.90 | 55  | 68.34      | 68.30 |
| 10  | 83.83 | 83.95 | 60  | 66.81      | 66.76 |
| 15  | 81.95 | 82.04 | 65  | 65.32      | 65.25 |
| 18  | 80.84 | 80.93 | 70  | 63.86      | 63.78 |
| 20  | 80.10 | 80.18 | 75  | 62.43      | 62.34 |
| 25  | 78.30 | 78.36 | 80  | 61.03      | 60.93 |
| 30  | 76.55 | 76.58 | 85  | 59.66      | 59.55 |
| 35  | 74.83 | 74.85 | 90  | 58.32      | 58.20 |
| 38  | 73.82 | 73.83 | 95  | 57.01      | 56.88 |
| 40  | 73.15 | 73.15 | 100 | 55.72      | 55.58 |
| 45  | 71.51 | 71.50 |     |            |       |

<sup>\*</sup>From data of Malmberg and Maryott (1956).

Table X. Complex Indices of Refraction vs Wavelength for Water (from Ref. 25)

| <br>m = n' + i n''      |        |       |  |  |  |  |
|-------------------------|--------|-------|--|--|--|--|
| λ <b>(</b> μ <b>m</b> ) | n''(λ) | n'(λ) |  |  |  |  |
| 100                     | -0.532 | 1.957 |  |  |  |  |
| 110                     | -0.531 | 1.966 |  |  |  |  |
| 120                     | -0.526 | 2.004 |  |  |  |  |
| 130                     | -0.514 | 2.036 |  |  |  |  |
| 140                     | -0.500 | 2.056 |  |  |  |  |
| 150                     | -0.495 | 2.069 |  |  |  |  |
| 160                     | -0.496 | 2.081 |  |  |  |  |
| 170                     | -0.497 | 2.094 |  |  |  |  |
| 180                     | -0.499 | 2.107 |  |  |  |  |
| 190                     | -0.501 | 2.119 |  |  |  |  |
| 200                     | -0.504 | 2.130 |  |  |  |  |
| <br>                    |        |       |  |  |  |  |

<sup>†</sup>From data of Owen, Miller, Milner and Cogan (1961).

for frequencies between 8 and 70 Ghz are presented here as Table XI. The disagreements between the two sets of refractive indices are more pronounced in the complex part, n", than in the real part, n'. Crane took the Debye index of refraction to be defined by

$$n(\lambda) = \sqrt{\frac{88 - 5.5}{1 + \frac{i \cdot \Delta \lambda(T)}{\lambda}} - 5.5} = n' + i \cdot n''$$

where  $\Delta\lambda(T)$  = temperature-dependent 1/2 width. "88" is actually a temperature-dependent static dielectric constant at 0 frequency. Wilcox and Grazino  $^{27}$  developed a compilation of the index of refraction of water vs temperature for  $\lambda$  = 1, 3, and 10 mm radiation, shown here as Table XII.

There seems to be a great amount of faith put on the use of the Debye formula for calculating the complex index of refraction of water in the microwave and millimeter wavelength range. It would be interesting to see some <u>measured</u> data in the 1250  $\mu m$  - 1 cm wavelength region, as there was in the 12  $\mu m$  - 100  $\mu m$  region for Deirmendjian's report.

To help visualize better some of the previously-described tabulated measured data on the complex index of refraction for water at wavelengths between 10 and 1000  $\mu m$ , several curves from Deirmendjian  $^{22}$  are reproduced here as Fig. 8. Also, in Fig. 9. we present the extinction coefficient of water as given by Hale and Querry  $^{25}$  (imaginary part of complex index of refraction) as a function of wavelength for wavelengths between  $10^{-6}$  m and 1 meter. Fig. 10 shows a set of plots from Hale and Querry  $^{25}$  giving the real part of the index of refraction of water for the spectral region 0.2 - 200  $\mu m$ . The individual data points on each set of curves refer to individual authors data that Deirmendjian and Hale and Querry, respectively, used. For further details about these points, please consult Refs. 21, 22, and 25.

Table XI. Refractive Index of Water for a Drop Temperature of 0.0°C

(Data from Ref. 26)

Computed Using Debye Model with Kerr Coefficients

| Frequency (GHz) | n <b>'</b>      |           | n''     |
|-----------------|-----------------|-----------|---------|
| 8.00            | 7.4786          |           | -2.7721 |
| 9.35            | 7.0969          |           | -2.9060 |
| 15.50           | 5.7619          | ž.        | -3.0278 |
| 35.00           | 3.9533          |           | -2.4301 |
| 70.00           | 3.0179          | . * . =   | -1.6856 |
| * ×             |                 |           |         |
| Computed Using  | Data Attributed | to Grant, | et al.  |

| 8.00  | 7.6474 | -2.7146 |
|-------|--------|---------|
| 9.35  | 7.2788 | -2.8692 |
| 15.50 | 5.9459 | -3.0694 |
| 35.00 | 4.055  | -2.5465 |
| 70.00 | 3.0410 | -1.8093 |

Table XII. Indices of Refraction for Water vs Wavelength (from data in Ref. 27)

| λ (mm)      | Temperature | :                                     | Index of       |
|-------------|-------------|---------------------------------------|----------------|
| /( (min)    | (deg C)     |                                       | refraction     |
| 1           | 0           |                                       | 2.407 - i0.477 |
|             | 10          |                                       | 2.481 - i0.705 |
|             | 18          |                                       | 2.561 - i0.885 |
|             | 20          |                                       | 2.587 - i0.937 |
| 3           | 0           | · · · · · · · · · · · · · · · · · · · | 2.759 - i1.241 |
|             | 10          |                                       | 3.106 - i1.663 |
|             | 18          | , , , , , , , , , , , , , , , , , , , | 3.411 - i1.937 |
|             | 20          | 4,                                    | 3.505 - i2.007 |
| <del></del> |             |                                       |                |
| 10          | 0           |                                       | 4.221 - i2.526 |
|             | 10          |                                       | 5.155 - i2.834 |
|             | 18          |                                       | 5.817 - i2.869 |
|             | 20          | 41. 1                                 | 5.992 - i2.900 |
|             |             |                                       |                |

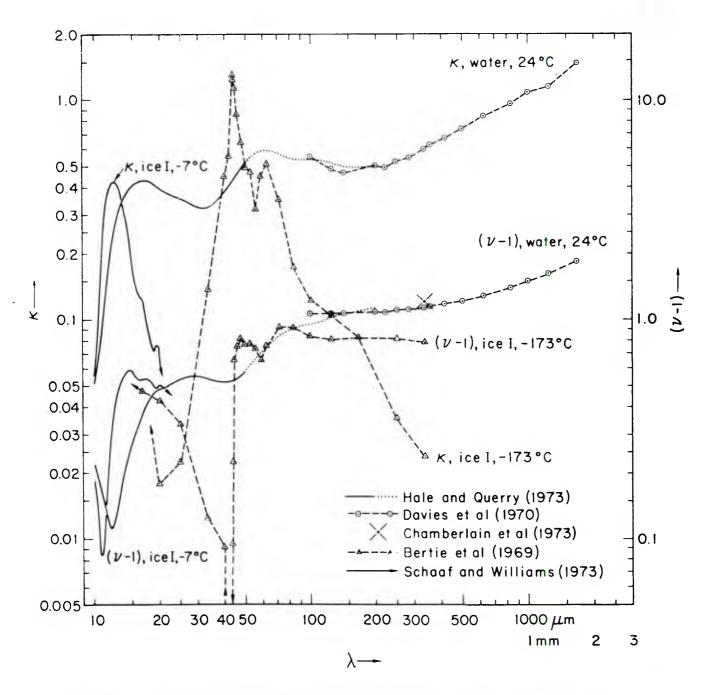


Fig. 8. Optical Constants of Water According to Recent Measurements (Data from Ref. 22)

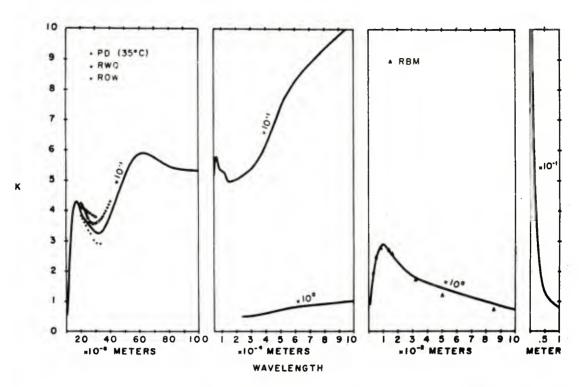


Fig. 9. Imaginary Part of the Index of Refraction of Water vs. Wavelength (from Ref. 25)

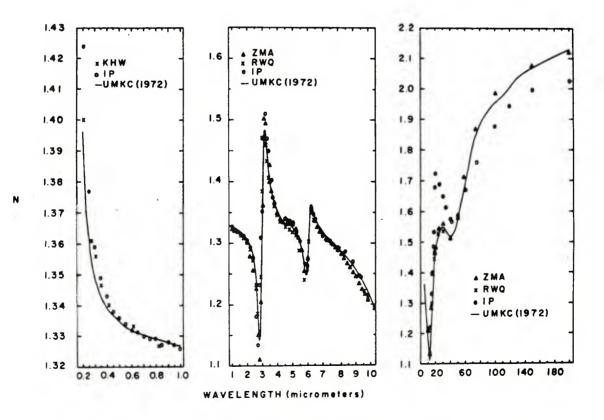


Fig. 10. Real Part of the Index of Refraction of Water vs. Wavelength (from Ref. 25)

Chamberlain, Zafer and Hasted $^{28}$  have measured the index of refraction of water between .1 mm and 0.5 mm using a Michelson interferometer. Results of their measurements, and some others they quote are shown in Fig. 11.

One needs to have indices of refraction (or the dielectric "constant", equivalently) available as a function of temperature when computing scattering, absorption and extinction cross sections with the use of Mie or Rayleigh theory.

The need for further work on the complex index of refraction for water is obvious; first in priority with respect to water is the need for experimental data on the complex index of refraction as a function of temperature over the entire wavelength range of interest. Most severe is the requirement in the 1 cm - 1 mm region where everyone seems to rely on the Debye equation with no references to actual dielectric/refractive index measurements in that spectral region.

A. Stogryn $^{29}$  has developed a modification of the Debye equation for the complex dielectric "constant" of saline water. He has given parameters in the equation as functions of water temperature and salinity. The dielectric constant is defined by

$$K = \varepsilon_{\infty} + \frac{\varepsilon_{o} - \varepsilon_{\infty}}{1 - i \cdot 2\tau \pi f} + \frac{i\sigma}{2\pi \varepsilon_{o}^{*} f}$$

with

 $\epsilon$  = temperature- and salt-control-dependent static dielectric constant

 $\tau$  = time constant as a function of temperature and normality of the salt solution =  $\tau(T,N)$ 

f = frequency in Hertz

 $\varepsilon_{\infty} = 5.5$ 

 $\sigma$  = ionic conductivity of the dissolved salt in mho/meter

 $\varepsilon_{o}^{*}$  = permittivity of free space = 8.854X10<sup>-12</sup> Farad/meter.

He gave  $\epsilon_0$ ,  $\tau$ , and  $\sigma$  as a function of the normality of the salt solution.

A relationship of this sort should be valuable in the calculation of scattering by slightly salty fogs (sea spray), or fogs that have become

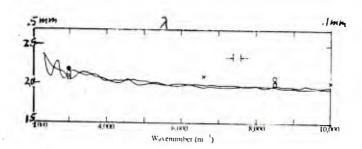


Fig. 11. Measured Values of the Real Component of the Refractive Index for Water (the full lines are from two independent measurements by the authors of Ref. 28. The points are measurements by other authors and by the authors of Ref. 28).

contaminated with ZnCl dust from smoke screens or from burning phosphorous, which forms  $^{P}2^{0}_{5}$ , which becomes dilute phosphoric acid when the  $^{P}2^{0}_{5}$  contacts a fog droplet.

There are several basic texts that are of value for information on dielectrics; these are: Dielectrics and Waves, by A. R. Von Hippel, Dielectric Materials and Applications, by A. R. Von Hippel, and The Theory of Electric and Magnetic Susceptibilities. Von Hippel's books have been the compendium of information on dielectric phenomena for 20 years. Van Vleck's treatise, now 44 years old, still is one of the best introductions to dielectric and magnetic phenomena extant. Van Vleck recently has written a revised version of his classic papers on line breadths and should be consulted for details as to validity of the formula presented here or by other authors regarding this area.

The principal difference between fog, rain and clouds when determining their scattering, absorption and extinction cross sections is in the range of drop diameters for each. The ranges of drop diameters for haze, fog, clouds, and rain, as given by G. D. Luhers, <sup>34</sup> are given in Table XIII. Note that although there is quite an overlap in drop diameters for fogs, clouds and rain, there is a tendency to larger drop diameters as the atmospheric conditions change from clouds to fog to rain.

The calculation of the absorption, scattering and extinction in a medium such as fog, clouds and rain is based on the knowledge of the absorption, scattering and extinction cross sections for individual particles. The theory for calculating these cross sections for individual spherical particles was developed by Mie. Mie's work was extended by Stratton and, as outlined in Kerr, by Goldstein. A Comprehensive study of the theory of electromagnetic scattering from small particles is also given by Van De Hulst.

A single dielectric sphere in the path of a plane wave will scatter and absorb some of the incident energy. These effects are characterized by several quantities called cross sections and have the dimensions

Table XIII. Drop Diameters for Various Atmospheric Conditions (from Ref. 34)

| ATMOSPHERIC CONDITION      | DROP SIZE RANGE Micrometers |
|----------------------------|-----------------------------|
| Haze                       | 0.01 - 3                    |
| Fog                        | 0.01 - 100                  |
| Clouds                     | 1 - 50                      |
| Drizzle (0.25 mm/hr)       | 3 - 800                     |
| Moderate Rain (4.0 mm/hr)  | 3 - 1500                    |
| Heavy Rain<br>(16.0 mm/hr) | 3 - 3000                    |

of area. The Gunn and East<sup>39</sup> definitions of the scattering, absorption, extinction, and backscatter cross-sections are:

Scattering Cross Section = 
$$\frac{\text{Total Power Scattered (over } 4\pi \text{ steradians)}}{\text{Incident Power Density}}$$

Absorption Cross Section = 
$$\frac{\text{Total Power Absorbed (as heat)}}{\text{Incident Power Density}}$$

Extinction Cross Section = 
$$\frac{\text{Total Power Lost (to the incident wave)}}{\text{Incident Power Density}}$$

The term extinction is used to describe the energy lost by the incident wave to a single particle; attenuation is the energy lost to a continuous volume of particles.

It should be noted that the conservation of energy requires that

$$Q_e = Q_a + Q_s$$

and

The scattering and absorption properties of single particles are complex functions of the size, shape, and index of refraction of the particles as well as the wavelength of the incident energy. The scattering, absorption, extinction and backscattering cross sections for 4.3 mm wavelength radiation interaction with spherical water spheres at 18°C (from Ref. 40), are presented in Fig. 12 as a function of the particle radius. It is seen that the cross sections increase with radius for radii between 0 and 6 mm.

For mm wavelength radar our interest lies in the backscatter and attenuation cross sections associated with a continuous distribution of particle sizes within a given volume. Particle size distributions for rain, fog and clouds are given by Deirmendjian 22 and Richard. If the particle size distribution is known, the reflectivity and attenuation can be determined, using the appropriate scattering theory.

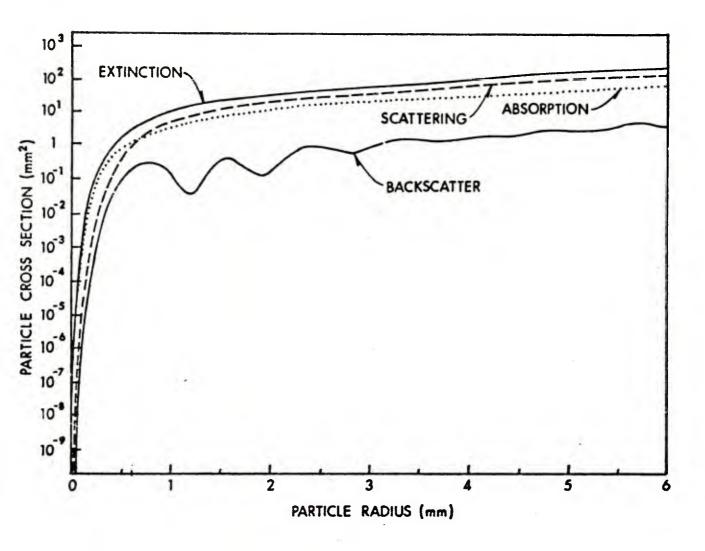


Fig. 12. Cross Sections of Water Spheres at 18°C for 4.3 mm Wavelength Energy (from Ref. 40)

The scattering theory to be used in the determination of the backscatter and attenuation of rain and fog depends on the size of the drops in the medium and the wavelength of the radiation. Mie scattering theory must be used for drops larger than 0.06 wavelength in diameter. For drops smaller than 0.06 wavelength the Rayleigh theory approximations are applicable.

Since rain is comprised of drops 258 micrometers (0.258 mm) and larger, Mie scattering theory must be used for millimeter wavelength radiation. The smaller drops in haze, fog and clouds allow the use of the Rayleigh approximation.

Fog results from the condensation of atmospheric water vapor into water droplets that remain suspended in the air. When the resulting cloud or water droplets or ice crystals envelop an observer and restrict his horizontal visibility to one kilometer or less, the international definition of fog has been satisfied. Evaporation and cooling are the principal physical processes which contribute to the formation of fog. Of the various fog classifications used by meteorologists, the two basic types of interest in radar applications are advection fog and radiation fog.

Advection is the horizontal movement of an air mass that causes changes in temperature or other physical properties. An advection (or coastal) fog is one which forms over open water as a result of the advection of warm moist air over colder water.

Radiation (or inland) fog forms in air that has been over land during the daylight hours preceding the night of its formation. Fogs which form in low, marshy land and along rivers on calm, clear nights are also considered radiation fogs.

The characteristics of these two fogs are given in Table XIV.

Note that the advection fog has a higher liquid water content, but greater visibility than the radiation fog. The correlation of visibility in fog to liquid water content is shown in Fig. 13 (from

Table XIV. Fog Characteristics
(Data from Ref. 40)

| ч                       | RADIATION<br>(INLAND) FOG | ADVECTION<br>(COASTAL) FOG |
|-------------------------|---------------------------|----------------------------|
| Average Drop Diameter   | 10 microns                | 20 microns                 |
| Typical Drop Size Range | 5-35 microns              | 7-65 microns               |
| Liquid Water Content    | 0.11 g/m <sup>3</sup>     | $0.17 \text{ g/m}^3$       |
| Droplet Concentration   | 200 cm <sup>-3</sup>      | - 40 cm <sup>-3</sup>      |
| Visibility              | 100 m                     | 200 m                      |
|                         | 0                         |                            |

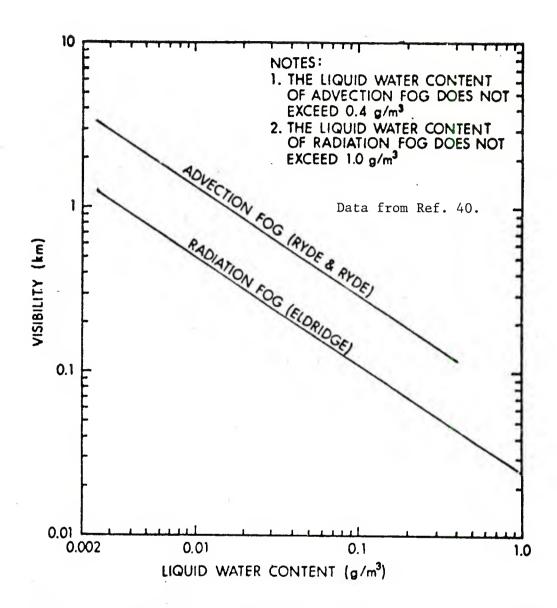


Fig. 13. Correlation of Visibility in Fog to Liquid Water Content

Ref. 40) for both advection and radiation fogs.

There is considerable variation in the water content of clouds and water fogs, but in general, stratus (or low) clouds and typical radiation or advection fogs have water contents on the order of 0.25 g/m $^3$  or less. Mason $^{41}$  reports that the maximum liquid water content of an advection fog approaches 0.4 g/m $^3$  when there is a strong temperature inversion. On rare occasions, the liquid water content can become as large as 0.5 to 1.0 g/m $^3$  in very dense radiation fogs (with 20 to 30 meters visibility).

The small size of water droplets comprising a fog allows the use of the Rayleigh approximations in the determination of the reflectivity and attenuation at 70 GHz. Atlas  $^{43}$  shows that in the Rayleigh scattering region the one-way attenuation coefficient,  $\alpha,$  is given by

$$\alpha = \frac{81.86 \text{ M Im}(-K)}{\lambda \rho} \text{ dB/km},$$

where M = 1 iquid water content per unit volume of fog in  $g/m^3$ , Im(-K) = absorption coefficient.

$$K = \frac{m^2 - 1}{m^2 + 2}$$

m = complex index of refraction,

 $\lambda$  = wavelength in mm,

 $\rho$  = density of water in g/cm<sup>3</sup>.

A density of 1  $g/cm^3$  for water is generally assumed for all temperatures, since the density varies no more than 0.78% over the 0°C to 40°C temperature range.

In the Rayleigh scattering region, attenuation is due mainly to absorption. To calculate the absorption coefficient for fog, the index of refraction for water must be determined for the frequencies of interest. The complex index of refraction, m, is given in terms of the complex dielectric constant,  $\epsilon_c$ , by:

$$m^2 = \varepsilon_c = \varepsilon_1 - j\varepsilon_2$$

where  $\epsilon$ , and  $\epsilon_2$  are the real and imaginary parts of the dielectric constant.

The dielectric constant may be evaluated by the Debye formula 37

$$\varepsilon_{c} = \frac{\varepsilon_{o} - \varepsilon_{\infty}}{1 + j \frac{\Delta \lambda}{\lambda}} + \varepsilon_{\infty},$$

where  $\boldsymbol{\epsilon}_{_{\mbox{O}}}$  ,  $\boldsymbol{\epsilon}_{_{\mbox{C}}}$  and  $\Delta\lambda$  are empirically derived constants.

Let us now look at some of the data currently available on millimeter and submillimeter wavelength attenuation in fog, clouds, and rain. Victor W. Richard, in Ref. 40, has given a good description of rain, fog and cloud data, from which a lot of this section's information is derived. A summary of the data from Richard 40 is presented in Figs. 14 and 15. Fig. 14 shows the positions of the atmospheric "windows", and the "walls". The profitable areas for further work in the millimetersubmillimeter region apparently should center around wavelengths of 94 GHz, 140 GHz, 240 GHz, 360 GHz, 420 GHz, and 890 GHz. Past 240 GHz, long-range communications do not appear to be practical; however, short range uses as missile guidance radar and imaging, target designators, and others, should be feasible. Fig. 15 is a comparison of the one-way attenuation due to a fog of 100 m visibility having a density of  $0.1 \text{ gm/m}^3$ with the one-way attenuation for 3 rain rates as a function of frequency. Fig. 16 (Ref. 40) shows in more detail the one-way attenuation of a fog as a function of frequency, temperature and liquid water content. A. R. Downs  $^{44}$  has calculated haze and fog attenuation coefficients for visible and IR radiation, as well as for microwaves with frequencies between 9.375 to 240 GHz. These data are shown on Table XV. Downs' article references 27 different papers on atmospheric transmission on rain, fog and battlefield dust conditions.

Dorothy Stewart  $^{45}$  in her extensive literature search on fogs and their drop sizes, has computed the extinction of visible. IR, and

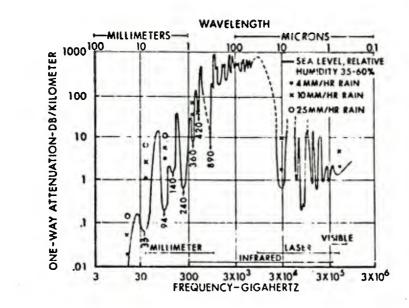


Fig. 14. Atmospheric Attenuation vs. Frequency (from Ref. 40)

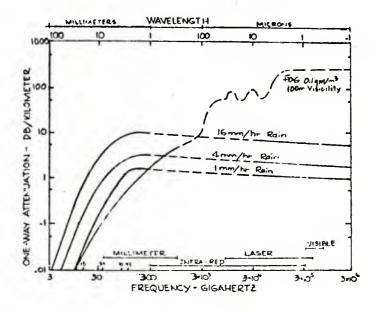


Fig. 15. Rain and Fog Attenuation vs. Frequency (from Ref. 40)

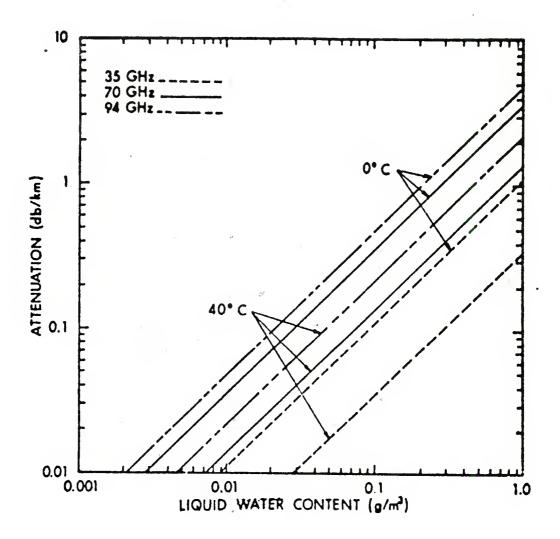
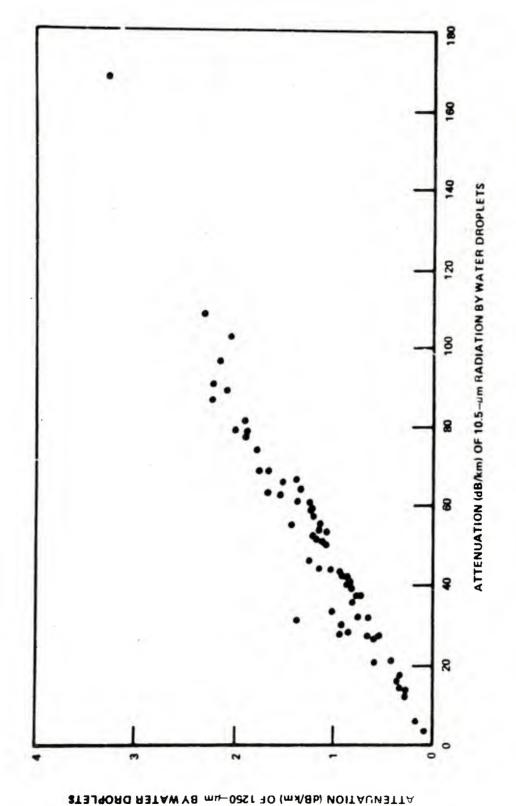


Fig. 16. One-Way Attenuation in Fog As a Function of Liquid Water Content (from Ref. 40)

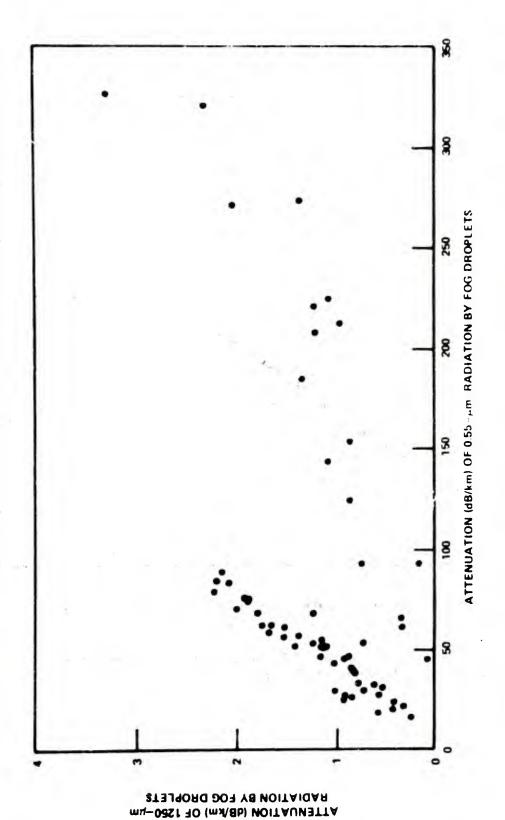
Haze and Fog Attenuation Coefficients as a Function of Visibility and Wavelength (from Ref. 44) Table XV.

1.4 g 10-1 2 10 x 3 3.2 4.4 # 10-2 FOG ATTEMATION CAEPFICIENTS (INC.) 1.6 # 10-2 9.275 8.0 x 10-6 9.4 x 10-2 1.7 x 10-1 6.7 x 10-2 3.1 x 10-1 1.3 x 10<sup>2</sup> 6.5 x 10° 1.7 x 10° 4.4 × 10° 1.2 x 10° 10.6 1 6.1 x 10-2 1.6 x 10-1 5.0 x 10-6 187 6.6 x 10<sup>-1</sup> 3.3 x 10-1 1.6 x 10° 7.1 x 10° 3.5 x 10° 4.0 x 10° 2.0 x 10° AMELENSTY (MICROICS) 3.7 x 10-5 8.3 x 10-2 4.2 x 10-1 2.1 x 10<sup>-1</sup> 1.5 x 10 8.7 × 10° .9 x 10° 3.8 x 10° 2.1 x 10° 4.4 x 10° 2.3 9.8 x 10-2 2.4 x 10<sup>-1</sup> 8.2 x 10-4 9.5 x 10-1 4.8 x 10-1 4.8 x 10° 2.2 x 10' 9.6 x 10° 2.2 x 10° 3.8 x 10° 1.2 x 10-2 9.5 x 10-2 4.8 x 10-1 2.4 x 19-1 9.5 x 10-1 4.8 x 10° 2.2 x 10° 2.2 x 10' 9.5 x 10° 3.8 x 10' 9.0 VISIBILITY (100) 2.0 5.0 10.0 8.0 9 326.0 0.2 <u>.</u>

submillimeter energy by fogs. Results of her calculations are shown in Figs. 17, 18, and 19. Fig. 17 shows a comparison of the attenuation of 1250  $\mu m$  and 10.5  $\mu m$  radiation by fog droplets; Fig. 18 shows a comparison of the attenuation of 1250  $\mu m$  and 0.55  $\mu m$  radiation by fog droplets; and Fig. 19 shows a comparison of the attenuation of 1250  $\mu m$  and 870  $\mu m$  radiation by fog droplets. We see from Fig. 18 that the visibility at .55  $\mu m$  is not necessarily a good indicator of 1250  $\mu m$  attenuation, but that the correlation of 10.6 and 1250  $\mu m$  attenuation is pretty good. Also, the correlation of attenuations of 870  $\mu m$  and 1250  $\mu m$  radiation is good.



Comparison of Attenuation of 1250- and 10.5-µm Radiation by Fog Droplets (from Ref. 45) Fig. 17.



Comparison of Attenuation of 1250- and 0.55-µm Radiation by Fog Droplets (from Ref. 45) Fig. 18.

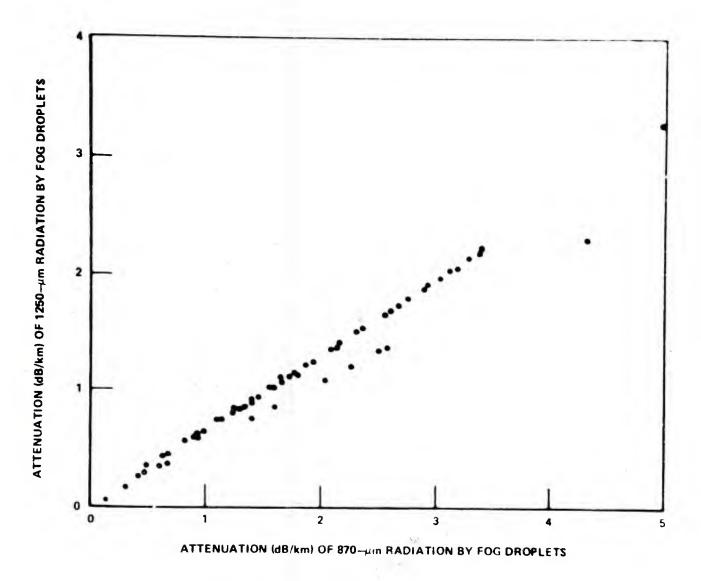


Fig. 19. Comparison of Attenuation of 1250- and 870- $\mu$ m Radiation by Fog Droplets. (data from Ref. 45)

Downs  $^{44}$  calculated the scattering coefficient for haze and fog at millimeter wavelengths and concluded that the scattering coefficient was between  $10^{-4}$  and  $10^{-5}$  (km $^{-1}$ ) which is at least 6 orders of magnitude below that of the scattering coefficients for haze and fogs at wavelengths of .55  $\mu$ m - 10.6  $\mu$ m.

- V. Corcoran 46 has calculated the fraction of the total attenuation along a zenith path through the atmosphere containing a 500-m thick stratocumulus cloud that results from the water droplets in the cloud and from the gaseous absorption along the total path. It is seen from Table XVI that the contribution to the attenuation by cloud droplets increases with an increase in the wavelength for wavelengths between 0.345 mm and 3 mm. Similarly the contribution to the attenuation by gaseous absorption increases with a decrease in wavelength. The attenuation resulting from gaseous absorption is seen in Table XVI to increase faster with decreasing wavelength than does the attenuation produced by the cloud droplets.
- D. Deirmendjian  $^{22}$  has calculated extinction coefficients according to 3 cloud models and 2 precipitation models; his results are shown in Fig. 20. His calculations were for wavelengths between 1.0  $\mu m$  to 100 mm. Tabulated values of this data are presented in Table XVII. Deirmendjian has also calculated a set of mass extinction coefficients for haze, clouds, and rain; this data are presented in Table XVIII for discrete wavelengths between 16  $\mu m$  to 2.0 mm.

Lo, Fannin and Straiton <sup>47</sup> have measured "the attenuation of 8.6 and 3.2 mm radio waves in clouds" by use of a millimeter wave radiometer. Results of their measurements are shown in Figs. 21, 22, and 23. Corrections were made to the measured data for the attenuation resulting from the atmosphere gaseous constituents to obtain estimates of the cloud attenuations. The correction for water vapor attenuation was based on ground-level water vapor density measurements. The sum was used as a source of millimeter wavelength radiation with the radiometer pointing at it through the clouds. Figure 21 presents 35 GHz (8.6 mm) attenuation vs 95 GHz (3.2 mm) attenuation for heavy pre-rain clouds. Figure 22 presents the total (zenith) attenuation due to cumulus clouds for 92

Table XVI. Proportion of Total Attenuation Due to a 500-m Strato-Cumulus Cloud in a Zenith Path (data from Ref. 46)

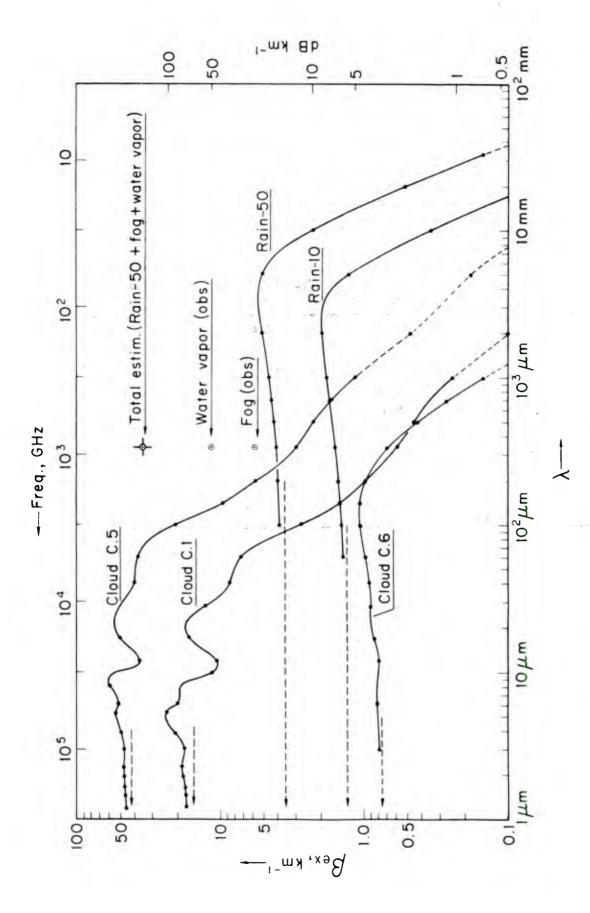
| Candidate windows |                  | Total                 | Contribution<br>by droplets   | Total<br>attenuation               | Proportion of total                  |
|-------------------|------------------|-----------------------|-------------------------------|------------------------------------|--------------------------------------|
| Window            | Wavelength λ     | gaseous<br>absorption | in a 500-meter<br>st-cu cloud | due to gases<br>and cloud droplets | attenuation due<br>to cloud droplets |
| 111               | 3mm              | 1.25 db               | 0.97 db                       | 2.22 db                            | 43.7%                                |
| IV                | 2.3mm            | 0.91 db               | 1.17 db                       | 2.08 db                            | 56.2%                                |
| ٧                 | 1.3mm            | 2.11 db               | 1.60 db                       | 3.71 db                            | 43.2%                                |
| VI                | 480 <sub>µ</sub> | 9.87 db               | 2.40 db                       | 12.27 db                           | 19.6%                                |
| 117               | 720 µ            | 22.0 db               | 2,92 db                       | 24.92 db                           | 11.7%                                |
| 1 X               | 620 u            | 57.0 db               | 3.00 db                       | 60,0 db                            | 5.0%                                 |
| XII               | 345µ             | 77.0 db               | 5,50 db                       | 82.5 db                            | 6.7%                                 |

Table XVII. Cloud Volume Extinction and Absorption Coefficients (data from Ref. 22)

 $(Neper km^{-1})$ 

|                | Cloud C.1 ( | $N = 10^2 cm^{-3}$ | Cloud C.5 | $(N = 10^2 cm^{-3})$ | Cloud C.6 (N | $I = 10^{-1} \text{cm}^{-3}$ |
|----------------|-------------|--------------------|-----------|----------------------|--------------|------------------------------|
| λ              | βex         | β <sub>ab</sub>    | βex       | βab                  | βex          | β<br>ab                      |
| (λ <b>→</b> 0) | (15.64)     |                    | (42.41)   |                      | (0.7540)     |                              |
| 12.µm          | 10.28       | 7.352              | 36.32     | 22.61                | 0.7933       | 0.4030                       |
| 17.μm          | 16.12       | 10.23              | 49.98*    | 28.49*               | 0.8500*      | 0.4113*                      |
| 28.µm          | 12.33       | 7.849              | 49.88     | 27.36                | 0.9004       | 0.4521                       |
| 40. բառ        | 8.468       | 6.392              | 39.86     | 24.89                | 0.9250       | 0.4774                       |
| 60.µm          | 7.013       | 5.816              | 37.69     | 25.41                | 0.9742       | 0.5065                       |
| 100.µm         | 2.690       | 2.415              | 20.70     | 14.55                | 1.061        | 0.553                        |
| 140.µm         | 1.420       | 1.352              | 9.742     | 7.797                | 1.074        | 0.555                        |
| 200,µm         | 0.9732      | 0.9570             | 5.617     | 5.109                | 0.9774       | 0.5190                       |
| 337.µm         | 0.5812      | 0.5789             | 2.949     | 2.880                | 0.6845       | 0.4016                       |
| 500.µm         | 0.4566      | 0.4560             | 2.235     | 2.219                | 0.4186       | 0.2911                       |
| 700.µm         | 0.3474      | 0.3472             | 1.676     | 1.671                | 0.2563       | 0.2031                       |
| 1000.µm        |             | (0.2423)           | 1.165     | 1.164                | 0.1440       | 0.1274                       |
| 2.mm           |             | (0.0999)           |           | (0.474)              |              | (0.0401)                     |
| 5.mm           |             | (0.0381)           |           | (0.181)              |              | (0.0153)                     |
| 10.mm          |             | (0.0119)           |           | (0.0563)             |              | (0.0048)                     |

<sup>\*</sup>Values from an earlier run with m = 1.369 - 0.438i.



Theoretical Extinction Coefficients According to Three Cloud Models and two Precipitation Models (data from Ref. 22) Fig. 20.

Table XVIII. Mass Extinction Coefficients for Haze, Clouds, and Rain (data from Ref. 22)

 $(\gamma_{\rm ex} \ {\rm in \ neper} \ {\rm km}^{-1} \ {\rm per} \ {\rm g} \ {\rm m}^{-3} \ {\rm liquid \ water \ content})$ 

|                     | Haze L                                     | Cloud C.1                      | Cloud C.5                     | Rain-10                       |
|---------------------|--------------------------------------------|--------------------------------|-------------------------------|-------------------------------|
| λ                   | $w = 1.167 \cdot 10^{-5} \text{ g m}^{-3}$ | $w = 0.06255 \text{ g m}^{-3}$ | $w = 0.2969 \text{ g m}^{-3}$ | $w = 0.5091 \text{ g m}^{-3}$ |
| (λ <b>→</b> 0)      | (3117.)                                    | (250.1)                        | (142.8)                       | (2.573)                       |
| 16.6µm              | 247.6                                      |                                |                               |                               |
| 17.0µm              |                                            | 257.8                          | 168.3                         |                               |
| 100. $\mu m$        | (36.8)                                     | 43.01                          | 69.72                         | 2.816                         |
| 200.µm              | (16.8)                                     | 15.56                          | 18.92                         | 2.950                         |
| $337.\mu\text{m} -$ | (10.5)                                     | 9.293                          | 9.932                         | 3.097                         |
| 500.µm              | (7.21)                                     | 7.301                          | 7.527                         | 3.243                         |
| 1.mm                | (3.87)                                     | (2.07)                         |                               |                               |
|                     | , ,                                        | (3.87)                         | 3.924                         | 3.580                         |
| 2,mm                | (1.60)                                     | (1.60)                         | (1.60)                        | 3.830                         |

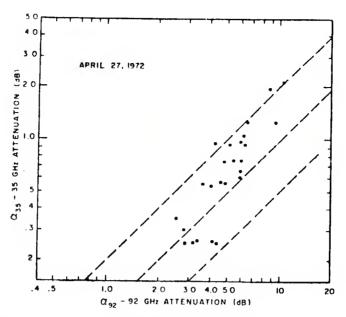


Fig. 21. 35 GHz Attenuation versus 95 GHz Attenuation for Heavy Prerain Clouds (data from Ref. 47)

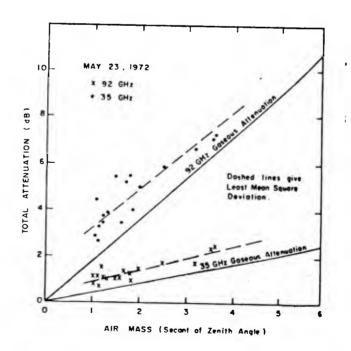


Fig. 22. Effect of Cumulus Clouds on Attenuation (data from Ref. 47)

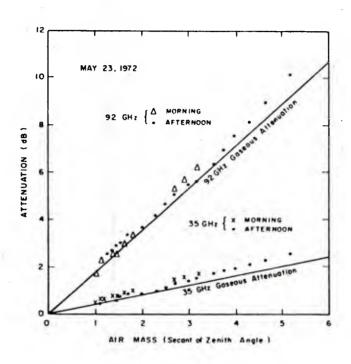


Fig. 23. Attenuation of General Overcast versus Air Mass for 35 GHz and 92 GHz (data from Ref. 47)

and 35 GHz radiation. Figure 23 shows the attenuation effects of an overcast sky versus air mass (secant of zenith angle) for 35 GHz and 92 GHz radiation.

As a function of cloud type,  ${\rm Lo}^{47}$  et al. have summarized their measurements in two tables: the first, presented here as Table XIX gives the attenuation in db, for 35 and 95 GHz radiation, due to individual fair-weather cumulus clouds. In Table XX is a summary of zenith cloud attenuation for 35 and 95 GHz radiation by different cloud types.

Corcoran  $^{46}$  has calculated data on the attenuation due to moderate rain of a 2-km depth (zenith path through a 500 m thick strato cumulus cloud). His data for attenuation of radiation with wavelengths in the atmosphere windows between 345  $\mu m$  to 3 mm are given in Table XXI.

There is a vast literature on the scattering and attenuation of millimeter and submillimeter radiation by rain. Before we get into the data and calcualtions that were found relevant, let us discuss some of the currently used size distributions for rain droplets. D. Deirmendjian 22 introduced a general raindrop sized distribution,

$$n(r) = ar^{\alpha} \exp(-br^{\gamma})$$

to model both clouds, hazes and raindrops. The parameters a,  $\alpha$ , b,  $\gamma$  are positive, real numbers that may be related to measurable parameters. For  $\gamma$  = 1,

$$\int\limits_{0}^{\infty} n(r)dr = N = \text{total number of particles per unit volume}$$

in the distribution. This gives

$$a = \frac{Nb^{\alpha+1}}{\Gamma(\alpha+1)} .$$

Some other properties of Deirmendjian's distribution are that there is only one peak in the distribution, there is exponential decay in the number density in both increasing drop size and a cut-off on decreasing drop size.

Table XIX. Attenuation due to Individual Fair Weather Cumulus Clouds (from Ref. 47)

| Cloud Atten | uation, dB | 95 GHz Attenuation |  |  |
|-------------|------------|--------------------|--|--|
| 15 GHz      | 95 GHz     | 35 GHz Attenuation |  |  |
| 0.16        | 0.88       | 5.5                |  |  |
| 0.04        | 0.18       | 4.5                |  |  |
| 0.12        | 0.65       | 5.4                |  |  |
| 0.06        | 0.22       | 3. 7               |  |  |
| 0.09        | 0.36       | 4.0                |  |  |
| 0.16        | 0.48       | 3.0                |  |  |
| 0.04        | 0.16       | 4.0                |  |  |
| 0.06        | 0.22       | 3.7                |  |  |

Table XX. Summary of Zenith Cloud Attenuation for Different Cloud Types (from Ref. 47)

| Cloud Type    | Number<br>of<br>Days | Total<br>Number<br>of<br>Observations | Ground Level<br>Water Vapor Density |                                           | 35 GHz Value in dB/95 GHz Value in dB |                                     |                      |                                              |
|---------------|----------------------|---------------------------------------|-------------------------------------|-------------------------------------------|---------------------------------------|-------------------------------------|----------------------|----------------------------------------------|
|               |                      |                                       |                                     | g/m <sup>3</sup><br>Standard<br>Deviation | Measured C<br>Mean                    | loud Attenuation Standard Deviation | Calculated (<br>Mean | Gaveous Attenuation<br>Standard<br>Deviation |
| Altocumulus   | 5                    | 7                                     | 16.8                                | 1.43                                      | .02/23                                | .09/.30                             | . 38/1. 93           | .02/,14                                      |
| Altostratus   | 2                    | 2                                     | 14.7                                | 1.53                                      | ,15/.30                               | .04/.05                             | , 34/1.73            | .03/.16                                      |
| Stratocumulus | 8                    | 22                                    | 18.9                                | 1,68                                      | .18/.61                               | .13/.41                             | . 43/2.14            | .03/.15                                      |
| Stratus       | 5                    | 8                                     | 19.1                                | 2.30                                      | .13/.12                               | .03/.24                             | .42/2.14             | .04/.21                                      |
| Nimbostratus  | 2                    | 5                                     | 20.8                                | 0.31                                      | .14/.11                               | ,06/.24                             | . 44/2. 32           | .01/.03                                      |
| Cumulus       | 13                   | 20                                    | 18.7                                | 1.81                                      | .12/.34                               | .14/.36                             | .41/2.12             | .03/.18                                      |
| Cumulonimbus  | 2                    | 6                                     | 18.1                                | 2.39                                      | . 34/2. 36                            | .22/1.86                            | .40/2.07             | .04/.23                                      |

Table XXI. Proportion of Total Attenuation due to Moderate Rain of 2-KM Depth (Zenith Path Through 500-M Strato-Cumulus Cloud) (data from Ref. 46)

| Candidate windows |                    | Total gaseous absorption plus contribution to | Contribution<br>by             | Total attenuation due to | Proportion of total                |
|-------------------|--------------------|-----------------------------------------------|--------------------------------|--------------------------|------------------------------------|
| Window            | Wavelength         | attenuation by 500-<br>meter st-cu cloud      | moderate rain<br>of 2 km depth | gases, cloud<br>and rain | attenuation<br>due to<br>2 km rain |
| 111               | 3 m m              | 2.22 db                                       | 5.2 db                         | 7.42 db                  | 70%                                |
| I V               | 2.3mm              | 2.08 db                                       | 2.5 db                         | 4.58 db                  | 55%                                |
| ٧                 | 1.3mm <sup>a</sup> | 3.71 db                                       | 2.5 db                         | 6.21 db                  | 40%                                |
| VI                | 880µª              | 12.27 db                                      | 2.4 db                         | 14.67 db                 | 16%                                |
| All               | 720µª              | 24.92 db                                      | 2.3 db                         | 27,22 db                 | 8%                                 |
| X 1               | 620µª              | 60.0 db                                       | (2.2) db                       | (62.2) db                | (3.5)                              |
| XII               | 345µª              | 82.5 db                                       | (2.0) db                       | (84.5) db                | (2.3)                              |

 $^{\rm a}\,\text{No}$  allowance made at these wavelengths for possible reduction in attenuation due to moderate rain by the mechanism of forward scatter.

Note: Values in parentheses are extrapolated.

Other prominently used drop-size distributions are those attributed to Laws and Parson  $^{49}$ , Marshall and Palmer  $^{50}$  and Best. These distributions are illustrated by the following tables and graphs. Table XXII shows, for the Laws and Parson drop-size distribution, the percent of the total of water versus the particle size for 5 different rain rates. Similar data for the Marshall and Palmer distribution are shown in Table XXIII. The data in Tables XXIII and XXIII were obtained from a paper by Wilcox and Graziano. Figure 24 shows data based on the Best model that gives the drop radius concentration as a function of droplet radius for rainfall rates of 1, 4, 16, and 64 mm/hr. The Best model describes the fraction of the total liquid water contained in the water drops which have diameters less than x (mm) for a given rainfall rate R (mm/hr). The Best model is defined by:

$$F(x) = 1-\exp[-(x/a)^{n}],$$
where 
$$a = AxR^{p}.$$

The total liquid water content expressed in  $mm^3/m^3$  is

$$w = CxR^r$$

A = 1.3, c = 60, p = 0.232, r = 0.846, and n = 2.25. Downs  $^{44}$  felt that the Best distribution most accurately describes the 70 GHz scattering data for rain. He calculated a rain scattering coefficient as a function of rainfall rate (or visibility) for visible light, IR, microwaves and millimeter wave radiation. Downs used the Laws and Parson's drop radius distribution in calculating the microwave and millimeter wave rain scattering coefficients. Downs' results are depicted in Tables XXIV and XXV. Table XXIV gives the rain scattering coefficient in km  $^{-1}$  vs visibility (or rainfall rate) for visible through 10.6  $\mu$ m radiation, and Table XXV gives the rain scattering coefficient per km vs rainfall rate for frequencies of 9.375 GHz through 240 GHz. Absorption coefficients in rain for 9.375 GHz to 240 GHz radiation were calculated by Setzer;  $^{53}$  his results are shown here as Table XXXVI.

Table XXII. Laws and Parsons Drop Size Distributions (data from Ref. 52)

| !     |      | Rta   | in rate (mm/    | hr)   |      |
|-------|------|-------|-----------------|-------|------|
|       | 1.25 | 2.5   | 5               | 25    | 100  |
| D(mm) |      | Perce | ent of total vo | lume  |      |
| 0.5   | 10.9 | 7.3   | 4.7             | 1.7   | 1    |
| 1     | 37.1 | 27.8  | 20.3            | 7.6   | 4.6  |
| 1.5   | 31.3 | 32.8  | 31.0            | 18, 4 | 8.8  |
| 2     | 13.5 | 19    | 22.2            | 23, 9 | 13.9 |
| 2.5   | 4.9  | 7.9   | 11.8            | 19.9  | 17.1 |
| 3     | 1.5  | 3.3   | 5.7             | 12.8  | 8.4  |
| 3.5   | 0.6  | 1.1   | 2.5             | 8.2   | 15   |
| 4     | 0.2  | 0.6   | 1               | 3, 5  | 9    |
| 4.5   |      | 0.2   | 0.5             | 2.1   | 5.8  |
| 5     |      |       | 0.3             | 1. 1  | 3    |
| 5.5   |      |       |                 | 0.5   | 1.7  |
| 6     |      |       |                 | 0.3   | 1    |
| 6.5   |      |       |                 |       | 0.7  |

Table XXIII. Marshall and Palmer Drop Size Distribution (data from Ref. 52)

|       |      | Rai  | n rate (mm/h    | r)    |      |
|-------|------|------|-----------------|-------|------|
|       | 1.25 | 2.5  | 5.0             | 25    | 100  |
| D(mm) |      | Perc | ent of total ve | olume |      |
| 0.5   | 85.9 | 81.6 | 76.6            | 65.0  | 54.3 |
| 1     | 12.1 | 15.0 | 17.8            | 22.9  | 24.8 |
| 1.5   | 1.7  | 2.8  | 4.3             | 7.9   | 11.5 |
| 2     | 0.3  | 0.5  | 1               | 2.8   | 5.2  |
| 2.5   |      | 0.1  | 0.3             | 1     | 2.4  |
| 3     |      |      |                 | 0.4   | 1.1  |
| 3.5   |      |      |                 | 1     | 0.5  |
| 4     |      | }    |                 |       | 0.2  |
| 4.5   |      |      |                 |       |      |
| 5     |      |      |                 |       | 1    |

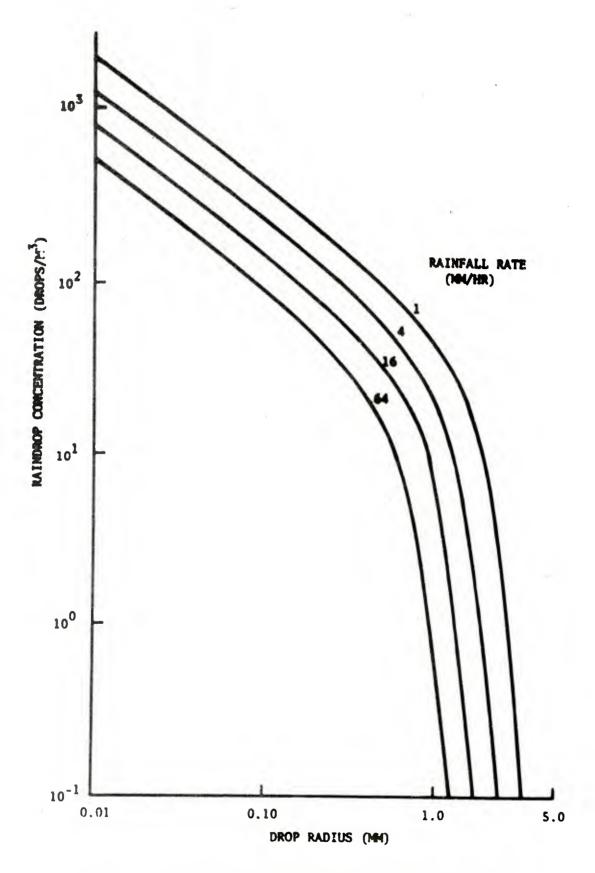


Fig. 24. Best Model for Drop Radius Distribution as a Function of Rainfall Rate (from data in Ref. 52)

Table XXIV. Scattering Coefficient for Rain as a Function of Rain Rate (or Visibility) for Wavelengths of 0.55, 1.06, 2.3, 3.8 and  $10.6~\mu m$  (Data from Ref. 44)

| MADIFALL                                | RAIN  | SCATTERIN | COEFFICIE   | WT (10( <sup>-1</sup> ) |       | VISI-  |
|-----------------------------------------|-------|-----------|-------------|-------------------------|-------|--------|
| MATE (MOVINE)                           |       | MAYELE    | ICEH (MICHO | NS)                     |       | DELETY |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 0.55  | 1.06      | 2.5         | 3.8                     | 10.6  | (180)  |
| 1                                       | 0.245 | 0.245     | 0.246       | 0.246                   | 0.249 | 16.0   |
| 2                                       | 0.376 | 0.376     | 0.376       | 0.377                   | 0.381 | 10.4   |
| 4                                       | 0.576 | 0.576     | 0.576       | 0.577                   | 0.582 | 6.8    |
| 8                                       | 0.882 | 0.882     | 0.882       | 0.883                   | 0.890 | 4.4    |
| 16                                      | 1.35  | 1.35      | 1.35        | 1.35                    | 1.36  | 2.9    |
| 32                                      | 2.07  | 2.07      | 2.07        | 2.07                    | 2.07  | 1.9    |
| 64                                      | 3.17  | 3.17      | 3.17        | 3.17                    | 3.18  | 1.2    |

Table XXV. Scattering Coefficient for Rain as a Function of Rain Rate for Frequencies of 9.375, 35, 94, 140 and 240 GHz (Data form Ref. 44)

| RAINFALL        |                      | RAIN SCATTE          | RING COEFF           | ICIENT (IOC          | 1)                   |
|-----------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| RATE<br>(MM/HR) |                      |                      | REQUESTRY (          |                      |                      |
| (M-712K)        | 9.375                | 35                   | 94                   | 140                  | 240                  |
| 1               | 6.0x10 <sup>-5</sup> | 1.7x10 <sup>-2</sup> | 1.4x10 <sup>-1</sup> | 1.6x10 <sup>-1</sup> | 1.6x10 <sup>-1</sup> |
| 2               | 1.7x10 <sup>-4</sup> | 4.0x10 <sup>-2</sup> | 2.3x10 <sup>-1</sup> | 2.4x10 <sup>-1</sup> | 2.4x10 <sup>-1</sup> |
| 4               | 4.7x10 <sup>-4</sup> | 8.5x10 <sup>-2</sup> | 3.7x10 <sup>-1</sup> | 3.8x10-1             | 3.8x10 <sup>-1</sup> |
| 8               | 1.4x10 <sup>-3</sup> | 1.8x10 <sup>-1</sup> | 6.4x10-1             | 6.4x10 <sup>-1</sup> | 6.4x10 <sup>-1</sup> |
| 16              | 4.0x10 <sup>-3</sup> | 4.0x10"1             | 1.1x10 <sup>0</sup>  | 1.1x10 <sup>0</sup>  | 1.1x10 <sup>0</sup>  |
| 32              | 1.2x10 <sup>-2</sup> | 8.2x10 <sup>-1</sup> | 1.8x10 <sup>0</sup>  | 1.8x10 <sup>0</sup>  | 1.8x10 <sup>0</sup>  |
| 64              | 3.2x10 <sup>-2</sup> | 1.7x10 <sup>0</sup>  | 2.9x10 <sup>0</sup>  | 2.9x10 <sup>0</sup>  | 2.9x10 <sup>0</sup>  |

Table XXVI. Absorption Coefficient for Rain as a Function of Rain Rate for Frequencies of 9.375, 35, 94, 140 and 240 GHz (data from Ref. 53)

| MAINFALL         |                      | MAIN ABSORPTION      | ON COEFFICIEN        | n (104 <sup>-1</sup> ) | -                   |
|------------------|----------------------|----------------------|----------------------|------------------------|---------------------|
| MATE<br>(HOLVER) |                      | PREQ                 | MINCY (GHz)          |                        |                     |
|                  | 9.378                | 35                   | 94                   | 140                    | 240                 |
| 1                | 2.0x10 <sup>-3</sup> | 4.5x10 <sup>-2</sup> | 1.2x10 <sup>-1</sup> | 1.4x10 <sup>-1</sup>   | 1.4x10              |
| 2                | 4.8x10-3             | 8.7x10 <sup>-2</sup> | 2.6x10 <sup>-1</sup> | 2.3x10 <sup>-1</sup>   | 2.3x10              |
| 4                | 1.2x10 <sup>-2</sup> | 1.6x10 <sup>-1</sup> | 3.3x10 <sup>-1</sup> | 3.7x10 <sup>-1</sup>   | 5.7x10              |
| 8                | 2.9x10 <sup>-2</sup> | 3.0x10 <sup>-1</sup> | 5.4x10 <sup>-1</sup> | 6.2x10 <sup>-1</sup>   | 6.2x10              |
| 16               | 6.5x10 <sup>-2</sup> | 5.6x10 <sup>-1</sup> | 8.7x10 <sup>-1</sup> | 1.0x10 <sup>0</sup>    | 1.0x10 <sup>0</sup> |
| 32               | 1.6x10-1             | 1.0x100              | 1.5x100              | 1.7x100                | 1.7x10 <sup>0</sup> |
| 64               | 3.8x10 <sup>-1</sup> | 1.8x10 <sup>0</sup>  | 2.3x100              | 2.6x100                | 2.6x10 <sup>0</sup> |

- D. C. Hogg's<sup>54</sup> measured data on the one-way attenuation due to rain at 70 GHz and some theoretical data by Crane<sup>26</sup> and SRI<sup>40</sup> are presented in Fig. 25. Crane<sup>26</sup> calculated the one-way attenuation in rain vs rainfall rate and showed that the Laws and Parson's model fits Hogg's data best; Crane's data are for frequencies of 15.5, 35, 70, and 94 GHz. V. Richard<sup>40</sup> compiled this set of Crane's data, and his compilation is shown in Fig. 26.
- D. Deirmendjian's  $^{22}$  calculations of the extinction coefficient resulting from rainfall are given in Fig. 20, where the extinction coefficient  $\beta_{\rm ext},~{\rm km}^{-1}$  vs wavelength is shown for 3 cloud models and 2 rainfall models. The wavelength coverage is from 1.0  $\mu m$  to 100 mm.

Downs<sup>44</sup> has combined the scattering and absorption tables for visible, IR, microwave and millimeter wave radiation, and his results, giving the rainfall attenuation coefficients vs rainfall rate, are presented in Table XXVII.

Wilcox and Graziano  $^{27}$  calculated the combined atmospheric attenuation by water vapor ( $\alpha_w$ (vapor)), oxygen ( $\alpha_o$ ), and rain ( $\alpha_w$ (cond)). They plotted the total attenuation (db/km) vs rainfall rate for radiation of wavelength 3, 4, 8, and 10 mm, for rainfall rates of 0.1 mm/hr to 100 mm per hour. Their results are presented in Fig. 27.

Crane 26 has calculated the rain backscatter cross section per unit volume of rain at 0°C vs rainfall rate for 15.5, 35, 70, and 94 GHz, using the Mie scattering theory. His data are presented in Fig. 28. (Downs 40 collected Crane's curves and produced the composite curve presented here as Fig. 28.) Victor Richard and John Kammerer 55 of BRL have collected data from measurements and calculations of the radar backscatter cross section per unit volume for 9.375, 35, 70 and 95 GHz frequencies. These data are plotted as a function of rain rate, from 0.1 mm/hr to 100 mm/hr in Figs. 29, 30, 31, and 32. Figure 29 presents BRL's measured data of backscatter cross section vs rain rate for the 4 frequencies mentioned. Figure 30 presents BRL's 35 GHz backscatter cross section vs rain rate as well as a number of other calculations and measurements. Figure 31 presents BRL's 70 GHz data and a collection of other calculations and

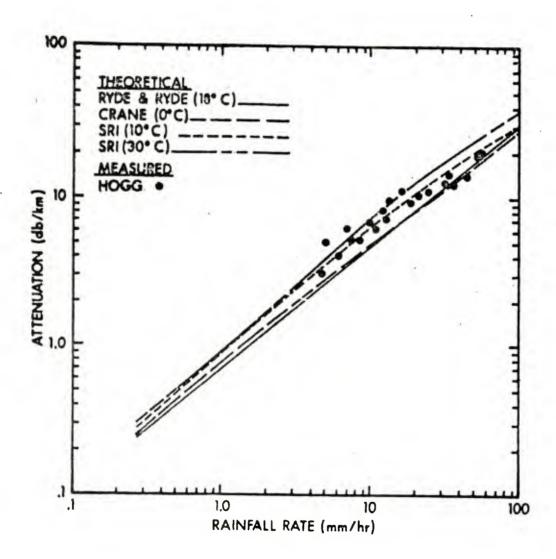


Fig. 25. Comparison of Theoretical and Measured Data on One-Way Attenuation in Rain at 70 GHz (data from Refs. 26, 40 and 54)

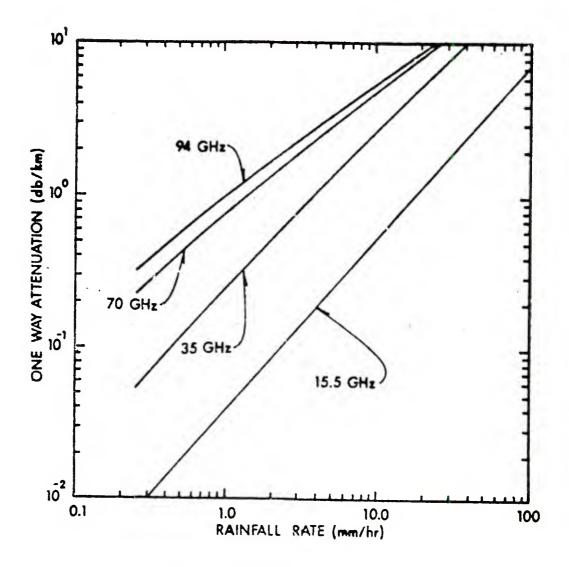


Fig. 26. One-Way Attenuation in Rain vs Rainfall Rate for Frequencies of 15.5, 35, 70 and 94 GHz (Data from Refs. 26 and 40)

Attenuation Coefficient for Rain as a Function of Rainfall Rate (Data from Ref. 44) Table XXVII.

|          |                        |                        |                  | -         | MAIN ATTENNATION COUFFICIENT (NC <sup>1</sup> ) | COEFICIENT (1          | هد،)                   |                        |                        |            |
|----------|------------------------|------------------------|------------------|-----------|-------------------------------------------------|------------------------|------------------------|------------------------|------------------------|------------|
| PATERIT  |                        |                        | MELENETH (NECHOR | ()        |                                                 |                        |                        | FREQUENCY (SEC)        |                        |            |
| <u> </u> | 0.56                   | 1.66                   | 2.3              | 3.8       | 10.6                                            | 9.378                  | ×                      | *                      | 140                    | 240        |
| -        | 2.4 x 10 <sup>-1</sup> | 2.5 x 10 <sup>-1</sup> | 3.0 x 16"        | 3.1 x 16" | 3.2 x 10-1                                      | 2.1 x 16 <sup>-3</sup> | 6.3 x 10 <sup>-2</sup> | 2.6 x 10 <sup>-1</sup> | 3.6 x 10-1             | 3.0 × 10-1 |
| ~        | 3.8 x 10-1             | 3.9 x 10 <sup>-1</sup> | 4.6 x 10"        | 4.7 x 16" | 4.8 x 10"                                       | 8.0 x 10-3             | 1.3 x 10-1             | 4.6 x 10-1             | 4.7 x 10-1             | 4.7 × 10-1 |
| •        | 5.8 x 10-1             | 6.9 x 10-1             | 7.6 x 16"        | 7.2 x 16" | 7.4 x 16"                                       | 1.2 x 10-2             | 2.4 x 10-1             | 7.0 x 10-1             | 7.5 x 10 <sup>-1</sup> | 7.5 x 10-1 |
| •        | 8.8 x 10-1             | 9.2 x 10 <sup>-1</sup> | 1.1 x 10         | 1.1 x 10° | 1.1 x 10                                        | 3.0 x 10-2             | 4.8 x 10-1             | 1.2 x 10°              | 1.3 x 10°              | 1.3 x 10°  |
| 36       | 1.4 x 10°              | 1.4 x 10°              | 1.7 a 10°        | 1.7 x 10° | 1.7 x 10°                                       | 6.9 x 10-2             | 9.6 x 10-1             | 2.0 x 10°              | 2.1 x 10°              | 2.1 x 10°  |
| ×        | 2.1 x 10°              | 2.2 x 19°              | 2.6 x 10°        | 2.6 x 10° | 2.7 x 10°                                       | 1.7 x 10-2             | 1.8 x 10°              | 3.3 x 10°              | 3.6 x 10°              | 3.6 × 10°  |
| 3        | 3.2 x 10°              | 3.4 x 10°              | 4.0 x 10         | 4.6 x 10° | 4.1 x 10°                                       | 4.1 x 10-1             | 3.6 x 10°              | 5.2 x 10°              | 5.5 x 10°              | 6.6 x 10°  |

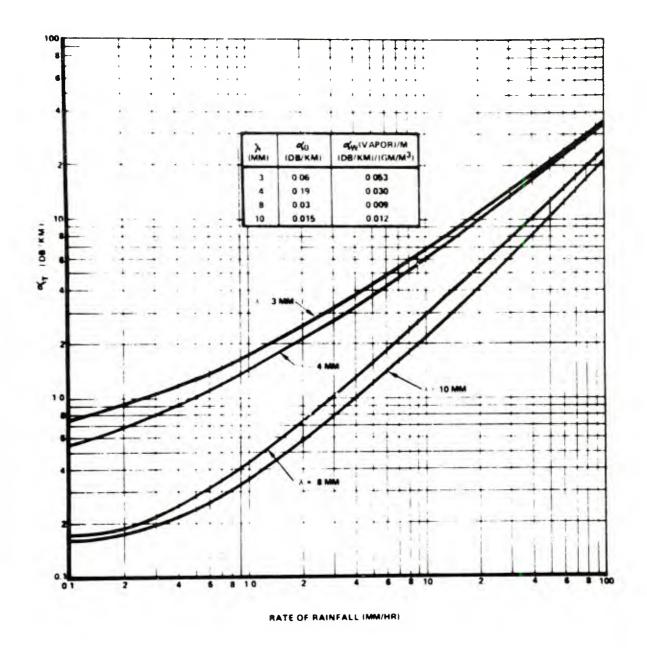


Fig. 27. Combined Atmospheric Attenuation Caused by Water Vapor ( $\alpha_{_{_{\hspace{-.05cm}W}}}$  (Vapor)), Oxygen ( $\alpha_{_{_{\hspace{-.05cm}O}}}$ ), and Rain ( $\alpha_{_{_{\hspace{-.05cm}W}}}$  (Cond)) as a Function of the Rate of Rainfall for Wavelengths of 3, 4, 8 and 10 mm (Data from Ref. 27)

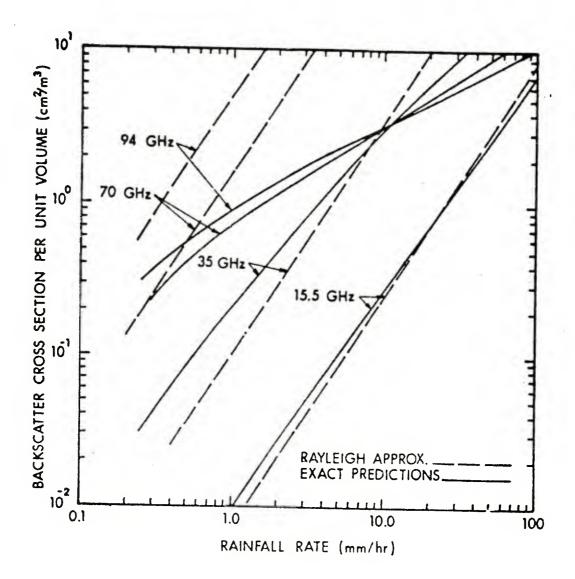
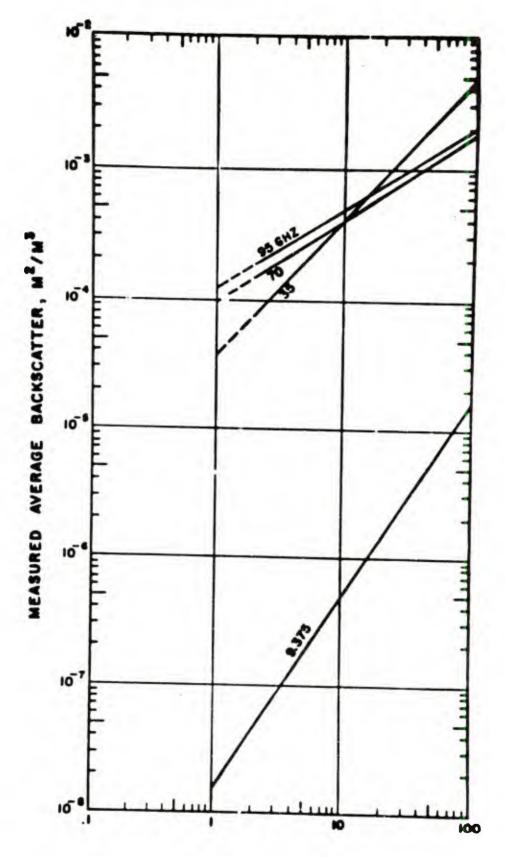


Fig. 28. Backscatter Cross Section per Unit Volume of Rain at 0°C versus Rainfall Rate for 15.5, 35, 70 and 94 GHz Radiation (Data from Refs. 26 and 40)



RAIN RATE (mm/hr)

Fig. 29. Measured Backscatter Cross Section for Rain vs Rain Rate for Frequencies of 9.375, 35, 70 and 95 GHz (Data from Ref. 55)

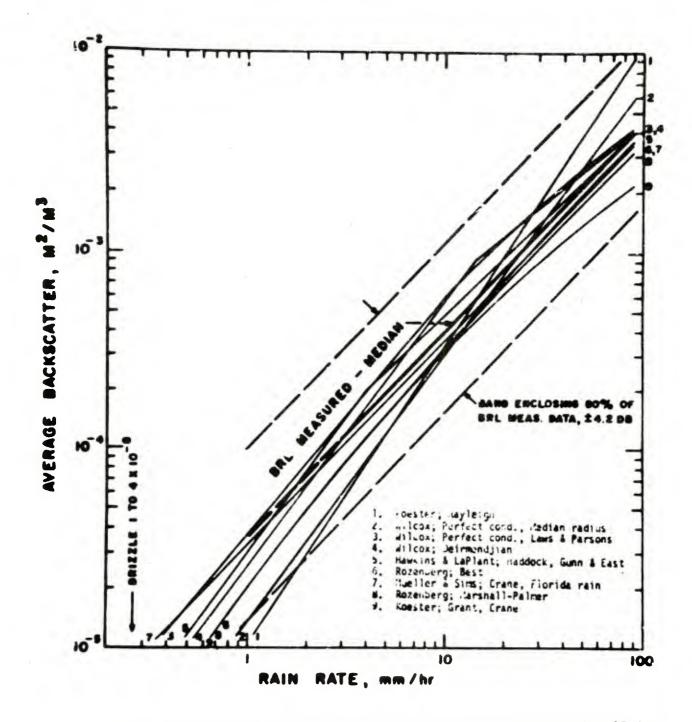


Fig. 30. Measured and Calculated Backscatter Cross Section for 35 GHz Radiation in Rain as a Function of Rain Rate (Data from Ref. 55)

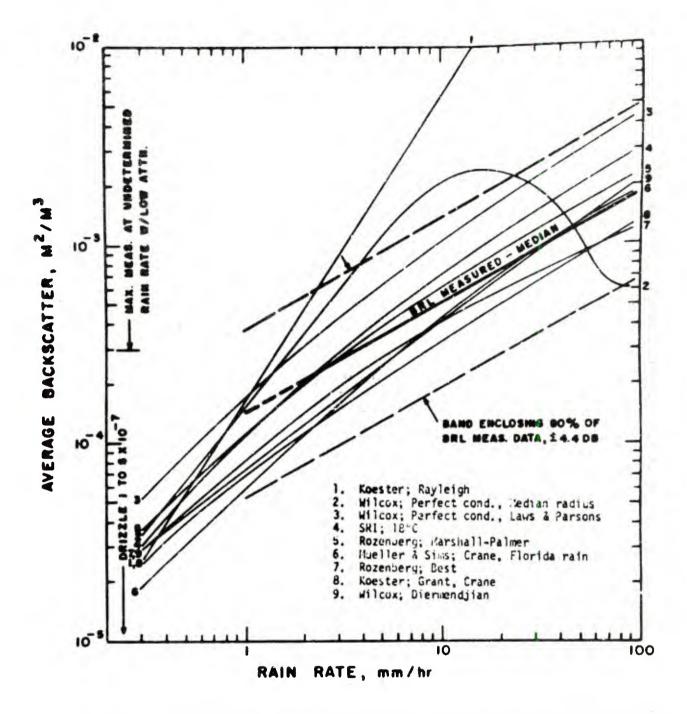


Fig. 31. Measured and Calculated Backscatter Cross Section for 70 GHz Radiation in Rain as a Function of Rain Rate (Data from Ref. 55)

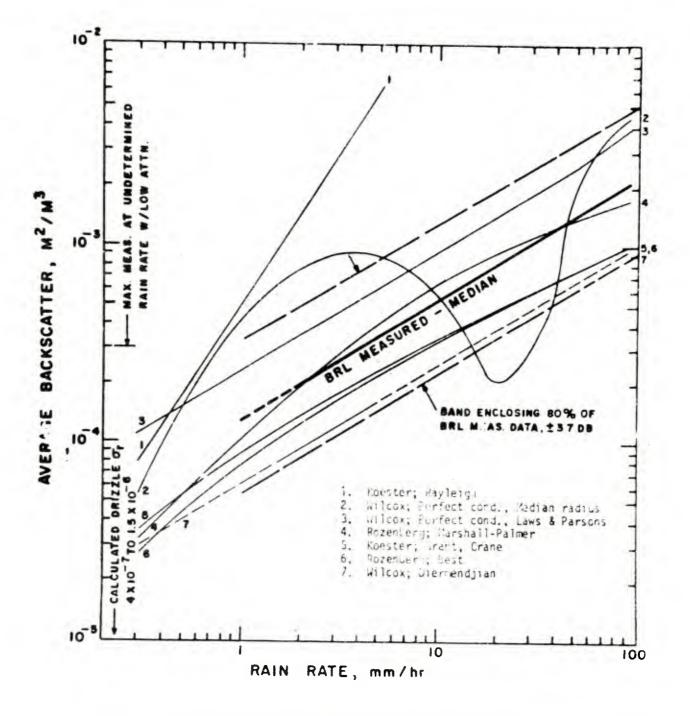


Fig. 32. Measured and Calculated Rain Backscatter Cross Section for 95 GHz Radiation in Rain as a Function of Rain Rate (Data from Ref. 55)

measurements which were referred to in their article. Figure 32 presents BRL's 95 GHz data along with other calculations and measurements. The reader is referred to Ref. 55 for further details on these curves.

A. V. Sokolov  $^{56}$  computed the attenuation in rain, in dB/km vs intensity of rainfall, 1-100 mm/hr, for visible, IR, and microwave frequencies, for .63  $\mu m$  - 8 mm, using Mie theory, where applicable, and Best's drop-size distribution. His results are shown in Table XXVIII.

Serge Godard<sup>57</sup> measured the reflectivity of rain drops as a function of drop radius for radiation of .86 cm, 3.21 cm, 5.5 cm, and 10 cm wavelength. His data on rain-drop reflections are shown here in Fig. 33. He also found that for 0.86 cm waves, the attenuation in rain is really independent of the drop-size distribution; even though the reflectivity is very much a function of drop diameter.

Malinkin, Sokolov, and Sukkonen measured the attenuation coefficient in dB/km for 8.6 mm radiation, and computed the attenuation for 1, 2, 4 and 8.6 mm radiation. The results of their calculations are shown in Fig. 34. Figure 35 shows more details of their measured and calculational data on the attenuation coefficient at  $\lambda$ =8.6 mm as a function of rainfall rate.

Sokolov and Sukkonen<sup>59</sup> computed the attenuation of radio-waves in the 0.1-2mm range using the drop-size distributions of both Best and Polyakova. For rain rate less than 10-12 mm/hr, using Mie theory, the computations were in agreement with experimental data at 0.96 mm. The results of their theoretical calculations are shown in Table XXIX.

Bakin. Zimin et al. 60 measured the attenuation in rain of radio-waves of 0.96 mm. The results of their measurements are shown in Fig. 36. They found that compared to radiation of 8.6 mm, the attenuation at 0.96 mm is larger roughly by a factor of 2.5 to 3.0. Table XXX tabulates their data (average values) with some of Medhurst 61 at 0.96, 4.3, 6.2, 8.6 and 9.6 mm for rainfall intensity of 5 and 12 mm/hr.

In 1970, V. I. Rozenberg  $^{62}$  performed a critical review of radar characteristics of rain in the submillimeter range. He calculated the backscattering cross section and the attenuation coefficient for submillimeter radiation using the Marshall-Palmer and Best drop-size

Table XXVIII. Attenuation Coefficient for Rain vs Rainfall Intensity for Wavelengths between 0.63  $\mu m$  and 8 mm (Data from Ref. 56)

### Attenuation Coefficient $\tau(dB/km)$

| Intensity<br>of rain.           |                                          |                                          |                                          | Wave                                     | length o                                 | fradiatio                                | on                                       |                                  |                                          |                                          |
|---------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|----------------------------------|------------------------------------------|------------------------------------------|
| mm/hr                           | 0.63 µ m                                 | 3.5 µm                                   | 10.6 µm                                  | 100 jim                                  | 300 µm                                   | 800 jim                                  | 1 mm                                     | 2 mm                             | 4 mm                                     | 8 mn                                     |
| 1<br>5<br>10<br>25<br>50<br>100 | 1.1<br>3.0<br>4.5<br>7.8<br>12.5<br>18.2 | 1.1<br>3.0<br>4.5<br>7.9<br>13.6<br>18.5 | 1.1<br>3.0<br>4.5<br>7.9<br>12.6<br>18.5 | 1.5<br>3.4<br>5.2<br>8.8<br>13.9<br>20.0 | 1.5<br>3.5<br>5.4<br>9.3<br>14.7<br>21.3 | 1.6<br>3.6<br>5.6<br>9.6<br>15.3<br>22.1 | 1.7<br>3.7<br>5.7<br>9.4<br>15.6<br>22.7 | 1.5<br>3.6<br>5.6<br>9.0<br>16.0 | 0.8<br>2.9<br>4.8<br>8 9<br>15.0<br>22.3 | 0.3<br>1.4<br>2.7<br>5.9<br>11.1<br>17.3 |

Table XXIX. Calculated Attenuation Coefficient for Rain vs Rainfall Rate for Drop-Size Distributions of Best and Polyakova at  $T=20\,^{\circ}\text{C}$ 

## Attenuation Coefficient $\gamma(dB/km)$

|                                                           |                                                        |                                                         |                                                        | W                                                       | aveler                                         | igth λ.                                                 | mm                                                     |                                          |                                                        |                                                         |
|-----------------------------------------------------------|--------------------------------------------------------|---------------------------------------------------------|--------------------------------------------------------|---------------------------------------------------------|------------------------------------------------|---------------------------------------------------------|--------------------------------------------------------|------------------------------------------|--------------------------------------------------------|---------------------------------------------------------|
| I.<br>nim/hr                                              | 2                                                      | .0                                                      | 1                                                      | 0                                                       | 0                                              | .8                                                      | 0                                                      | 5                                        | 0                                                      | .1                                                      |
|                                                           | Вa                                                     | ьp                                                      | В                                                      | P                                                       | В                                              | P                                                       | В                                                      | P                                        | В                                                      | P                                                       |
| 0.5<br>1.0<br>2.5<br>5.0<br>10.0<br>25.0<br>50.0<br>100.0 | 0.7<br>1.5<br>2.3<br>3.6<br>5.6<br>9.3<br>16.0<br>23.0 | 0.8<br>1.3<br>2.6<br>4.1<br>7.7<br>13.8<br>22.1<br>34.0 | 0.9<br>1.7<br>2.4<br>3.7<br>5.7<br>9.9<br>15.6<br>22.7 | 0,8<br>1,3<br>2,5<br>3,9<br>7,2<br>12,8<br>20,5<br>31,5 | 0.9<br>1.6<br>2.4<br>3.6<br>5.6<br>9.6<br>15.3 | 0.8<br>1.3<br>2.4<br>3.8<br>7.0<br>13.5<br>20.0<br>30.0 | 0.9<br>1.6<br>2.3<br>3.5<br>5.4<br>9.3<br>14.7<br>21.3 | 0.8<br>1.1<br>3.4<br>6.3<br>11.1<br>18.4 | 0.8<br>1.5<br>2.1<br>3.2<br>4.9<br>8.3<br>12.7<br>18.0 | 0.6<br>1.0<br>2.0<br>3.1<br>5.8<br>10.4<br>16.6<br>20.5 |

- a. Calculated using the Best Distribution
- b. Calculated using the Polyakova Distribution

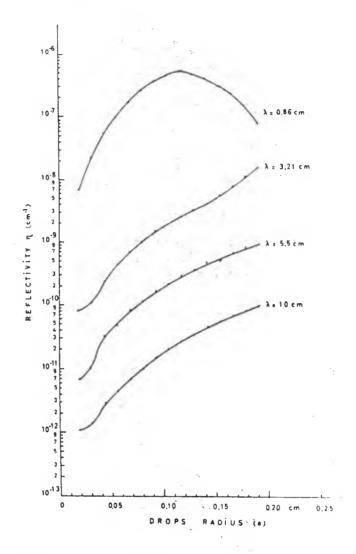
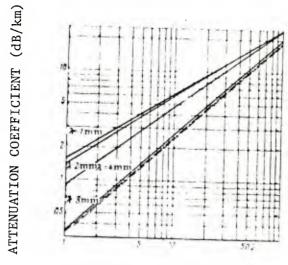


Fig. 33. Rain Drop Reflection as a Function of Drop Size for Several Wavelengths (Data from Ref. 57)



RAIN RATE (mm/hr)

Fig. 34. Computed Attenuation Coefficients at  $\lambda=1$ , 2, 4 and 8.6 mm vs Rainfall Rate (Data from Ref. 58)

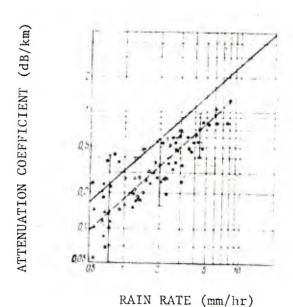
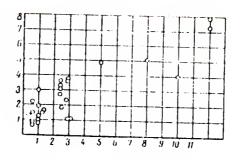


Fig. 35. Measured and Calculated Attenuation Coefficients at  $\lambda=8.6$  mm vs Rainfall Rate: Solid Curve is Calculated Data, Dashed Curve is Average of Measured Data, Points are Measured Data (Data from Ref. 58)





RAINFALL RATE (mm/hr)

Fig. 36. Measured Attenuation in Rain for 0.96 cm Radiation vs Rainfall Rate (Data from Ref. 60)

Table XXX. Average Values of the Attenuation Coefficient in Rain for Rainfall Intensities of 5 and 12 mm/hr and Wavelengths of 0.96, 4.3, 6.2, 8.6 and 9.6 mm (Data from Ref. 63)

# Attenuation Coefficient (dB/km)

| Wave-<br>length | Ir<br>(mm/ | ntensity<br>'hr) |
|-----------------|------------|------------------|
| (mm)            | 5          | 12               |
| 0.96            | 4.8        | 7.8              |
| 4.3             | 3.5        | 6.0              |
| 6.2             | 3.0        | 6.5              |
| 8.6             | 2.2        | 3.0              |
| 9.6             | 1.2        | 2.0              |

distributions. Results of his calculations for the backscattering cross section in units of  $(m^{-1})$  are shown in Fig. 37. His attenuation coefficient, in dB/km, is shown in Fig. 38. Both calculations were for radiation of wavelengths of 0.3 mm to 10 cm, and rainfall rates of 0.1, 1, 10, and 100 mm/hr. He presented a large bibliography on work performed prior to 1970, with 60 references.

Joerg Sander  $^{63}$  measured the attenuation due to rain at 5.77, 3.3, and 2 mm. Simultaneously recorded were rainfall rate and a part of the drop-size spectrum. He calculated the total cross section of spherical water drops at a temperature of 10°C as a function of radius, from 0.3-3.5 mm, using Mie scattering theory. Sander's calculated cross section data are shown in Fig. 39. His measured attenuation data are presented in Figs. 40, 41, and 42 as scattergrams for 5.77, 3.3 and 2.0 mm wavelength radiation respectively. The measured data are compared in these figures with a calculation of the attenuation in dB/km vs rainfall rate for 5.77 mm, 3.3 mm and 2 mm radiation, respectively. Also plotted on these scattergrams were regression curves for rainfall rate with attenuation,  $\overline{R}_{A}|_{D}$ , and attenuation with rainfall rate  $\overline{D}|_{R}_{A}$ .

Robert Crane wrote a tutorial article on "Attenuation due to Rain, a Mini Review." He reviewed progress on the development and verification of a theory of rain-caused attenuation, and considers the the statistical models required to predict attenuation, ca 1975. Wavelength coverage in his article appears to be from 15 cm to 0.8 cm.

- R. R. Rogers<sup>65</sup> has reviewed "Statistical Rainstorms Models: Their Theoretical and Physical Foundations," in a long article, ca 1976. Most of the data discussed by Rogers is for propagation of 10-20 GHz radiation in rain, but some millimeter wavelength data is discussed. He has a number of suggestions for further research.
- G. C. McCormick  $^{66}$  wrote an article on theory of propagation in a precipitation medium, considering the polarization aspects of the rain. He concluded that the most advantageous polarizations for the measurements for (rain) medium characteristics are right-hand circular, left-hand circular, and  $\pm$  45° slant linear (with respect to the rainfall direction).

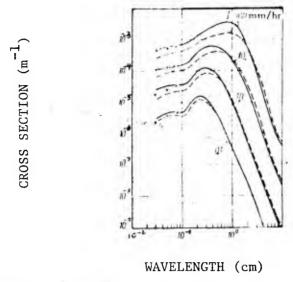


Fig. 37. Specific Backscattering Cross Section of Rain of Different Intensity at 18°C, Marshall-Palmer Distribution (dashed lines) (Data from Ref. 62)

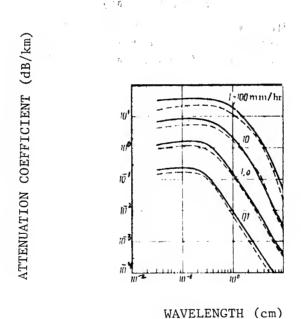


Fig. 38. Attenuation Coefficient of Rain of Different Intensity at 18°C, Marshall-Palmer Distribution (continuous lines) and Best Distribution (dashed lines) (Data from Ref. 62)

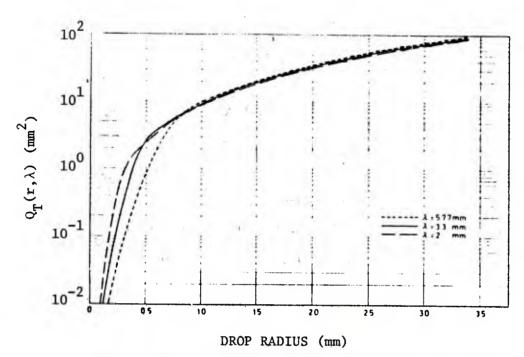


Fig. 39. Mie Calculations of the Extinction Efficiency for Rain Drops vs Drop Radius for  $\lambda=5.77$ , 3.3 and 2.0 mm (Data from Ref. 63)

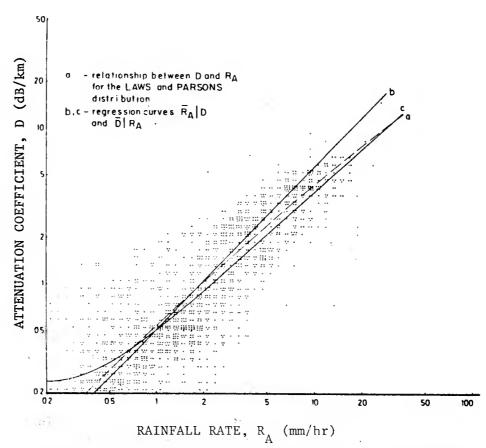


Fig. 40. Measured Attenuation Coefficients vs Rainfall Rate,  $R_{A}$  at  $\lambda = 5.77~\mu m$  (Data form Ref. 63)

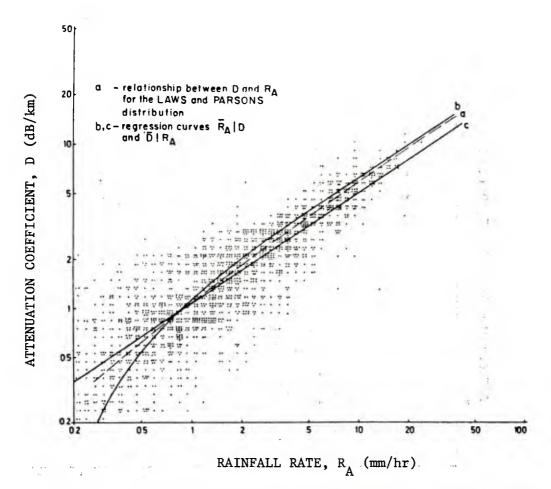


Fig. 41. Measured Attenuation Coefficients vs Rainfall Rate,  $R_{\mbox{\scriptsize A}}$  , at  $\lambda = 3.3$  mm (Data from Ref. 63)

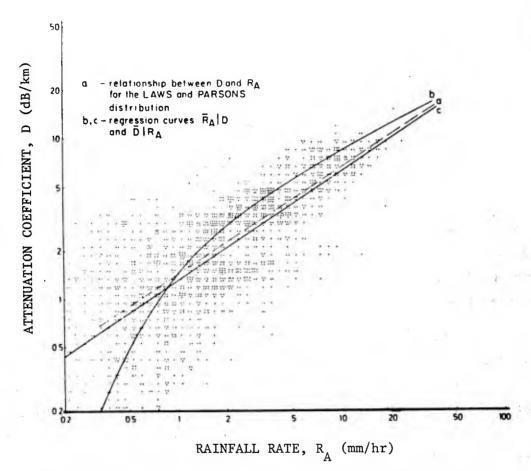


Fig. 42. Measured Attenuation Coefficients vs Rainfall Rate, R  $_{A}$  , at  $\lambda = 2$  mm (Data from Ref. 63)

Radio waves of 16.5 - 30.9 GHz were considered in his calculations.

Julian Goldhirsh $^{67}$  computed some attenuation fade statistics for satellite to 2 ground stations separated by a distance d. He modeled the total (zenith path) attenuation by

$$A_{i} = \int_{0}^{\ell i} k(\ell) d\ell \text{ (in dB),}$$

where

$$k(\ell) \simeq a[z(\ell)]^b$$
 in dB/km..

The values of a and b used by Goldhirsh are given in Table XXXI. He also computed the joint conditional probability that attenuation at two terminals separated by a distance d exceeds the abcissa at path elevation angle  $\theta$  = 45° at 100 GHz. His joint probability calculations are presented here as Fig. 43. He has done similar calculations for frequencies of 13, 18, and 30 GHz. He used the radar reflectivity of rain at 2.8 GHz as part of his data base.

- P. Wiley 68 in his PhD thesis, considered the non-sphericity of raindrops regarding scattering calculations, reviewing Oguchi's work of the 1960s. He then extensively reviewed the literature on cm and mm rainfall propagation experiments. He analyzed in detail some 19.3 GHz data for polarization effects. He compared his results for rainfall attenuation with that of Oguchi, for horizontal and vertical polarization for a 1.43 km path at 19.3 GHz. His data are shown here as Fig. 44. He calculated the cross polarization vs pathlength for a tilt angle of 60° and a frequency of 19.36 GHz. His results are shown in Fig. 45. He did similar calculations for a tilt angle of 75°; those results are shown in Fig. 46. Conclusions he reached regarding the influence of polarization on millimeter wave propagation through rain are the following:
- 1) The best polarizations to use for a depolarization experiment are  $\pm$  45° from the vertical. 2) Vertical and horizontal polarizations should not be used for a depolarization experiment. 3) Vertical polarization suffers the least average attenuation during rainfall. 4) Oguchi's attenuation and phase rotations for 19.36 GHz are correct. 5) The effective

Table XXXI. Best Fit Values of a and b for  $k = aZ^b$ (k in dB/km, Z in mm<sup>6</sup>/m<sup>3</sup>)

(Data from Ref. 67)

| f<br>(GHz) | а                       | Ь     |
|------------|-------------------------|-------|
| 13         | 3.15 × 10 <sup>-4</sup> | 0.732 |
| 18         | 9.12 × 10 <sup>-4</sup> | 0.681 |
| 25         | 3.25 × 10 <sup>-3</sup> | 0.610 |
| 30         | 6.82 × 10 <sup>-3</sup> | 0.570 |
| 100        | 6.20 × 10 <sup>-2</sup> | 0.429 |

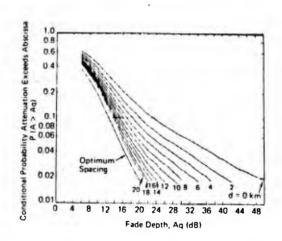


Fig. 43. Joint Conditional Probability that Attenuation at Two Terminals Separated by Distance d Exceeds the Abscissa at Path Elevation Angle  $\theta$ =45° at f=100 GHz (Data from Ref. 67)

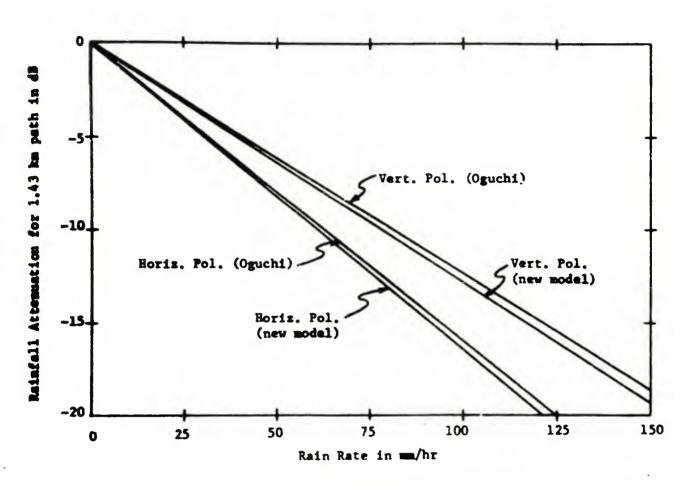
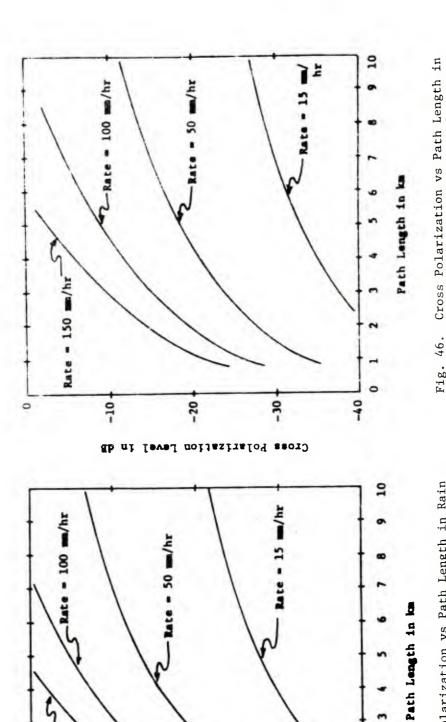


Fig. 44. Theoretical Prediction of Rainfall Attenuation at 19.3 GHz for a 1.43 km Path (Data from Ref. 68)



Cross Polarization vs Path Length in Rain for a Tilt Angle of 60° and a Frequency of 19.3 GHz (Data from Ref. 68) Fig. 45.

9

Rain for a Tilt Angle of  $75^\circ$  and a Frequency of 19.3 GHz (Data from Ref. 68)

Fig. 46.

-30

-20

Cross Polarization Level in db

-10

percentage of oblate drops assumed in an analysis is critical to the predicted polarization level. 6) Polarization diversity is not feasible as a means of increasing resistance to rain-induced fading. 7) The use of polarization multiplexing utilizing orthagonal polarizations is limited to very short path lengths. 8) Use of a distribution of rain-drop sizes is unnecessary to get good agreement between theory and experiment(!).

Louis Ippolito, 69 the NASA Goddard ATS-5 and 6 millimeter wave communications experiment manager, wrote his 1977 PhD thesis on "Scattering in Discrete Random Media with Implications to Propagation through Rain." Ippolito 70 investigated the multiple scattering effects on wave propagation through a volume of discrete scatterers. The mean field and intensity for a distribution of scatterers was developed using a discrete random media formulation, and second order series expansions for the mean field and total intensity derived for onedimensional and three-dimensional configurations. The volume distribution results were shown to proceed directly from the one-dimensional results. Ippolito's analyses demonstrated that either discrete or continuous techniques may be employed for the mean field and intensity expansions, as long as care is taken to insure non-overlapping scatterers in the formulation. The multiple scattering intensity expansion was compared to the classical "single scattering" intensity and the classical result was found to represent only the first three terms in the total intensity expansion. The Foldy approximation to the mean field was applied to develop the coherent intensity, and was found to exactly represent all coherent terms of the total intensity. An incoherent intensity term, secular in L, in path length, was found which was not accounted for in the Foldy approximation result or in the "single scattering" formulation. Ippolito's study demonstrated the feasibility of using discrete random media techniques for the determination of multiple scattering effects in propagation through a volume of discrete scatterers, and has provided some insight to the more general problem of multiple scattering in a rain volume.

L. Ippolito  $^{70}$  chaired a meeting on the 20 and 30 GHz experiments with the ATS-6 satellite. A number of interesting papers on the attenuation and depolarization of 20 and 30 GHz radiation was presented at that meeting.

### 2.4 Scattering and Attenuation by Snow

The scattering of radiation by snow is different than the scattering by rain in that the dielectric constant of ice is much less than that of water, and that the ice particle making up snow is distinctly nonspherical.

M. D. Blue  $^{71}$  of Georgia Tech measured the permittivity of water and ice at 97-103 GHz by a reflectivity measurement of water and ice relative to mercury. He found that the reflectivity of water was:

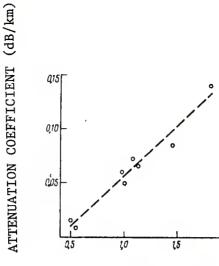
 $R = 0.392 \pm .014$  for 103.8 GHz radiation,

thus n - ik = 3.24 - 1.825i for the index of refraction for water and  $\epsilon' - i\epsilon'' = 7.16 - 11.825i$  for water's dielectric constant.

He also measured the reflectivity of water at temperatures from 32°C to 47°C at 103.8 GHz, though no sets of terms for Debye's equation were given, as a function of temperature. The index of refraction of ice at 99 GHz was found to be  $1.7 \pm .08$ , real, within experimental measuring ability.

The literature on scattering and attenuation by snow in the millimeter wave range is very sparse. Malinkin, Sokolov and Sukhonin <sup>58</sup> measured the attenuation due to snow at 8.6 mm wavelength. Their result, in dB/km vs snowfall rate in mm/hr is shown here as Fig. 47. They concluded that the attenuation in dry snow is 2.5-5 times smaller than the attenuation in rain of the same intensity. Reference 58 includes a reference list of 11 articles.

Yu. S. Babkin et al., measured the attenuation of radiation at a wavelength of 0.96 mm in snow, with a vertical polarization, and a 680 m path length. The following empirical relation was found to fit the mean attenuation in dB/km vs snowfall rate in mm/hr,



SNOWFALL RATE (mm/hr)

Fig. 47. Measured Attenuation Coefficient at  $\lambda=8.6$  mm vs Snowfall Rate (for a Snow Density of  $\rho\simeq0.008$  gm/cm<sup>3</sup>). Dashed Curve Gives Averaged Experimental Data (from Ref. 58)

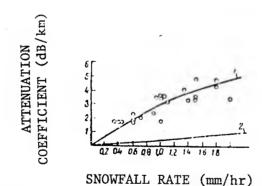


Fig. 48. Comparison of Measured and Calculated Attenuation Coefficient in Snow vs Snowfall Rate for  $\lambda$ =0.96 mm (Curve 1 and Points are Experimental Data, Curve 2 is Based on Mie Computations) (Data from Ref. 72)

$$\gamma (dB/km) = 3.02 \text{ I}^{.79}$$

where I = snowfall rate per mm/hr.

When the authors of Ref. 72 tried to analyze the measured attenuation data with the use of Mie theory, they obtained results that disagreed with the measurements by a factor of about 3. They assumed that the ice index of refraction was 1.78-0.00024i, and estimated that a homogenous mixture of ice, water and air (making up snow) would have an index of refraction of

$$m_{S} = 1.052 - 0.00012i \text{ for } \lambda = 0.96 \text{ mm.}$$

They assumed that an equivalent volume of snow (melting ice) would have a density of  $0.07~{\rm gm~cm}^{-3}$ . They calculated an attenuation coefficient related to that of water of the same wavelength. Doing this, they found that attenuation in rainfalls is 30-40% less than in snow of the same equivalent water content. Babkin's data on snowfall attenuation in dB/km vs snowfall rate is shown in Fig. 48.

#### 2.5 Attenuation by Ozone in the Atmosphere.

Ozone is an atmospheric constituent that manifests itself most at higher altitudes except during thunderstorms, lightning, etc., and in and around arcking electronic devices (brush type motors).

The most comprehensive article on the millimeter wave spectrum of ozone is by M. Lichtenstein, J. Gallagher, and S. A. Clough. They used a Stark effect spectrometer and measured absorption lines for frequencies between 9.2 to 320 GHz. Results of their absorption measurements are given in Table XXXII. Note that the strongest lines (where the intensity is more than  $5 \times 10^{-4}$  X  $10^{-19}$  cm  $^{-1}$ /molecule/cm ) occur at frequencies higher than 230 GHz.

A. Barbe, C. Secroun et al., more recently (1977) remeasured some of the absorption lines of ozone in the 15-80 GHz region; their

Table XXXII.  $0_3$  Pure Rotational Ground Vibrational State Transitions (Data from Ref. 73)

| Upper<br>State     | Lower<br>State     | Obs.<br>Frequency | Calc.<br>Frequency                     | Obs<br>Calc. | Intensity<br>296°K 10 <sup>-19</sup> cm-1/ |
|--------------------|--------------------|-------------------|----------------------------------------|--------------|--------------------------------------------|
| J KAKC             | J K K C            | MH z              | MH z                                   | MHz          | Molec/cm <sup>2</sup>                      |
| 21 2 20            | 23 3 17            | 9201.             | 9200.34                                | 0.66         | 0.0000002                                  |
| 10 1 9             | 9 2 8              | 10226.            | 10225.55                               | 0.45         | 0.0000003                                  |
| 4 C 4              | 3 1 3              | 11073.            | 11072.38                               | -0.38        | 4.0000004                                  |
| 23 4 20            | 24 3 21            | 14856.            | 14306.45                               | -0.45        | 3.33.53.4                                  |
| 27 3 25            | 25 4 22            | 16163.            | 16162.58                               | 0.42         | 0.0000004                                  |
| 18 7 15            | 19 2 18            | 23961.            | 23 59.66                               | 0.34         | 0.0000014                                  |
| 39 6 32            | 39 5 35            | 25511.            | 25511.08                               | -0.08        | 3.0000022                                  |
| 16 7 14<br>36 3 33 | 17 1 17<br>37 2 36 | 25649.            | 25650.89                               | 0.11         | 0.0000006                                  |
|                    |                    | 2 2 4 4 4         | 27459.81                               |              | 0.0000001                                  |
| 41 5 37            | 40 5 34            | 27662.            | 27861.35                               | -0.35        | 3.0000002                                  |
| 24 4 20<br>15 3 13 | 25 3 23            | 28960.            | 28960.36                               | -0.36        | 0.0000015                                  |
| 15 3 13<br>14 2 12 | 15 2 14<br>15 1 15 | 30052.            | 30091.85                               | 0.15         | 3.3.60326                                  |
| 18 2 15            |                    | 30181.            | 30161.15                               | -0.15        | 3.000014                                   |
| 23 7 22            |                    | 30525.            | 30523.94                               | 0.06         | 0.0000008                                  |
| 18 2 16            | 22 3 19<br>17 3 15 | 36023.            | 36021.95                               | 0.05         | 9.0000023                                  |
| 3-3 2 32           | 32 3 29            | 37832 •           | 37832+38                               | -0.38        | 0.0000042                                  |
| 1 1 1              | 2 3 2              | 42932.62          | 39477.25                               |              | 0.0000005                                  |
| 12 2 10            | 13 1 13            | 43654.            | 42932.29                               | 0.13         | 0.0000018                                  |
| 37 6 32            | 38 5 33            | 430344            | 43653 <b>.</b> 24<br>43654 <b>.</b> 56 | -0.24        | 0.0000035                                  |
| 20 2 18            | 21 1 21            |                   | 44471.08                               |              | 0.0009338<br>0.0000013                     |
| 30 5 25            | 31 4 28            |                   | 50034.82                               |              | 0.0000013                                  |
| 35 4 32            | 34 5 29            |                   | 51053.15                               |              | 0.0000026                                  |
| 26 3 23            | 25 4 22            | 51975.75          | 51076.00                               | -0.25        | J.0300044                                  |
| 49 5 44            | 48 7 41            | , , , , ,         | 51981.00                               | -0.23        | 0.0000002                                  |
| 7 2 5              | 8 1 7              | 53689.15          | 53545.28                               | -3.13        | 0.0000002                                  |
| 25 2 24            | 24 3 21            | 55354.56          | 55354.51                               | 3.05         | 0.0000043                                  |
| 44 7 37            | 45 5 40            |                   | 56973.57                               | ,            | 0.000004                                   |
| 29 3 27            | 28 4 24            |                   | 58094.11                               |              | 0.00000044                                 |
| 31 2 30            | 30 3 27            |                   | 58410.52                               |              | 0.0000017                                  |
| 29 5 25            | 30 4 26            | 61347.54          | 61347.33                               | 0.21         | 3.3353342                                  |
| 51 8 44            | 52 7 45            | •                 | 61-29.47                               |              | 0.0000001                                  |
| 16 3 13            | 17 2 16            | 61925.85          | 51920.78                               | 0.08         | 0.00000399                                 |
| 34 4 30            | 33 5 29            |                   | 63078.75                               |              | 0.0000031                                  |
| 10 2 8             | 11 1 11            | 65236.15          | 65236.08                               | 0.07         | 0.0000083                                  |
| 27 2 26            | 25 3 23            |                   | 55058.43                               |              | 3.0333345                                  |
| 29 2 28            | 23 3 25            |                   | 67249.37                               |              | 0.0000034                                  |
| 5 0 5              | 5 1 5              | 67356.24          | 57356.13                               | 3.11         | 0.3000222                                  |
| 49 3 47            | 45 4 44            |                   | 67836.39                               |              | 0.0000551                                  |
| 22 2 23            | 23 1 23            |                   | 68421.95                               |              | 0.0000020                                  |
| 39 3 35            | 39 2 38            |                   | 73921.59                               |              | 0.0000005                                  |
| 42 5 37            | 41 5 35            |                   | 75847.61                               |              | 0.0000014                                  |
| 22 4 19            | 23 3 21            | "c393.52          | 76393.46                               | 0.06         | 0.0000119                                  |
| 12 1 11            | 11 2 13            | 76533.76          | 76573.56                               | 3.25         | 0.0000225                                  |
| 21 4 18            | 22 3 19            |                   | 77602.44                               |              | 0.0000130                                  |
| 35 6 30            | 37 5 33            |                   | 73993.19                               |              | 0.0000029                                  |
| 43 5 39            | 42 5 36            |                   | 80840.04                               |              | 0.0000013                                  |
| 43 7 37            | 44 6 38            |                   | 81292.09                               |              | 0.0000009                                  |
| 50 8 42            | 51 7 45            |                   | 90008.01                               |              | 0.0000003                                  |
| 50 5 44<br>9 2 5   | 49 7 43            | 02025             | 91029.25                               |              | 0.0000004                                  |
| 9 2 5              | 9 1 9              | 93844.35          | 93844.37                               | -0.02        | 0.0000165                                  |

Table XXXII. (Continued)

| State                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | υ | ppe            | r              | 1 | Lou | er  |   |     |     |     | ж   |     |    | _    |      |              |     |        |   |       |       |        |    |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---|----------------|----------------|---|-----|-----|---|-----|-----|-----|-----|-----|----|------|------|--------------|-----|--------|---|-------|-------|--------|----|
| 13 3 11 14 2 12 93955.05 93955.03 -2.18 0.0002336 2 1 1 2 0 2 95796.40 95796.35 -2.19 0.0002396 2 1 1 2 0 2 96228.34 96222.36 -0.55 0.0002096 2 1 1 2 0 2 96228.34 96222.36 -0.55 0.0002096 3 1 3 29 30 4 26 95796.40 95796.35 -2.19 0.0002096 2 1 1 3 4 3 6 5 21 96228.34 96222.36 -0.55 0.0002096 3 1 6 30 36 5 31 10136.87 102591.92 0.0003052 4 1 3 4 0 4 10136.87 102591.92 0.0003052 4 1 3 14 0 4 0 4 102378.39 103876.39 0. 0.0003051 1 3 11 15 2 14 102378.39 103876.39 0. 0.0003051 1 3 11 15 2 14 102378.39 103876.39 0. 0.0003051 1 5 45 50 7 43 10259.39 103876.39 0. 0.0003051 2 7 19 17 3 17 109555.33 103969.26 0.07 0.000305 2 7 19 17 3 17 109555.33 103969.26 0.07 0.000305 2 7 19 17 3 17 109555.33 103969.26 0.07 0.000305 2 7 19 17 3 17 109557.33 103969.26 0.07 0.000305 2 7 19 17 3 17 109557.33 103969.26 0.07 0.0003051 3 1 1 1 0 0 0 1 119364.34 11074.36 5 2 4 6 1 5 11997.22 114677.30 -0.10 0.0003051 1 1 1 0 0 0 1 119364.34 11394.45 -0.15 0.0003051 1 1 1 0 0 0 1 119364.34 11394.45 -0.15 0.0003051 1 1 1 0 0 0 1 119364.34 11394.45 -0.15 0.0003051 1 1 1 0 0 0 1 129369.36 11394.45 -0.15 0.0003051 2 8 3 25 27 4 24 123349.10 123349.45 -0.38 0.0002328 8 0 2 7 1 7 1 223349.10 123349.45 -0.38 0.0002386 8 0 2 7 1 7 1 223349.13 123349.45 -0.38 0.0002386 8 0 2 7 1 7 1 223349.13 123349.45 -0.38 0.0002386 8 0 2 7 1 7 1 223349.13 123349.49 -0.39 0.00001279 2 2 4 6 2 1 3 19 125411.19 125419.2 -0.10 0.000167 4 0 3 3 41 2 40 12349.13 123349.49 -0.09 0.00001279 3 3 3 1 2 4 2 2 1 12094.81 13395.27 0.0001010 3 4 4 0 2 3 5 5 11 130954.81 130399.40 0.0003386 6 2 0 7 7 1 7 1 223319.55 128319.94 -0.09 0.00002564 6 1 9 4 10 0 10 1 142175.12 142174.97 0.15 0.0000167 9 4 10 0 10 1 142175.12 142174.97 0.15 0.0000165 9 4 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                                                                                                                                                                                                                                                                                                                |   |                |                | 5 | Sta | te  | / |     | F   |     |     |     | -y |      |      |              |     |        |   |       |       |        |    |
| 13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | J | K <sub>A</sub> | K <sub>C</sub> | J | K   | A K |   |     |     |     |     |     | •  |      |      | ,            |     |        |   | 296°K | lecto | . 7 cm | 1/ |
| 11 3 29 30 4 26 95796.15 5 -0.18 0.0000236 2 1 1 2 0 2 96228.34 96228.34 96228.35 -0.18 0.0000236 37 4 34 6 5 31 125 96228.34 96228.36 -0.15 0.0000236 38 5 30 36 5 31 100591.92 0.0000352 38 5 23 129 4 26 101835.42 10136.73 0.14 0.0000352 38 5 23 129 4 26 101835.42 10136.73 0.1 0.0000352 38 5 23 129 4 26 101835.42 1013435.17 0.25 0.0000352 30 7 18 19 3 17 109559.33 10969.26 0.07 0.0000352 30 7 18 19 3 17 109559.33 10969.26 0.07 0.000035 40 3 45 46 4 42 1103836.04 110335.67 0.17 0.000035 5 2 4 6 1 5 5 0 6 110336.04 110335.67 0.10 0.000005 5 2 4 6 1 5 14979.20 116576.36 0.000005 5 2 4 6 1 5 116979.20 116576.30 0.000005 5 2 4 6 1 7 1009.20 116577.30 0.10 0.000005 5 2 4 6 1 7 8 0 6 120287.46 12038.49 0.000005 5 2 4 6 1 7 8 0 6 120287.46 120387.49 0.000005 5 2 7 5 23 28 4 24 119277.50 118577.50 0.10 0.0000167 5 2 0 2 1 6 1 7 1 7 125369.58 125389.28 0.30000236 6 1 7 8 0 6 120287.46 120387.49 0.0000236 6 1 7 8 0 6 120287.46 120387.49 0.0000236 6 1 7 8 0 6 120287.46 120387.49 0.0000236 6 1 7 1 7 125369.58 125389.28 0.30000236 6 1 7 1 7 125369.58 125389.28 0.30000236 6 1 7 1 7 125369.58 125389.28 0.30000236 6 1 7 1 7 125369.58 125389.28 0.30000167 6 1 9 1 0 1 0 1 0 1 0 1 0 1 0 0 0 0 0 0 0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |   | _              |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       | 100/0 | -      |    |
| 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                |                |   |     | _   |   |     |     |     |     |     |    |      |      |              | -   | -3.18  | ļ | 0.00  | cacz: | 36     |    |
| 27                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   | _              |                |   |     |     |   |     |     |     |     |     | _  |      |      |              | -   | -2.19  |   | 0.0   | occc  | 76     |    |
| 24 2 22 25 1 25 1 25 1 25 1 25 1 25 1 25                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |   |                |                |   |     |     |   |     | 96  | 2   | 29  | • 3 | 4  |      |      |              | -   | 0.05   |   |       |       |        |    |
| 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 28 5 23 1 29 4 26 10138.87 10138.73 0.14 3.0003015 18 3 11 15 214 102878.39 103874.39 0. 2.25 0.20002015 11 6 46 50 7 43 102878.39 105618.33 0. 2.0003049 17 3 45 46 4 22 102836.04 110335.67 0.17 0.2003049 18 7 3 45 46 4 22 110336.04 110335.67 0.17 0.2003049 18 7 3 45 46 4 22 110336.04 110335.67 0.17 0.2003049 18 1 7 8 6 6 1 3 114979.20 114776.30 -0.10 0.00020212 19 1 1 0 0 0 118364.34 118364.45 -0.15 0.0003021 11 1 0 0 0 0 118364.34 118364.45 -0.15 0.0003021 12 3 25 27 4 24 119277.65 119277.55 0.10 0.10 0.0000167 18 1 7 8 0 8 124087.46 124087.26 0.30 0.000127 19 1 7 10 0 0 118364.34 118364.45 -0.38 0.000127 20 4 16 21 2 19 125413.19 125403.2 -0.00 0.000167 21 3 3 31 22 4 28 124087.46 124087.26 0.30 0.0001279 22 4 16 2 2 3 19 125413.19 125403.2 -0.00 0.0001279 23 3 31 22 4 28 124094.82 125939.29 0.30 0.0001279 24 6 2 2 3 7 4 1 2 40 2 12192.25413.19 125403.2 -0.00003046 23 3 3 1 22 4 28 124094.82 125939.29 0.30 0.0001279 24 6 2 2 3 7 1 1 200000000000000000000000000000000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.3   | زودود | 25     |    |
| 28 5 23 29 4 26 101835.42 101835.17 0.25 c.3003126 14 3 11 15 2 14 103978.39 103878.39 0. 0.2003126 15 6 46 50 7 43 109959.33 109659.26 0.77 c.3000365 10 7 19 17 3 17 109559.33 109659.26 0.77 c.3000365 11 5 6 6 6 6 110336.04 110351.36 c.17 0.000365 15 2 4 6 1 5 8 8 114979.22 110941.36 c.3000365 15 2 4 6 1 5 114979.22 114679.30 -0.10 c.0003271 15 1 1 0 0 0 1 119364.34 118184.49 -0.15 0.0000271 11 1 1 0 0 0 1 119364.34 118184.49 -0.15 0.0000271 11 1 1 0 0 0 0 119364.34 118184.49 -0.15 0.0000271 11 1 1 0 0 0 0 119364.34 118184.49 -0.15 0.0000271 11 1 1 0 0 0 0 119364.34 118184.49 -0.15 0.0000271 11 1 1 0 0 0 0 119364.34 118184.49 -0.10 0.0001272 12 3 25 27 4 24 123349.10 1123349.45 -0.15 0.00002718 11 7 8 0 0 0 124087.46 124087.26 0.10 0.10 0.1000127 12 4 16 21 3 19 125413.19 125413.29 -0.10 0.0001279 13 3 3 3 1 3 2 4 28 125089.58 125089.28 0.30 0.0001279 14 1 1 2 40 12589.58 128133.95 128133.94 -0.09 0.0000278 16 2 0 7 1 7 126813.85 128133.94 -0.09 0.0000278 16 2 0 7 1 7 126813.85 128133.94 -0.09 0.0000278 17 3 5 4 6 6 2 8 5 5 31 130954.81 130954.72 0.0000278 18 4 16 20 3 17 136860.24 136960.24 0.0000378 14 1 1 3 13 2 12 144919.44 14919.66 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 13 13 2 12 144919.44 14919.16 0.26 0.0000994 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   | _              |                |   |     |     |   | _   |     |     |     |     |    |      |      |              |     |        |   | 0.00  | 00005 | 52     |    |
| 14 3 11 15 2 14 103978.39 103278.39 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000280 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.2000281 0. 0.200 |   |                |                |   |     |     |   |     |     |     |     |     |    | 101  | 736  | • 73         |     | 0.14   |   | 0.00  | CODE  | 15     |    |
| \$1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     | 0.25   |   | 0.00  | 0001  | 26     |    |
| 22 2 18 19 3 17 109559.33 109469.26 0.37 3.35 4.6 4.2 110936.04 110751.36 0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |   |                |                |   |     |     |   | 1   | C 3 |     | ? @ | • 3 | 9  | 103  | £76. | • 39         |     | ٥.     |   | 3.00  | CCSZS | 3 C    |    |
| 47 3 45 66 1 22 6 110836.04 11075136 0.37 6 1 5 6 0 6 110836.04 11075136 0.3020021 6 2 7 35 43 5 38 11104979.20 1144975.30 -0.10 0.0020021 6 2 4 6 1 5 114979.20 1144975.30 -0.10 0.0020025 1 1 1 0 0 0 11836.34 11836.44 -0.15 0.0020025 1 1 1 0 0 0 0 11836.34 11836.44 -0.15 0.0020025 27 5 23 28 4 24 119277.60 119277.50 0.10 0.0020255 28 3 25 27 4 24 123349.10 123349.48 -0.38 0.000238 8 1 7 8 0 8 124087.46 124087.28 0.10 0.0020127 20 4 16 21 3 19 125889.58 1253589.28 0.30 0.0001279 20 4 16 21 3 19 125813.19 125413.20.01 0.0020128 6 2 2 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 3 5 5 31 130954.81 130954.72 0.9 0.0020254 6 2 3 5 5 31 130954.81 130954.72 0.9 0.0020254 6 2 4 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 1 7 1 7 188313.85 128313.94 -0.09 0.0020254 6 2 1 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 7 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 1 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 1 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 1 7 1 7 128313.85 128313.94 -0.09 0.0020254 6 2 2 2 7 1 27 1 16860.24 13366.75 0.0020115 6 2 2 4 7 1 7 1 188313.85 138313.99 0.0020115 6 2 2 4 7 1 7 1 18860.24 13366.75 0.0020115 6 2 2 4 7 1 27 1 144915.12 142174.97 0.15 0.0020234 6 2 2 4 7 1 27 1 148744.85 148744.95 0.00009944 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |   |                | _              |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 3.00  | 0000  | 5      |    |
| 6 1 5 6 6 C 6 110836.04 110835.87 C.17 C.CC01273 C.0000055 C 2 4 5 1 5 114979.20 114979.30 -0.10 C.0000021 C.000005 C 114916.17.79 C.15 C.000005 C.21 C.00005 C 11 1 1 1 C C C C C C C C C C C C C C                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |   |                |                |   |     | -   |   | 1   | 29  | 5 5 | 5 9 | • 3 | 3  |      |      |              |     | 0.37   |   | 0.30  | 0634  | ۶.     |    |
| 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                | _              |   |     | -   |   | _   |     |     |     | _   |    |      |      |              |     |        |   | 0.00  | 0000  | . 5    |    |
| 5 2 4 6 1 5 114979.20 114779.30 -0.10 C.CC.2022                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |   |                |                |   |     | _   |   | 1   | 1 0 | 93  | 36  | ٠.  | 4  | 110  | 35.  | . <u>e</u> 7 |     | C.17   |   | 0.00  | 3127  | 73     |    |
| 49 8 42 50 7 43                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.00  | 00002 | 21     |    |
| 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                |                |   |     |     |   | 1   | 14  | Ç.  | 7 9 | . 2 | 2  |      |      |              | _   | 0.10   |   | 0.00  | :::25 | 2      |    |
| 27 5 23 28 4 24 110277.50 119277.50 0.10 0.2000167 28 3 25 27 4 24 123349.10 123349.46 70.38 0.2000238 8 1 7 8 0 8 124087.46 124327.28 0.18 0.2000163 8 0 7 1 7 125389.58 125339.28 0.30 0.000179 20 4 16 21 3 19 125413.19 12543.2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   |                |                |   |     |     |   |     |     |     |     |     |    | 115  | 177. | 79           |     |        |   |       |       |        |    |
| 28 3 25 27 4 24 119277.65 119277.55 0.10 C.0000167 8 1 7 8 C E 123349.10 123349.45 0.18 0.000023E 8 C E 7 1 7 125369.58 125339.28 0.30 0.0001379 20 4 16 21 3 19 125413.19 125413.2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   |                | _              |   |     |     |   |     |     |     |     |     |    | 119  | 264, | 49           | -   | C-15   |   | 9.00  | :0026 | .5     |    |
| 8                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                |                |   |     |     |   |     |     |     |     |     |    | 119  | 277, | . 5 J        |     | 0.10   |   |       |       |        |    |
| 8 C 8 7 1 7 125389.52 125399.28 0.30 0.0001279 20 4 16 21 3 19 125413.19 125413.2 -0.01 0.0001279 40 3 37 41 2 40 127717.94 0.0000346 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 7 1 7 128313.85 128913.94 -0.09 0.0000254 6 2 4 27 1 27 1 27 144010.61 6 1 9 10 0 10 14916.44 144919.13 0.26 0.0000944 6 8 40 49 7 43 14368.82 144919.13 0.26 0.0000944 6 1 1 3 13 2 12 144914.85 148744.95 0.20 0.0000944 6 2 1 2 1 2 1 2 154046.43 154046.95 -0.10 0.0000944 6 2 1 2 2 1 2 154046.43 154046.95 0.23 0.000008 6 2 1 2 2 1 2 154046.43 154046.95 0.23 0.000008 6 2 1 2 2 1 2 1 154046.43 154046.95 0.23 0.000008 6 2 2 4 7 1 7 0.0000008 6 2 1 2 2 1 2 1 154046.43 154046.95 0.23 0.000008 6 2 2 4 7 1 7 1 2 165784.45 165784.33 0.12 0.000008 6 2 2 4 1 3 173485.53 173485.60 -0.10 0.0000394 6 2 2 2 5 1 5 167572.71 167572.81 -0.10 0.0000275 7 3 3 5 36 4 32 7 45 166584.65 0.0000094 7 3 3 4 1 6 3 6 167572.71 167572.81 -0.10 0.0000275 7 3 3 5 3 6 4 32 7 17412.46 166591.80 0.0000094 7 3 3 4 1 6 3 6 167572.71 167572.81 -0.10 0.000000000000000000000000000000                                                                                                                                                                                                                                                                                                                                                                                                                                           |   |                | _              | _ |     |     |   | 1   | 23  | 34  | • 9 | . 1 | Э  | 123  | 349  | . 4 ŝ        | -   | 0.38   |   |       |       |        |    |
| 20 4 16 21 3 19 125413.19 125413.2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                |   |     |     |   |     |     |     |     |     |    | 1243 | )E7. | 26           |     |        |   |       |       |        |    |
| 20                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                | _              |   |     |     |   |     |     |     |     |     |    | 125  | 359  | 28           |     | 0.30   |   |       |       |        |    |
| 127717.94   2.0000.008   3 3 1 32 2 4 28   128094.82   128313.95   128313.95   -0.17   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.132   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.0000.135   0.00000.135   0.00000.135   0.000000.135   0.00000.135   0.00000.135   0.00000.135   0.00000.135     |   |                |                |   |     |     |   | 1   | 25  | 41  | . 3 | . 1 | 9  | 125  | -13. | . 2 .        |     |        |   |       |       |        |    |
| 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   |                | -              | _ |     |     |   |     |     |     |     |     |    | 127  | 717. | 94           |     |        |   |       |       |        |    |
| 36 4 32 35 5 31 130954.81 130954.72                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   |                |                |   |     |     |   |     |     |     |     |     |    | 1290 | 94.  | . 99         | -   | 0.17   |   |       |       |        |    |
| 30 4 52 35 5 31 130954.81 130954.72                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   |                | -              |   |     |     |   |     |     |     |     |     |    | 128  | 213. | 94           | _   | 0.09   |   |       |       |        |    |
| 34                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                |   |     |     |   | 1   | 30  | 95  | 4   | • 5 | 1  | 1309 | 554. | . 72         |     | 0.09   |   |       |       |        |    |
| 13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                |   |     |     |   |     |     |     |     |     |    | 1323 | 885. | 37           |     |        |   |       | _     | -      |    |
| 19 4 16 20 3 17 136 860 24 136 860 24 2 136 860 24 2 136 860 24 2 1 27 1 27 12 140 767 61 0.000036 10 1 9 10 0 10 142175 12 142174 97 0.15 0.000236 10 1 9 10 0 10 142175 12 143 888 .02 143 866 95 0.0000015 11 13 13 2 12 144919 44 144919 .65 0.0000034 14 1 13 13 2 12 144919 44 144919 .65 0.0000034 12 3 9 13 2 12 148744 .85 14874 .95 -0.10 0.000094 12 3 9 13 2 12 148744 .85 151986 .17 0.0000034 13 3 3 3 3 4 4 3 0 153 724 .19 153 724 .00 0.000094 13 13 3 9 12 2 10 154046 .43 154046 .56 -0.13 0.000033 11 3 9 12 2 10 154046 .43 154046 .56 -0.13 0.000033 11 3 9 12 2 10 154046 .43 154046 .56 -0.13 0.000033 11 3 9 12 2 10 154046 .43 154046 .56 -0.13 0.000036 11 3 0.000036 11 12 11 12 0 12 165 784 .45 165 784 .39 0.000036 0.000008 164 772 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 772 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 772 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 772 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 72 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 72 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 72 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 72 9 156106 .80 155107 .17 -0.37 0.000015 0.000008 164 165 784 .33 165 784 .45 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 165 784 .35 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 186 .25 175 18                                 |   |                |                |   |     |     |   |     |     |     |     |     |    | 1330 | 40.  | 90           |     |        |   |       |       |        |    |
| 14                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                |   |     |     |   |     |     |     |     |     |    | 1363 | 39.  | 94           |     |        |   |       |       |        |    |
| 26 2 24 27 1 27 1 27 1 40767.61 1 40767.61 1 9 10 0 10 1 42175.12 1 42174.97 0.15 0.000036 1 48 4 4 4 40 1 49175.12 1 4388.02 0.0000252 0.0000253 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |   |                |                |   | _   |     |   | 1   | 3 £ | 96  | Ç   | • 2 | 4  | 1369 | ٠£٥. | 24           |     | ċ.     |   |       |       |        |    |
| 10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   | _              |                |   |     |     |   |     |     |     |     |     |    | 139: | 40.  | . ≈ 3        |     |        |   |       |       |        |    |
| 10 1 9 10 10 142175.12 142174.97 C.15 0.00002522 45 45 3 43 44 4 40 143 688.02 143 688.02 143 688.02 143 688.02 143 688.02 144 6910.65 144 6910.65 144 6910.65 144 6910.65 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 15 188 688.02 |   |                |                |   | _   |     |   |     |     |     |     |     |    | 140  | 67.  | 61           |     |        |   |       |       |        |    |
| 48       8       40       49       7       43       143£88.02       0.0000015       0.0000015       0.0000015       0.0000015       0.00000944       0.00000944       0.00000944       0.00000944       0.00000944       0.00000944       0.00000944       0.00000944       0.00000944       0.0000008       0.00000944       0.0000008       0.00000944       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.00000156       0.00000156       0.00000156       0.00000156       0.00000156       0.000000156       0.00000156       0.00000156       0.00000156       0.000000156       0.000000156       0.000000156       0.000000156       0.000000156       0.000000156       0.000000156       0.00000001       0.00000005       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.00000056       0.000000056       0.00000056       0.00000056       0.00000056                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |   | _              |                |   |     |     |   | 1   | 42  | 17  | 5   | - 1 | 2  | 1421 | 74.  | 97           |     | 0.15   |   |       |       |        |    |
| 14 36 38 5 33 144919.44 144919.19 0.26 0.0000944 12 3 9 13 2 12 144919.44 144919.19 0.26 0.0000944 12 3 9 13 2 12 142744.85 148744.95 -0.10 0.0000944 12 2 5 5 46 51 7 45 151986.17 0.000008 12 2 10 153724.19 153724.00 0.11 0.000033 11 3 9 12 2 10 154046.43 154046.56 -0.13 0.000038 11 3 9 12 2 10 154046.43 154046.56 -0.13 0.000038 11 3 9 12 2 10 154046.43 154046.56 -0.13 0.000038 13 3 6 29 34 5 29 156106.80 155107.17 -0.37 0.0000156 164772.09 0.0000008 12 11 12 0 12 165784.45 165784.33 0.12 0.000008 12 11 12 0 12 165784.45 165784.33 0.12 0.000038 165584.65 165584.65 165584.65 165584.65 165584.65 165584.65 16584.65 16584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584.65 166584. |   |                |                |   |     |     |   |     |     |     |     |     |    | 1435 | έê.  | .03          |     |        |   |       |       |        |    |
| 14 1 13 13 2 12 144919.44 144919.19 0.26 0.0000944  12 3 9 13 2 12 148744.85 148744.95 -0.10 0.0000944  52 5 46 51 7 45                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |   |                | -              |   |     |     |   |     |     |     |     |     |    | 1439 | 66.  | 95           |     |        |   |       |       |        |    |
| 12 3 9 13 2 12 148744.85 148744.95 -0.10 0.0000944.  52 6 46 51 7 45 153724.19 153724.09 0.0000068  35 3 33 34 4 30 153724.19 153724.09 0.00003333  13 9 12 2 10 154045.43 154046.56 0.23 0.00003333  33 6 29 34 5 29 156106.80 155107.17 -0.37 0.0000156  53 6 48 52 7 45 161099.24 0.0000008  40 7 33 41 6 36 164772.09 0.0000008  12 1 11 12 0 12 165784.45 165784.33 0.12 0.000008  12 1 11 12 0 12 165784.45 165784.33 0.12 0.0000016  43 3 41 42 4 38 165584.65 165584.65 0.0000001  47 8 40 48 7 41 170303.47 0.0000017  37 3 35 36 4 32 173485.53 175186.26 -0.07 0.0000017  37 3 35 36 4 32 173485.53 175186.26 0.0000059  18 4 14 19 3 17 175445.65 175465.71 -0.06 0.0000059  18 4 14 19 3 17 175445.65 175465.71 -0.06 0.0000059  17 5 43 46 6 40 183964.63 0.068 0.0000059  18 0 10 9 1 9 184378.31 184377.63 0.68 0.0000059  18 2 2 0 2 13 19 184788.84 184748.88 1 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |   |                |                |   |     |     |   |     |     |     |     |     |    | 1449 | 110. | 65           |     |        |   | 0.00  | CCCS  | 3      |    |
| 52       5       46       51       7       45       151986.17       0.3000008         35       3       33       34       4       30       153724.19       153724.32       0.11       0.30000141         26       5       21       27       4       24       153953.29       153953.06       0.23       0.0000333         31       3       9       12       2       10       154046.43       154046.56       -0.13       0.0000156         53       6       48       52       7       45       161099.24       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.0000008       0.00000008       0.00000008       0.00000008       0.00000008       0.000000008       0.000000008       0.000000008       0.000000008 </td <td></td> <td>-</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>0 - 26</td> <td></td> <td>0.00</td> <td>0094</td> <td>4</td> <td></td>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   | -              | -              |   |     |     |   |     |     | -   |     |     |    |      |      |              | 1   | 0 - 26 |   | 0.00  | 0094  | 4      |    |
| 15198617                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |   |                |                |   |     | _   |   | 1   | 4 8 | 74  | 4   | . 8 | 5  | 1487 | 44.  | 95           | -   | 0.10   |   | 0.00  | 0054  | 2      |    |
| 26 5 21 27 4 24 153953.29 153953.26 0.23 2.0c02333  11 3 9 12 2 10 154046.43 154046.56 -0.13 0.0c0056  33 6 28 34 5 29 156106.80 156107.17 -0.37 0.0000156  40 7 33 41 6 36 164772.99 0.0000056  3 1 3 2 0 2 164951.82 164951.80 0.02 0.0c00008  12 1 1 1 12 0 12 165784.45 165784.33 0.12 0.0003336  60 7 53 59 8 52 166801.40 0.0003336  60 7 53 59 8 52 166801.40 0.0003032  47 8 40 48 7 41 170303.47 0.00001  37 3 35 36 4 32 173485.53 173485.60 -0.07 0.000001  3 2 2 4 1 3 173485.53 175186.25 0.07 0.000059  18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059  18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000093  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000096                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |   | _              |                |   |     |     |   | _   |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                | _              |   |     | -   |   |     |     |     |     |     |    | 1537 | 24.  | , Ç e        |     | 2.11   |   | 0.36  | JJ14  | 1      |    |
| 33 6 29 34 5 29 156126.8C 155107.17 -0.37 G.0000156 53 6 48 52 7 45 161099.24 C.2000008 40 7 33 41 6 36 164772.09 C.2000008 3 1 3 2 0 2 164951.82 164951.80 0.02 C.200006 12 1 11 12 0 12 165784.45 165784.33 G.12 0.000136 43 3 41 42 4 38 165784.45 165784.33 G.12 0.0003336 60 7 53 59 8 52 166801.40 0.0003032 4 2 2 5 1 5 167572.71 167572.81 -0.10 0.0003021 47 8 40 48 7 41 170303.47 0.0003017 73 3 3 3 36 4 32 173485.53 173485.60 -0.07 0.0003017 25 5 21 26 4 22 175186.35 175186.28 0.07 0.0003024 25 5 21 26 4 22 175186.35 175186.28 0.07 0.000059 18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059 18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059 18 4 14 19 3 17 175445.65 178576.65 18 5 43 46 6 40 183964.83 0.068 0.0000059 10 0 10 9 1 9 184378.31 184377.63 0.68 0.0000059 10 0 10 9 1 9 184748.84 184748.881 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |   | -              |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     | 0.23   |   | 0.00  | 0033  | 3      |    |
| 53                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                | - |     |     |   |     |     |     |     |     |    |      |      |              | -   | 0.13   |   | 3.03  | -556  | 5      |    |
| 40 7 33 41 6 36 164772.09 C.0000008 3 1 3 2 0 2 164951.82 164951.80 C.02 C.000008 12 1 1 1 12 0 12 165784.45 165784.33 C.12 0.0003336 60 7 53 59 8 52 166801.40 0.0003336 60 7 53 59 8 52 166801.40 0.0003022 67 8 40 48 7 41 170303.47 0.000001 73 3 35 36 4 32 170303.47 0.000001 73 3 35 36 4 32 170303.47 0.000001 74 8 40 48 7 41 170303.47 0.000001 75 5 21 26 4 22 175186.53 175186.22 0.07 0.0000059 18 4 14 19 3 17 175445.65 175445.71 -C.06 0.000059 18 4 14 19 3 17 175445.65 175445.71 -C.06 0.0000059 18 4 14 19 3 17 175445.65 178576.65 178576.65 0.0000059 18 5 43 46 6 40 183964.83 0.68 0.0000059 18 6 7 5 43 46 6 40 183964.83 0.68 0.0000059 10 0 10 9 1 9 184378.31 184377.63 0.68 0.0000059 11 184748.84 184748.81 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |   | _              | -              |   |     |     |   | 1   | 5 5 | 13  | 6   | - 5 | C  |      |      |              | -   | 0.37   |   | 5.30  | 0015  | 6      |    |
| 3 1 3 2 0 2 164951.82 164951.80 0.02 0.00003336 12 1 11 12 0 12 165784.45 165784.33 C.12 0.0003336 43 3 41 42 4 38 165584.65 0.000032 4 2 2 5 1 5 167572.71 167572.81 -0.10 0.0000275 47 8 40 48 7 41 170303.47 37 3 35 36 4 32 173485.53 173485.60 -0.07 0.0000017 32 2 4 1 3 173485.53 173485.60 -0.07 0.0000029 18 4 14 19 3 17 175445.65 175465.71 -0.06 0.0000059 18 4 14 19 3 17 175445.65 175445.71 -0.06 0.0000059 18 4 14 19 3 17 175445.65 175445.65 0.0000059 18 4 14 19 3 17 175445.65 175445.65 0.0000059 19 1 9 184378.31 184377.63 0.68 0.0000059 10 0 10 9 1 9 184378.31 184377.63 0.68 0.0000059 11 184748.84 184748.81 0.03 0.0000396                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |   |                |                |   |     | _   |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 12 1 11 12 0 12 165784.45 165784.33                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   | ,              | -              |   |     |     |   | _   | ,   |     |     | _   | _  |      |      |              |     |        |   |       |       |        |    |
| 143 3 41 42 4 38 165784.33 C.12 C.00033336  60 7 53 59 8 52 166584.65 0.0003001  47 8 40 48 7 41 170303.47 0.0003017  37 3 35 36 4 32 173485.53 173485.65 -0.07 0.0003017  3 2 2 4 1 3 173485.53 173485.65 -0.07 0.0003017  18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059  18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059  41 3 39 40 4 36 178576.65 0.0000059  47 5 43 46 6 40 183964.63  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000093  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000093  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000099  12 2 2 0 21 3 19 184748.84 1847468.81 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |   | ÷              | , ,            |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.00  | 3101  | 5      |    |
| 165 84.65   16584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584.65   166584. | - |                |                |   |     |     |   | 1 : | 5 5 | 7.9 | 4   | • 4 | 5  |      |      |              | - 1 | 0.12   |   |       |       |        |    |
| 4 2 2 5 1 5 167572.71 167572.81 -0.10 0.0000275  47 8 40 48 7 41 170303.47 0.0000017  37 3 35 36 4 32 171412.46 0.0000124  25 5 21 26 4 22 175186.35 175186.26 -0.07 0.0000269  18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059  41 3 39 40 4 36 178576.65 0.0000059  41 3 39 40 4 36 183964.63 0.0000059  47 5 43 46 6 40 183964.63 0.0000059  10 0 10 9 1 9 184378.31 184377.63 0.68 0.0000035  10 0 10 9 1 9 184378.31 184377.63 0.68 0.000035  22 2 2 0 21 3 19 184748.84 184748.81 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | _ |                | _              |   | -   |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.00  | CJC3  | 2      |    |
| 47 8 40 48 7 41 170303.47 2.0000017 37 3 35 36 4 32 171412.46 0.000017 25 5 21 26 4 22 175186.35 173435.60 -0.07 0.0000459 18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059 18 3 37 38 4 34 180001.07 0.0000059 180001.07 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000059 183964.63 0.0000 |   |                |                |   |     |     |   |     |     |     | _   | _   | _  |      |      |              |     |        |   |       |       |        |    |
| 37 3 35 36 4 32 173485.53 173485.60 -0.07 0.0000124 25 5 21 26 4 22 175186.35 175186.28 0.07 0.000076459 21 4 1 9 3 17 175445.65 175445.71 -0.06 0.0000764 21 3 3 9 40 4 36 178576.65 178576.65 0.0000059 21 4 3 4 4 4 4 4 3 4 4 4 4 4 3 4 4 4 4 4                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   |                |                |   |     |     |   | 1 ( | 5 7 | 57  | 2   | • 7 | 1  |      |      |              | -:  | 3.13   |   | 0.30  | 0027  | 5      |    |
| 3 2 2 4 1 3 173485.53 173485.60 -0.07 0.0000269 25 5 21 26 4 22 175186.35 175186.28 0.07 0.0000459 18 4 14 19 3 17 175445.65 175445.71 -0.06 0.000059 41 3 39 40 4 36 178576.65 0.0000059 47 5 43 46 6 40 183964.83 0.00001.07 0.0000035 10 0 10 9 1 9 184378.31 184377.63 0.68 0.000093 22 2 20 21 3 19 184748.84 1847468.81 0.03 0.0000968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |   |                | -              |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 18 4 14 19 3 17 175485.63 173485.6C -0.07 0.0000459 184 14 19 3 17 175445.65 175445.71 -0.06 0.000059 0.000059 0.000059 0.000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.0000059 0.00000 |   |                |                |   |     |     |   |     |     |     |     |     | _  |      |      | -            |     |        |   | 0.33  | 3612  | 4      |    |
| 18 4 14 19 3 17 175445.65 175445.71 -C.06 C.CGGC7C4 41 3 39 40 4 36 178576.65 175445.71 -C.06 C.CGGC7C4 47 5 43 46 6 40 180001.07 C.CGG0093 10 0 10 9 1 9 184378.31 184377.63 0.68 0.0002972 22 2 20 21 3 19 184748.84 184748.81 0.03 0.0003968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 41 3 39 40 4 36 178576.65 0.C0C059 39 3 37 38 4 34 180001.07 C.CC00093 47 5 43 46 6 40 183964.63 0.C0C055 10 0 10 9 1 9 184378.31 184377.63 0.68 0.C0C2972 22 2 20 21 3 19 184748.84 184746.81 0.03 0.C0C0966                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |   | -              |                |   |     |     |   |     |     |     |     |     |    |      |      |              | ;   | 0.07   |   | 0.00  | C 545 | ç      |    |
| 39 3 37 28 4 34 180001.07 0.000093 47 5 43 46 6 40 183964.63 0.0000255 10 0 10 9 1 9 184378.31 184377.63 0.68 0.0002972 22 2 20 21 3 19 184748.84 184748.81 0.03 0.0003968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |   |                |                |   |     |     |   | 1   | ( 5 | 44  | 5   | • 6 | >  |      |      |              | -(  | 0.06   |   |       |       |        |    |
| 180001.07                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |   |                |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.00  | 0005  | ç      |    |
| 1C 0 10 9 1 9 184378.31 184377.63 0.68 0.0002972 22 2 20 21 3 19 184748.84 184746.81 0.03 0.0003968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |   | -              |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 22 2 20 21 3 19 184748.84 184748.81 0.03 0.0003968                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |   | -              |                |   |     |     |   | , . |     |     |     | _   |    |      |      |              |     |        |   |       |       |        |    |
| 32 6 26 33 5 70 18555 01 104/40-01 U-U3 G-OCCU96E                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |   | -              |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   |       |       |        |    |
| 0 20 33 3 29 100000091 185557.04 -0.13 C.0C00244                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |   | _              |                |   |     |     |   |     |     |     |     |     |    |      |      |              |     |        |   | 0.00  | 0396  | ŧ      |    |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |   | ,              | - 0            |   | و   | 4 7 |   | 1 6 | 2)  | ככ  | ۰ ۰ | . y | ī  | 1622 | 57.  | U4           | -(  | 1.13   |   | C.0C  | 0024  | 4      |    |

Table XXXII. (Continued)

|          | per          |          | ower<br>tate                  | Obs.<br>Frequency                       | Calc.                  | Obs           | Intensity 296°K 1C-17 cm-1/ |
|----------|--------------|----------|-------------------------------|-----------------------------------------|------------------------|---------------|-----------------------------|
|          |              | ์<br>J   |                               | MHz                                     | Frequency              | MHz           | Molec/cm <sup>2</sup>       |
|          | KA KC        |          | K <sub>A</sub> K <sub>C</sub> |                                         |                        |               |                             |
| 41       | 4 39         | 40       | 5 35                          |                                         | 187132.45              |               | 0.0000102                   |
| 42       | 3.39         | 43<br>29 | 2 42                          |                                         | 197633.43              |               | 0.0053011                   |
| 25       | 7 33         | 40       | 1 29                          |                                         | 187985.35              |               | 0.0000045                   |
| 39<br>17 |              | 18       | 6 34<br>3 15                  | 100001 00                               | 190574.46<br>193351.17 |               | 0.0000092                   |
| 14       | 4 14 1 13    | 14       | 3 14                          | 193351.30                               | 195430.23              | 0.13          | 3.0000862                   |
| 10       | 3 7          | 11       | 2 10                          | 195430.51<br>195721.19                  | 195721.27              | J.31<br>-C.08 | 0.0004254<br>0.0000822      |
| 46       | 8 38         | 47       | 7 41                          | 192721019                               | 197536.21              | -0.08         | 0.0000027                   |
| 30       | 3 27         | 29       | 4 26                          |                                         | 199384.77              |               | 0.0000535                   |
| 53       | 9 45         | 54       | 9 46                          |                                         | 203367.90              |               | 3.0000006                   |
| 38       | 4 34         | 27       | 5 33                          |                                         | 203452.87              |               | 0.0000198                   |
| 24       | 5 19         | 25       | 4 22                          |                                         | 206131.95              |               | 3.0000669                   |
| 46       | 5 41         | 45       | 6 40                          |                                         | 207482.22              |               | 0.0000354                   |
| 5        | 1 5          | 4        | 0 4                           | 208642.44                               | 208642.33              | 0.11          | 0.0002407                   |
| 31       | 6 26         | 32       | 5 27                          | 210423.10                               | 210423.14              | -0.04         | 0.0003345                   |
| 2        | 5 0          | 3        | 1 3                           |                                         | 210762.38              |               | 0.0000131                   |
| 9        | 3 7          | 10       | 2 8                           | 210803.80                               | 210903.35              | 0.44          | 0.0000870                   |
| 16       | 1 15         | 15       | 2 14                          |                                         | 214955.48              |               | 0.0002320                   |
| 5.5      | 6 50         | 54       | 7 47                          |                                         | 215129.44              |               | 0.0000009                   |
| 54       | 6 48         | 53       | 7 47                          |                                         | 215483.75              |               | 0.0000011                   |
| 3.5      | 7 31<br>8 38 | 39       | 6 34<br>7 39                  |                                         | 218120.19              |               | 0.0000138<br>0.0000041      |
| 45<br>43 | 4 40         | 46<br>42 | 5 37                          |                                         | 223900.19              |               | 0.0000105                   |
| 16       | 4 12         | 17       | 3 15                          |                                         | 226054.12              |               | 0.0001163                   |
| 59       | 4 56         | 58       | 5 53                          |                                         | 228322.59              |               | 0.0000002                   |
| 23       | 5 19         | 24       | 4 2C                          |                                         | 229574.88              |               | 0.0000869                   |
| 16       | 1 15         | 16       | 0 16                          |                                         | 231281.25              |               | 0.0005224                   |
| 49       | 5 45         | 48       | 6 42                          |                                         | 232984.27              |               | 0.0000039                   |
| 16       | 2 14         | 16       | 1 15                          |                                         | 235709.64              |               | 0.0007527-                  |
| 14       | 2 12         | 14       | 1 13                          |                                         | 237146.00              |               | 0.0007264                   |
| 30       | 6 24         | 31       | 5 27                          |                                         | 238431.95              |               | 0.0000483                   |
| 18       | 2 16         | 18       | 1 17                          |                                         | 239093.03              |               | 0.0007685-                  |
| 30       | 2 28         | 31       | 1 31                          |                                         | 240905.00              |               | 0.0000049                   |
| 12       | 2 10         | 12       | 1 11                          | 2/0/52 70                               | 242318-60              | 0.10          | 0.0006839                   |
| 12<br>37 | 0 12         | 11<br>35 | 1 11 6 32                     | 243453.70                               | 243453.57<br>244147.00 | 0.13          | 0.0006180-<br>0.0000195     |
| 8        | 3 5          | 9        | 6 32<br>2 8                   | 244158.04                               | 244158.54              | -0.5C         | 0.0001006                   |
| 15       | 4 12         | 16       | 3 13                          | 247761.22                               | 247761.85              | -0.63         | 0.0001372                   |
| 20       | 2 18         | 20       | 1 19                          | 245183.32                               | 248183.14              | 0.18          | 0.0007787                   |
| 7        | 1 7          | - 6      | 0 6                           | • • • • • • • • • • • • • • • • • • • • | 249788.46              |               | 0.0004537                   |
| 10       | 2 8          | 10       | 1 9                           |                                         | 249961.90              |               | 0.0006201~                  |
| 44       | 8 36         | 45       | 7 39                          |                                         | 250731.11              |               | 0.0000061                   |
| 44       | 3 41         | 45       | 2 44                          |                                         | 252324.69              |               | 0.0000012                   |
| 45       | 4 42         | 44       | 5 39                          |                                         | 256885.65              |               | 0.0000094                   |
| 22       | 5 17         | 23       | 4 2C                          |                                         | 258202.06              |               | 0.0001141                   |
|          | 2 6          | 8        | 1 7                           |                                         | 258716.10              |               | 0.0005325                   |
| 24       | 2 22         | 23       | 3 21                          |                                         | 262858.07              |               | 0.0001877<br>0.0007858-     |
| 22       | 2 20         | 22<br>30 | 1 21<br>5 25                  |                                         | 263592.36<br>263886.06 |               | 0.0007898                   |
| 29<br>57 | 4 54         | 56       | 5 51                          |                                         | 264325.31              |               | 0.0000005                   |
| 7        | 3 5          | 8        | 2 6                           |                                         | 264926.05              |               | 0.0000997                   |
| 6        | 2 4          | 6        | 1 5                           |                                         | 267266.54              |               | 0.0004211                   |
| 57       |              | 56       | 7 49                          |                                         | 268319.85              |               | 0.0000009                   |
| 36       | 7 29         | 37       | 6 32                          |                                         | 271092.80              |               | 0.0003271                   |
| 18       | 1 17         | 18       | 0 18                          |                                         | 273050.63              |               | 0.0006176-                  |
| 4        | 2 2          | 4        | 1 3                           |                                         | 274478.42              |               | 0.0002866                   |
| 14       | 4 10         | 15       | 3 13                          | 276923.78                               | 276923.62              | 0.16          | 0.0001653                   |
| 43       | e 36         | 44       | 7 37                          |                                         | 277042.33              |               | 0.0000087                   |
| 51       | 5 47         | 50       | 6 44                          |                                         | 279332.66              |               | 0.0000038                   |
| 48       | 5 43         | 47       | 6 42                          | 3704 ** 00                              | 279467.41<br>279485.78 | 0.12          | 0.0000069<br>0.0001209      |
| 2        | 2 0          | 2        | 1 1                           | 279485.90                               | 217403010              | A + 15        | 310001207                   |

Table XXXII. (Continued)

|    | ppe  |                |      | OVE |                | Obe.      | Calc.     | Obs<br>Calc. | Intensity<br>296°K cm-1 |
|----|------|----------------|------|-----|----------------|-----------|-----------|--------------|-------------------------|
|    | tate |                |      | tet |                | Frequency | Frequency |              |                         |
| J  | Kλ   | K <sub>C</sub> | J    | ĸ,  | K <sub>C</sub> | 161 z     | Miz       | MHz          | Molec/cm <sup>2</sup>   |
| 32 | 3    | 29             | 31   |     | 29             | 279893.48 | 279893.03 | 0.45         | 0.0000892               |
| 40 | 4    | 36             | 39   | 5   | 35             |           | 280994.06 |              | C.0000259               |
| 47 | 4    | 44             | 46   | 5   | 41             |           | 281958.91 |              | 0.0000075               |
| 56 | 6    | 50             | 55   | 7   | 49             |           | 282129.63 |              | 0.0000013               |
| 21 | 5    | 17             | 22   | 4   | 18             | 282837.66 | 282837.04 | 0.62         | 0.0001411               |
| 18 | 1    | 17             | 17   | 2   | 16             | 286087.20 | 286087.52 | -5.32        | 3.3334445               |
| 24 | 2    | 22             | 24   | 1   | 23             | 286156.50 | 286156.31 | C.19         | 0.0007893~              |
| 3  | 2    | 2              | 3    | 1   | 3              | 286294.20 | 286294.71 | -0.51        | 0.0002129               |
| 9  | 1    | 9              | 8    | 0   | - 8            | 288958.95 | 288959.01 | -0.06        | 0.0007454               |
| 55 | 4    | 52             | 54   | 6   | 49             |           | 289389.72 |              | 0.0000011               |
| 28 | 6    | 22             | 29   | 5   | 25             |           | 290974.95 |              | 0.0000841               |
| 5  | 2    | 4              | 5    | 1   | 5              | 293171.25 | 293171.29 | -0.04        | 0.0003722               |
| 6  | 3    | 3              | 7    | 2   | 6              |           | 293548.42 |              | 0.0003961               |
| 35 | 7    | 29             | 36   | 6   | 30             |           | 297173.58 |              | 0.0000365               |
| 32 | 2    | 30             | 33   | 1   | 33             |           | 298601.92 |              | 0.0000050               |
| 49 | 4    | 45             | 4.8  | 5   | 43             |           | 298796.19 |              | 0.0000054               |
| 13 | 4    | 10             | 14   | 3   | 11             | 300685.80 | 300685.24 | 0.56         | 0.0001=56               |
| 14 | ٥    | 14             | _ 13 | 1   | 13             | 301812.48 | 301812.76 | -3.28        | 3-0010742*              |
| 7  | 2    | 6              | 7    | 1   | 7              | 303163.20 | 303164.85 | -1.60        | 0.0005187-              |
| 53 | 4    | 50             | 5.2  | 5   | 47             |           | 303289.78 |              | 0.0000023               |
| 42 | 8    | 34             | 43   | 7   | 37             |           | 303573.61 |              | 3.0000121               |
| 51 | 4    | 48             | 50   | •   | 45             |           | 306222.56 |              | <pre>6.0000035</pre>    |
| 20 | 5    | 15             | 21   | 4   | 18             | 310062.72 | 310063.36 | -3.64        | 0.0001730               |
| 26 | 2    | 24             | 26   | 1   | 25             | 315874.47 | 315974.94 | -0.47        | J 7272°                 |
| 9  | 2    | 8              | 9    | 1   | 9              |           | 316327.04 |              | 0.0006555               |
| 27 | 6    | 22             | 28   | 5   | 23             |           | 316681.45 |              | 0.0001066               |
| 5  | 3    | 3              | 6    | 2   | 4              |           | 317195.13 |              | 0.00000#11              |
| 20 | 1    | 19             | 20   | 2   | 20             |           | 319996.27 |              | 0.0007037               |

new results are presented here as Tables XXXIII and XXXIV. Table XXXIII is for rotational lines of  $0_3$  in the  $\nu_1$  (ground) state and Table XXXIV is for rotational lines of  $0_3$  in the  $\nu_3$  (ground) state.

A spacecraft instrument was developed for the measurement of the mm characteristics of ozone by personnel at the Ewin Knight Company. They chose a line at 101.7 GHz for radiometrically measuring the emitted radiation of the air mass beneath the spacecraft. Reference 75 describes the design of the instrument from concept phase, laboratory phase, through a balloon-mounted instrument, and to a spacecraft flight instrument. Canton, Manneller et al. 8 define the ozone absorption coefficient as:

$$\alpha_{OZ} = \frac{A_1 e^{-A_S/T}}{T^{5/2}} NO_3 \cdot v^2 \left[ \frac{\Delta v}{(v-A_3)^2 + (\Delta v)^2} + \frac{\Delta v}{(v+A_3)^2 + (\Delta v)^2} \right]$$

where  $\Delta v = \left[ \left[ A_4 PT^{-1/2} \right]^2 + \left[ A_5 T^{1/2} \right]^2 \right] 1/2$ 

For the 101.7 GHz transition,

$$A_1 = 1.2 \times 10^{-24} \text{km}^{-1}$$
;  $A_2 = 13.1^{\circ}\text{K}$ ;  $A_3 = 101.7368 \times 10^4 \text{Hz}$   
 $A_4 = 5.28 \times 10^7 \text{Hz} (^{\circ}\text{K}^{1/2}) \text{ mm}^{-1}$ ,  $A_5 = 7.31 \times 10^3 (^{\circ}\text{K})^{-1/2}$ 

These constants  $A_1$ ,  $A_2$ ,  $A_3$ ,  $A_4$  and  $A_5$  are from Gora, and Townes and Schawlow. A comparison of measured absorption profile data taken with use of the instrument described in Ref. 75 and calculated absorption profiles based on the above equation is shown in Fig. 49.

Table XXXIII. Rotational Lines of  $^{16}\mathrm{O}_3$  in the  $\nu_1$  State (Data from Ref. 74)

| lower     | upper                             | calc. (MHz) | Obs. (MHz) |
|-----------|-----------------------------------|-------------|------------|
| J K_1 K+1 | J K <sub>-1</sub> K <sub>+1</sub> |             |            |
| 1 1 1     | 2 0 2                             | 43059.674   | 43059.910  |
| 4 0 4     | 3 1 3                             | 10518.195   | 10518.320  |
| 606       | 5 1 5                             | 66332.847   | 66333.070  |
| 726       | 8 1 7                             | 56322.535   | 56322.620  |
| 10 2 8    | 11 1 11                           | 60569.033   | 60569.120  |
| 12 2 10   | 13 1 13                           | 36254.758   | 36254.790  |
| 14 2 12   | 15 / 15                           | 19215.805   | 19215.910  |
| 15 3 13   | 16 2 14                           | 36281.384   | 36281.440  |
| 16 2 14   | 17 1 17                           | 10272.456   | 10272.310  |
| 16 3 13   | 17 2 16                           | 60127.209   | 60127.340  |
| 18 3 15   | 19 2 18                           | 20308.969   | 20309.340  |
| 18 2 16   | 17 3 15                           | 29143.551   | 29143.300  |
| 18 2 16   | 19 1 19                           | 9669.776    | 9669.570   |
| 22 4 18   | 23 3 21                           | 77996.535   | 77996.306  |
| 29 5 25   | 30 4 26 .                         | 69900.455   | 69901.401  |
| 25, 2 24  | 24 3 21                           | 69297.245   | 69296.890  |
| 12 1 11   | 11 2 10                           | 71611.790   | 71611.625  |
| 23 2 22   | 22 3 19                           | 45505.101   | 45504.288  |
| 29 3 27   | 28 4 24                           | 60198.237   | 60198.452  |
| 30 5 25   | 31 4 28                           | 54788.390   | 54788.333  |
| 23 4 20   | 24 3 21                           | 23786.015   | 23786.275  |
| 24 4 20   | 25 3 23                           | 29888.538   | 29889.336  |

Table XXXIV. Rotational Lines of  $^{16}\mathrm{O}_3$  in the  $^{\vee}_3$  State (Data from Ref. 74)

| lower       | upper   | calc. (MHz) | Obs. (MHz) |
|-------------|---------|-------------|------------|
| J K-1 K+1 - | J K K 1 |             |            |
| 2 1 2       | 3 0 3   | 15664.591   | 15664.570  |
| 503         | 4 1 4   | 39099.335   | 39099.200  |
| 8 2 7       | 8 1 9   | 18673.215   | 18673.010  |
| 11 1 10     | 10 2 9  | 46687.931   | 46688.170  |
| 11 2 9      | 12 1 12 | 59371.426   | 59371.480  |
| 13 2 11     | 14 1 14 | 45388.259   | 45388.270  |
| 14 3 12     | 15 2 13 | 56314.345   | 56313.970  |
| 15 2 13     | 16 1 16 | 40733.576   | 40733.370  |
| 17 2 15     | 16 3 14 | 10705.554   | 10705.730  |
| 17 2 15     | 18 1 13 | 45990.313 . | 45989.990  |
| 17 3 14     | 18 2 +7 | 45322.044   | 45321.930  |
| 19 2 17     | 20 1 20 | 61286.619   | 61286.730  |
| 19 3 16     | 20 2 19 | 12594.171   | 12593.910  |
| 29 5 24     | 30 4 27 | 71318.362   | 71317.572  |
| 23 4 19     | 24 3 22 | 51441.035   | 51441.095  |
| 25 3 22     | 24 4 21 | 28460.893   | 28460.788  |
| 30 3 29     | 29 4 25 | 70678.174   | 70677.947  |
| 30 5 20     | 31 4 27 | 21292.446   | 21292.100  |

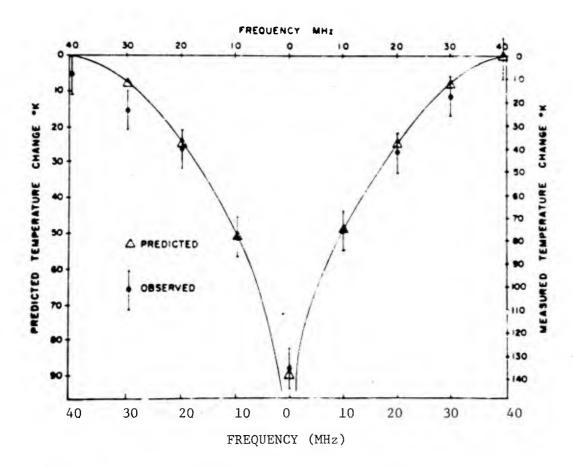


Fig. 49. Measured and Predicted Ozone Absorption Profiles Normalized to Equal Amplitude for a Background Sun Temperature of 2500 °K (Data from Ref. 75)

### 2.6 Attenuation and Scattering by Atmospheric Aerosols

First, let us consider just what constitutes an aerosol.

Depending on where you are on the earth (or up in the stratosphere) an aerosol could mean various things.

Lendberg and Gillespie  $^{79}$  at White Sands, New Mexico, collected dust samples and ran them through a fractionated dust stage to sort them out for sizes. They found that the particle composition varies as a function of their sieve pore size that allowed these dust particles to pass. The result is shown in Table XXXV. They measured the imaginary index of refraction of these dust sample stages from 0.3  $\mu$ m to 1.7  $\mu$ m and showed that there was a vast difference in this quantity with dust size.

The major reference on atmospheric dust and aerosols has to be the conference proceedings  $^{80}$  "Atmospheric Aerosols; Their Optical Properties and Effects"; this conference was held at Williamburg, Virginia, December 13-15, 1976. K. Bullrich and G. Hänel  $^{80}$  presented (Paper MH1) data on particle size distributions for different types of aerosols. Their distributions are shown in Fig. 50. They also showed that the humidity has a definite impact on the optical characteristics. The mass absorption coefficient  $k/\rho$  vs wavelength (1.0  $\mu m$  to  $10.0~\mu m$ ) is given in Fig. 51 for 3 levels of humidity. One would expect that the humidity will also affect the absorption coefficient of aerosols at longer wavelengths.

- H. E. Gerber et al. in paper TUA6  $^{80}$ , presented a paper on "Laser Transmissions through a Concentrated Aerosol." They used a centrifuge-type device to concentrate aerosols to simulate a light path through the cell of up to 1 km. They measured data on the transmission as a function of time for a concentrated oil aerosol and for 0.63, 1.06, 3.8 and 10.6  $\mu$ m wavelength radiation. Their results are given in Fig. 52.
- E. P. Shettle and F. E. Voltz,  $^{80}$  in their paper MC14 "Optical Constants for a Meteoric Dust Aerosol Model" calculated the attenuation

Table XXXV. Optically-Significant Components of Size Fractionated Dust Samples (Data from Ref. 79)

|                            |   |   | S | Stage 1 | numbe | er              |   |            |
|----------------------------|---|---|---|---------|-------|-----------------|---|------------|
| Component                  | 7 | 6 | 5 | 4       | 3     | 2               | 1 | 0          |
| Clay minerals <sup>b</sup> |   |   | X | X       | X     | X               | Y | Y          |
| Quartz                     |   |   | X | X       | X     |                 | X | X          |
| Calcite                    |   |   | _ | X       | X     | $\widetilde{X}$ | X | $\ddot{x}$ |
| Gypsum                     |   |   | X | X       | _     |                 |   |            |
| Ammonium sulfate           | X | X | _ |         |       |                 |   |            |
| Carbon <sup>c</sup>        | X | X | _ |         |       |                 |   |            |

 $<sup>^</sup>a$  The X indicates that the material was present; the symbol — indicates that the material was detectable but present in much lower concentration.

<sup>b</sup> Specifically montmorillonite, illite, and kaolin group clays.

The presence of carbon was estimated by other means, as discussed in text.

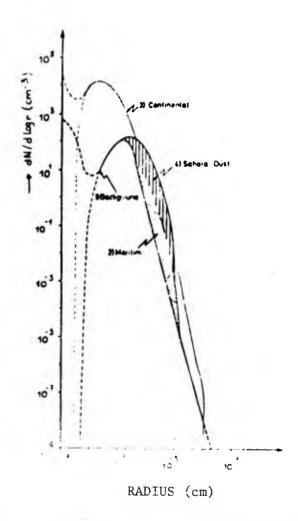


Fig. 50. Aerosol Particle Size Distributions as Measured by Bullrich and Hänel (Ref. 80) for Continental, Sahara Dust and Maritime Hazes

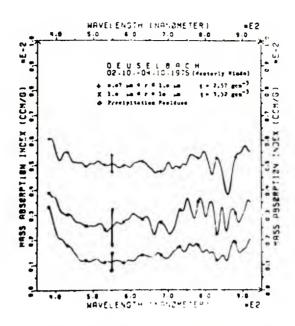


Fig. 51. Mass Absorption Cross Section,  $k/\rho$ , of Aerosols at Three Different Humidities (Data from Ref. 80)

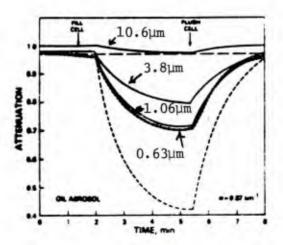


Fig. 52. Attenuation of Laser Radiation by Oil Aerosols as a Function of Time (Data from Ref. 80)

coefficient for a set of samples of meteoric dust whose reflectivity had been measured in the spectral region 2.5 to 40  $\mu m$ . A 9-oscillator model was fitted to these measurements using a nonlinear least squares optimization of his sets of equations, which were:

$$Ra = \frac{(n-1)^2 + k^2}{(n+1)^2 + k^2} = reflectivity$$

$$n^{2} - k^{2} = A_{0} + \sum_{j} \frac{2A_{j}(v_{j}^{2} - v^{2})}{(v_{j}^{2} - v^{2})^{2} + \gamma_{j}^{2}v^{2}}$$

$$nk = \sum_{j} \frac{A_{j} \gamma_{j} \nu}{(\nu_{j}^{2} - \nu^{2})^{2} + \gamma_{j}^{2} \nu^{2}}$$

 $v_i$  = frequency of jth oscillator

 $A_{i} = oscillator strength$ 

 $\gamma_i$  = damping constant or band width

Results of their calculation of the aerosol attenuation coefficient are show in Fig 53.

James W. Fitzgerald at the Optical Submillimiter Atmospheric Propagation Conference 1 presented a paper on "Effect of Relative Humidity on Aerosol Size Distribution and Visibility-Modeling Studies." Fitzgerald derived a relationship between the relative humidity and the equilibrium size of an aerosol particle that had an insoluble core with a soluble covering in the form of a pure salt. The equilibrium saturation ratio, S, is described by

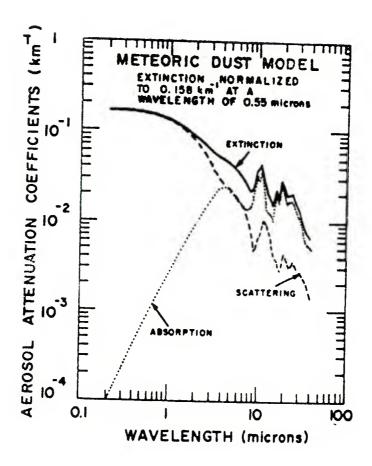


Fig. 53. Scattering, Absorption and Extinction Coefficients vs Wavelength for Meteoric Dust Model (Data from Ref. 80)

$$S = \exp \left[ \frac{2\sigma'}{r\rho' R_{v}^{T}} \right] \left[ 1 + \frac{i \epsilon \rho_{d} M_{w} r_{d}^{3}}{M_{s} \{ \rho' (r^{3} - r_{d}^{3} (1 - \epsilon)) - \epsilon \rho_{d} r_{d}^{3} \}} \right]^{-1}$$

where

S = equilibrium saturation ratio (% relative humidity divided by 100),

r = equilibrium radius of the particle (solution droplet)

 $r_d$ ,  $\rho_d$  = radius and density of the dry particle,

 $M_{LJ}$  = molecular weight of water,

 $\mathbf{M}_{\mathbf{S}}^{}$  = molecular weight of the soluble component,

i = Van't Hoff factor,

 $R_{v}$  = specific gas constant of water vapor,

 $\epsilon$  = mass fraction of the soluble material on the dry particle

 $\sigma'$ ,  $\rho'$  = surface tension and density of the aqueous salt solution.

On a cruise off the coast of Nova Scotia, a sea-fog aerosol size distribution was measured, and compared with calculations obtained from the above model. Results of the calculations and measurements are shown in the next two figures. The first, Fig. 54, is for 10 km downwind of the formation edge of a fog, and the second, Fig. 55, is for 25 km downwind of the fog formation line. These are models that should prove useful for millimeter wave studies on sea-fog aerosols.

It is apparent that some calculations and measurements of radiation scattering by aerosol have been made for wavelengths up to 30  $\mu m$  in the IR region, but no measured data were found in the .1 mm to 1 cm region.

Information on the aerosol index of refraction needs to be generated and measurements made in the submillimeter region. Experimentally, the Fourier transform spectrometer could be used to determine the complex index of refraction of a number of different types of particles.

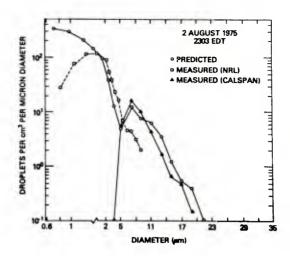


Fig. 54. Comparison of Observed and Predicted Droplet Size Distributions at a Point 10 km Downwind of the Forming Edge of the Fog on 2 August 1975 (Data from Ref. 81)

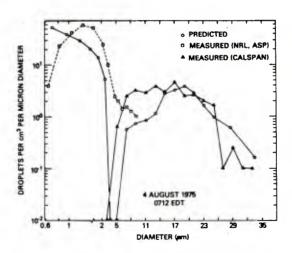


Fig. 55. Comparison of Observed and Predicted Droplet Size Distributions at a Point 25 km Downwind of the Forming Edge of the Fog of 4 August 1975 (Data from Ref. 81)

Some of the types of aerosol particles that need to be considered when making index of refraction measurements are:

| Soluble Materials               | Non Soluble Materials                                     |
|---------------------------------|-----------------------------------------------------------|
| $(NH_4)_2 SO_4$                 | Clay minerals (montmorillonite, illite, and kaolin group) |
| NH <sub>4</sub> NO <sub>2</sub> | Quartz                                                    |
| NaNO <sub>3</sub>               | Calcite                                                   |
| NH <sub>L</sub> C1              | Gypsum                                                    |
| CaCl <sub>2</sub>               | Carbon                                                    |
| NaBr                            | Basalt                                                    |
| NaCl                            | ·                                                         |
| $M_9C1_2$                       |                                                           |
| LiCl                            |                                                           |
| ZnC1 <sub>2</sub>               |                                                           |
| P <sub>2</sub> O <sub>5</sub>   |                                                           |

# 2.7 Attenuation and Scattering by Battlefield Dusts and Smokes

The literature relating to the attenuation and scattering properties of battlefield dust and smokes in the millimeter and submillimeter wave region in very sparse.

G. Tinsley and T. Cosden  $^{\mbox{\footnotesize 82}}$  measured the particle size distribution of some machine-gun smoke. The particle distributions shown in Fig. 56 are one-minute averages. The "1514" time is before the smoke reached the particle counter. At 1518, the smoke had largely passed. They calculated the extinction in this smoke for 3.9  $\mu m$  radiation. E. W. Stuebing, F. O. Verderame et al., in paper 14 of the conference 81, presented a talk on the "Nature of Gun Smoke and Dust Observation." They developed the data listed in Table XXXVI which gives the products of nitro-cellulose combustion from a 30 mm Rarden cannon round. Stuebing et al. also modeled an obscuring smoke cloud which they assumed was due to a combination of gun smoke and the dust created from the ground by the muzzle blast of the cannon. calculated the optical densities at 0.5, 1.06 and 10.6  $\mu m$  wavelengths that were provided by the smoke produced by the firing of a  $30\ \mathrm{mm}$  Rarden cannon from measured transmission vs time measurements for those wavelengths. The optical density is defined by the equation  $T = 0.1^{D}$  where T is the measured transmission and D is the optical density. Figures 57 and 58 show the measured optical density vs time for the three wavelengths used in the measurements. Also shown in these figures are the optical densities obtained from model calculations. The transmission through the smoke has two minima: the first appears to result from the smoke produced by the products of nitrocellulose combustion (which was modeled as water) and the second results from the dust created from the ground. The comparison between the model results and the measured densities for  $\lambda$  = 0.53  $\mu m$  appears to be good. Although the data in Figs. 57 and 58 are for wavelengths in the visible and near infrared, the models giving the "smoke" particle size distribution vs time could be used with Mie theory to determine absorption, scattering and extinction coefficients for millimeter and submillimeter wavelength radiation.

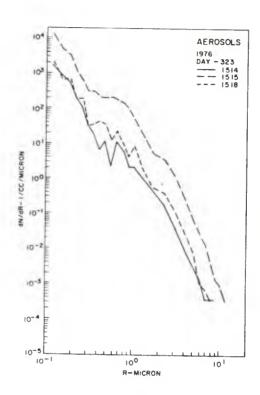


Fig. 56. Measured Particle Size Distributions for Machine-Gun Smoke; time = 1515 (Data from Ref. 82)

Table XXXVI. Products of Nitrocellulose Combustion. (from Data in Paper 14 of Ref. 81)

### Major Products

CO,  $\text{CO}_2$ ,  $\text{H}_2$ ,  $\text{H}_2\text{O}$  (Water Gas Equilibrium)

N<sub>2</sub>

### Major Minor Products

 $CH_4$ ,  $NH_3$ 

## Minor Minor Products

C, K<sub>2</sub>O, SnO<sub>2</sub>, Na<sub>2</sub>O, BaO

(Pb, Sb, Si, Zr, Ca, A1)

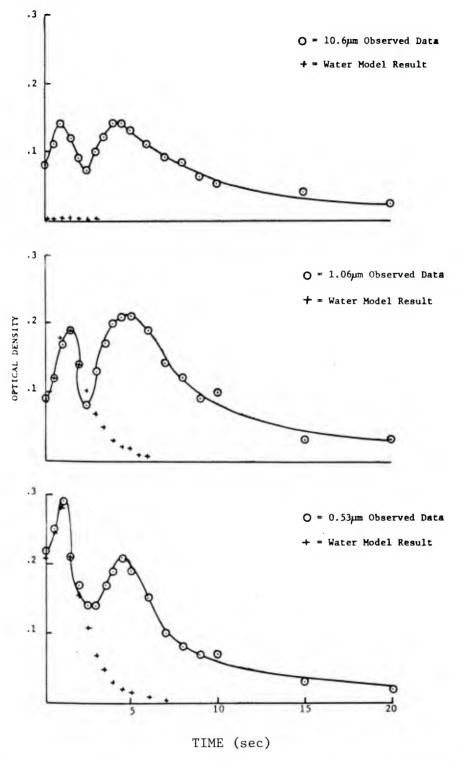


Fig. 57. Measured and Calculated Optical Density vs Time After Firing of Cannon (from Ref. 81)

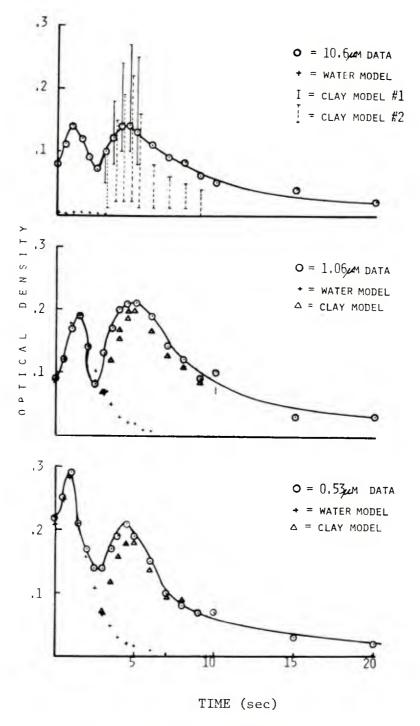


Fig. 58. Measured and Calculated Optical Density due to Gun Smoke and Dust Model (from Ref. 81)

Alan Downs in Ref. 44 has reviewed the transmission of optical radiation through smoke and dust. The transmission through several smokes for visible and 10.6 µm wavelength laser light as a function of the particle concentration is shown in Fig. 59. Further work of optical transmission in smokes is alluded to in Downs' report. Downs also reported data on transmission versus time for visible (.4 - .7µm), near IR (.7 - 1.1 µm) and IR (3-5µm and 8-14µm) radiation through 105 mm HC round caused smoke cloud (presented here as Fig. 60), a 60 mm WP morter caused smoke cloud presented here as Fig. 61) and a fog oil smoke cloud (presented here as Fig. 62). The latter fog oil cloud was produced by 9-M-7 fog oil smoke pots. Downs reported that when 94 GHz and 140 GHz radar beams were transmitted through each of these clouds, the resulting signals showed no attenuation. Table XXXVII lists the time in minutes that each of the visible and IR systems could "see" the smoke phenomena that were described in the previous three figures.

Downs also presented data on transmissions through a dust cloud that were collected at Fort Sill during smoke tests. The transmission through the cloud is shown here in Fig. 63. The reduction in transmission during the 0-20 second time period is due to the smoke and the cause for the transmission loss in the 123 second -200 second time period is due to dust.

Downs also reported on another dust cloud experiment. The results obtained from the experiment are shown in Fig. 64. Downs reported that there was  $\underline{no}$  apparent attenuation of 94 GHz and 140 GHz radar by the dust.

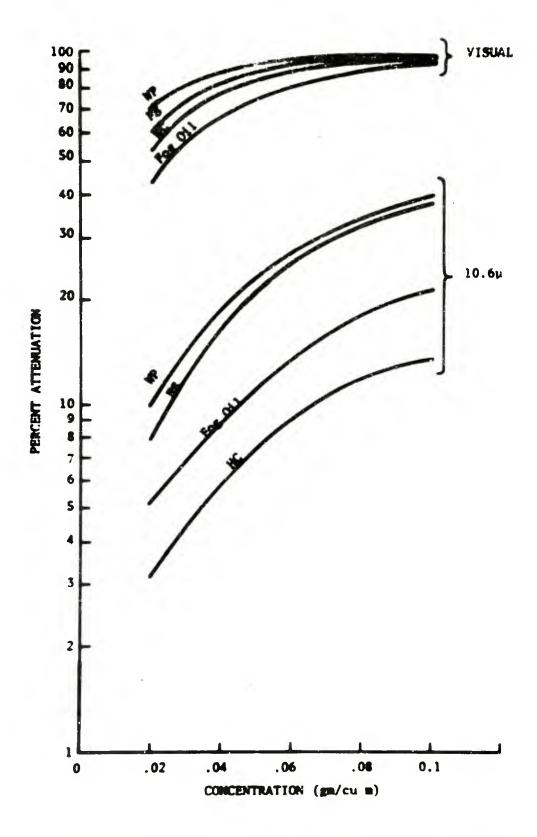
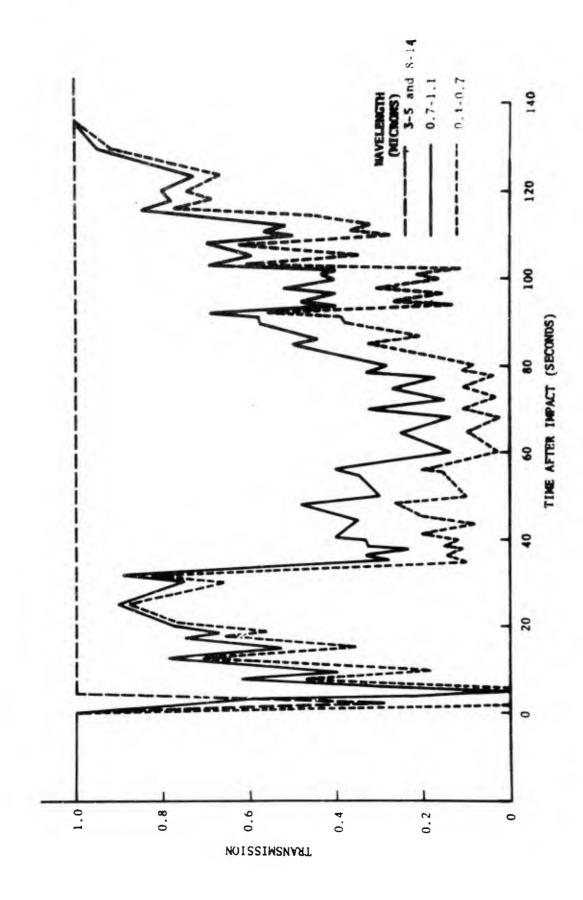
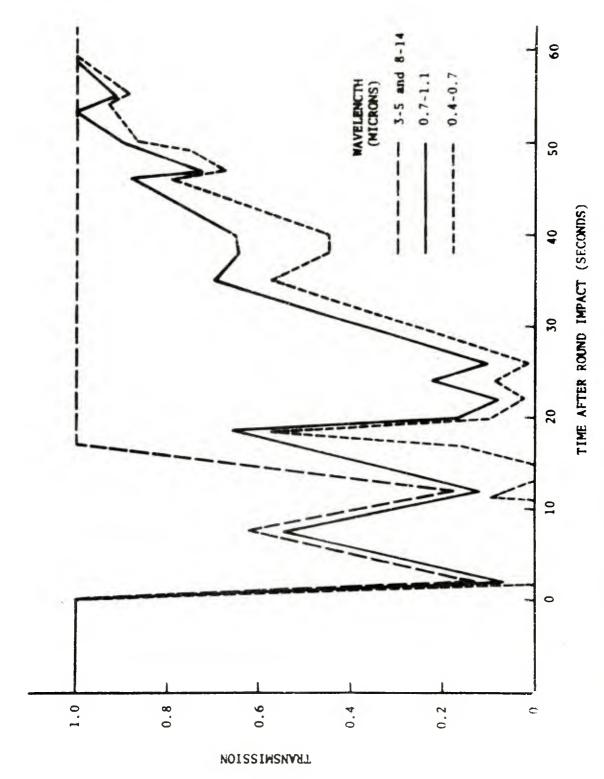


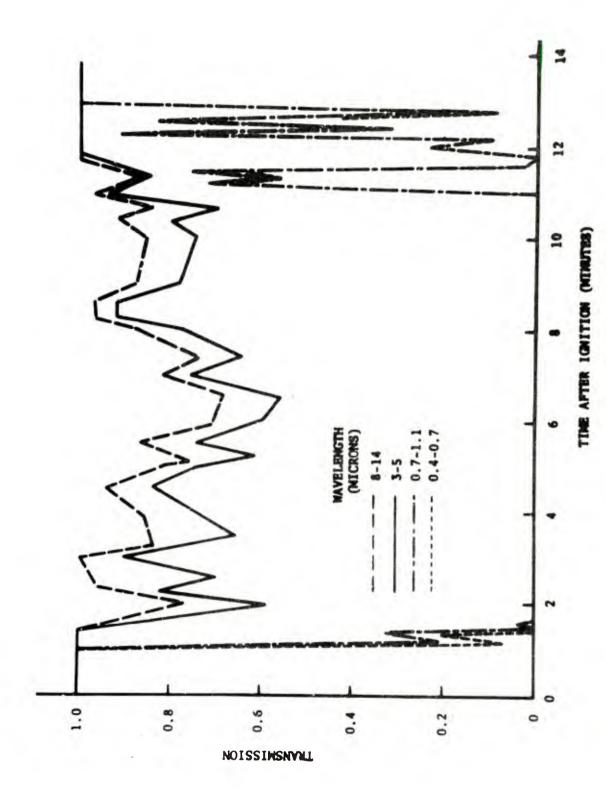
Fig. 59. Transmission through Several Smokes as a Function of Concentration for Visible Light and  $10.6\mu m$  Laser Radiation (Data from Ref. 44)



Optical Transmission through an HC Smoke Cloud as a Function of Time After Impact for Indicated Wavelength Ranges (Data from Ref. 44) Fig. 60.



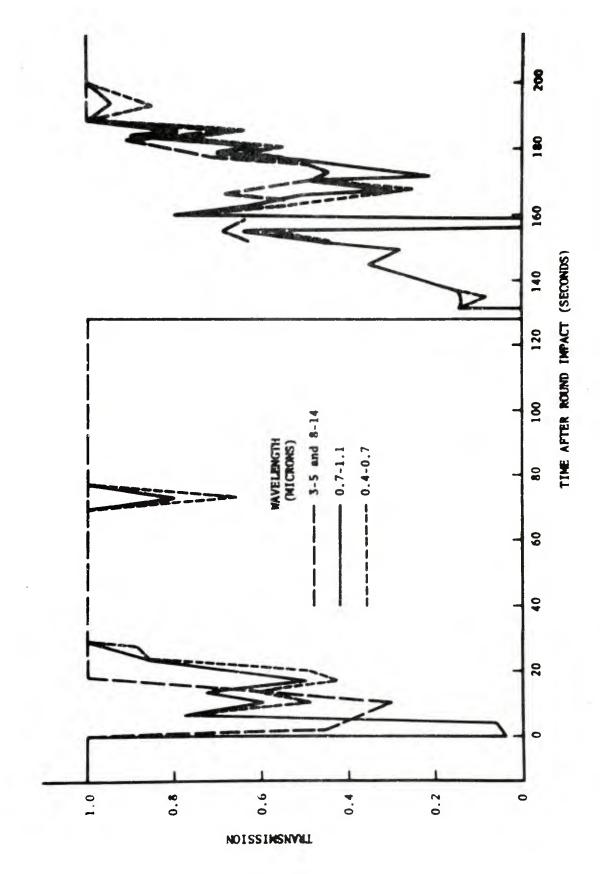
Optical Transmission Through a WP Smoke Cloud as a Function of Time After Impact for Indicated Wavelength Ranges (Data from Ref. 44) Fig. 61.



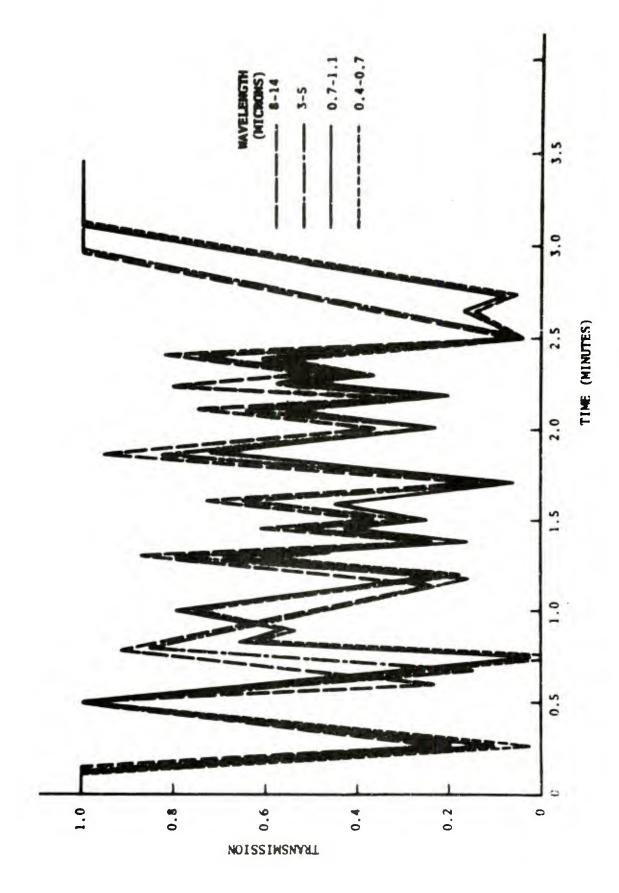
Optical Transmission Through a Fog Oil Smoke Cloud as a Function of Time After Ignition for Indicated Wavelength Ranges. (Data from Ref. 44) Fig. 62.

Table XXXVII. Time in Minutes After Production of Smoke that the Presence of the Smoke Could be Detected by Radiation in the Indicated Wavelength Ranges (Data from Ref. 44)

|                         |                                      |         | 123        | ITTICE TYPE    |                              |
|-------------------------|--------------------------------------|---------|------------|----------------|------------------------------|
| WAVELENGTH<br>(NECEONS) | MEASURED<br>QUANTITY                 | POG OIL | HC<br>POTS | UK<br>GRENADES | AND ARTILLERY<br>PROJECTILES |
| 0.4-0.7                 | Maximum Time of<br>Total Attenuation | 10      | 17         | 4              | 45                           |
| 0.7-1.1                 | Maximum Time of<br>Total Attenuation | 10      | 17         | 4              | 43                           |
| 3-5                     | Maximum Time of<br>Total Attenuation | 0       | •          | 0              | 17                           |
|                         | Average<br>Transmission              | 0.80    | 0.70       | 0.65           |                              |
|                         | Minimum<br>Transmission              | 0.35    | 0.15       | 0.05           | 0                            |
| 8-14                    | Maximum Time of<br>Total Attenuation | 0       | 0          | 0              | 13                           |
|                         | Average<br>Transmission              | 0.90    | 0.80       | 0.70           |                              |
|                         | Minimum<br>Transmission              | 0.50    | 0.35       | 0.15           | 0                            |



Optical Transmission Through a Dust Cloud as a Function of Time after Round Impact for Indicated Wavelength Ranges (Data from Ref. 44) Fig. 63.



Optical Transmission Through Dust Cloud as a Function of Time After Cloud Formation for Indicated Wavelength Ranges (Data from Ref. 44) Fig. 64.

# III. SUMMARY OF DOCUMENTS SURVEYED IN THE LIMITED DOCUMENT LITERATURE

Only documents that were felt worthy of mention, as containing information not found in the open literature will be discussed here. The technical areas will be along the same format as was in the unlimited version.

### 3.1 Attenuation and Scattering by Rain and Hail

Vogel reports in Ref. 83 on Mie theory calculations for spheres of water (rain) and ice (hail) at frequencies of 30, 100, 150 and 300 GHz. The values he used for the index of refraction for water and for ice are given in Table XXXVIII. He points out that frozen rain (hail) scatters more radiation than does liquid rain for frequencies above 150 GHz. The Russians concur with this conclusion in their articles on attenuation by snow (see Ref. 72). Richard and Kammerer also points out that mm radiation scattering by ice will tend to be more peaked in the forward direction for frequencies above 100 GHz than that computed for water droplets. The single scattering of ice was found to be critically dependent on its conductivity. A number of different Mie theory calculations of the phase function for scattering are given in Ref. 55. Attenuations due to rainfall at 100 GHz based on the Mie theory calculations were compared with measurements taken by Setzer, Asari and Medhurst and were found to be within the experimental error.

### 3.2 Attenuation by Water Vapor

Gamble and Hodgens  $^{84}$  reported on a literature survey for mm waves of wavelength 0.735 - 8.57 mm. They caution about dimer effects during heavy fog (relative humidity >95%) or rain (RH >80%). Dimer effects are (H $_2$ 0) - (H $_2$ 0) interactions that tend to broaden the water vapor absorption

Table XXXVIII. Index of Refraction of Water and Ice
(Data from Ref. 84)

| Frequency |               | Index of        |
|-----------|---------------|-----------------|
| (GHz)     | State         | Refraction      |
| 30        | Water<br>20°C | 5.9 - 2.9       |
|           | Ice           | 1.91 - 0.002j   |
| 100       | Water<br>20°C | 3.505-2.007j    |
|           | Ice           | 1.88 - 0.00076i |
| 150       | Water<br>20°C | 3. 039-1. 575j  |
| *         | Ice           | 1.88 - 0.00076i |
| 300       | Water<br>20°C | 2.587-0.937j    |
|           | Ice           | 1.88 - 0.00076i |

85,86 lines. Dimer effects were also considered by Russian authors Gamble and Hodgens present data in Ref. 84 on the in band attenuation in dB/cm vs. visibility for a number of wavelengths between 320 mm to 8.57 mm and for atmospheric temperatures between 0° and 30°C in 5° C steps. A sample of their data is given here as Table XXXIX. Three figures of interest from Ref. 84 should be noted; data on the wavelength dependence of the refractive index of ice, presented here as Fig. 65; data giving the volume concentration of water droplets by size, presented here as Fig. 66, and the attenuation due to the liquid water content as a function of visibility for a number of wavelengths between 320 µm and 8.57 mm and a temperature of 24° C, presented here as Fig. 67. Gamble and Hodgens conclude that at any particular wavelength chosen in the mm band, water vapor absorption will be the driving unknown parameter, and will be a strong function of temperature and humidity. He feels that high resolution measurements need to be made to back up the actual calculations to be certain of the absolute attenuation at a given frequency.

### 3.3 Refractive Indices for Sea Spray

Eric Shettle  $^{87}$  has reported on measurements of sea spray for wavelengths between 0.1  $\mu m$  and 40.0  $\mu m$  and a relative humidity of 80%. His data are presented here in Fig. 68. He also reported measured data on the refractive indices of water, sea spray aerosol and sea salt for wavelengths in the visible and infrared wavelength regions. There is a paucity of data on indices of refraction in the mm and sub mm wavelength ranges.

Total Attenuation (dB/km) For Water Vapor at  $20^{\circ}$  C (Data from Ref. 84) Table XXXIX.

| >    |        |        |        |        |        |        | Wavelength | dî.    |       |        |      |      |
|------|--------|--------|--------|--------|--------|--------|------------|--------|-------|--------|------|------|
| •    | 320 µm | 345 µm | 450 µm | 490 pm | 620 µm | 650 µm | 720 μm     | 880 11 | 1.3   | 2.3 mm | 3.19 | 8.57 |
| 1000 | 190.80 | 95.46  | 85.91  | 108.52 | 95.41  | 18.99  | 30.59      | 19.13  | 4.81  | 1.55   | 0.76 | 0.25 |
| 8    | 190.82 | 95.48  | 85.93  | 108.54 | 95.43  | 66.82  | 30, 60     | 19.14  | 4.82  | 1.55   | 0.76 | 0.25 |
| 80   | 190.85 | 95.51  | 85.95  | 108.56 | 95.44  | 66.84  | 30.61      | 19.16  | 4.83  | 1.56   | 0.77 | 0.25 |
| 780  | 190.89 | 95.55  | 85.99  | 108.60 | 95.47  | 98.99  | 30.64      | 19.18  | 4.84  | 1.56   | 0.77 | 0.25 |
| 8    | 190.95 | 95.61  | 86.04  | 108.65 | 95.51  | 96.90  | 30.68      | 19.21  | 4.86  | 1.57   | 0.79 | 0.25 |
| 8    | 191.05 | 95.70  | 86.12  | 108.72 | 95.57  | 96.99  | 30.73      | 19.25  | 68.9  | 1.58   | 0.79 | 0.25 |
| 8    | 191.19 | 95.84  | 86.24  | 108.84 | 95.66  | 67.04  | 30.81      | 19.32  | 4.93  | 1.60   | 0.81 | 0.26 |
| 8    | 191.47 | 96.11  | 86.48  | 109.06 | 95.83  | 67.21  | 30.98      | 19.46  | 5.02  | 1.6    | 0.83 | 0.26 |
| 200  | 192.19 | 96.81  | 87.09  | 109.64 | 96.28  | 07.64  | 31.40      | 19.81  | 5.24  | 1.75   | 0.89 | 0.27 |
| 8    | 195.11 | 99.66  | 89.57  | 111.97 | 98.11  | 66.39  | 33.12      | 21.23  | 6.13  | 2.16   | 1.15 | 0.30 |
| 8    | 195.91 | 100.44 | 90.25  | 112.61 | 98.61  | 69.87  | 33.59      | 21.62  | 6.38  | 2.28   | 1.22 | 0.31 |
| 08   | 196.95 | 101.45 | 91.14  | 113.44 | 99.25  | 70.50  | 34.20      | 22.13  | 6.70  | 2.42   | 1.31 | 0.32 |
| 0,   | 198.39 | 102.86 | 92.36  | 114.60 | 100.13 | 71.33  | 35.05      | 22.83  | 7.14  | 2.63   | 1.44 | 0.33 |
| \$   | 200.47 | 104.83 | 94.10  | 116.23 | 101.43 | 72.53  | 36.24      | 23.83  | 7.77  | 2.92   | 1.61 | 0.35 |
| 8    | 203.57 | 107.93 | 96.80  | 118.72 | 103.41 | 74.48  | 38.11      | 25.37  | 8.74  | 3.37   | 1.89 | 0.39 |
| 9    | 208.87 | 113.13 | 101.30 | 123.02 | 106.73 | 77.63  | 41.21      | 27.96  | 10.38 | 4.12   | 2.36 | 97.0 |
| 8    | 219.07 | 123.03 | 109.90 | 131.15 | 113.13 | 83.73  | 47.21      | 32.87  | 13.50 | 5.58   | 3.25 | 0.55 |
|      |        |        |        |        |        |        |            |        | _     | 1      |      |      |

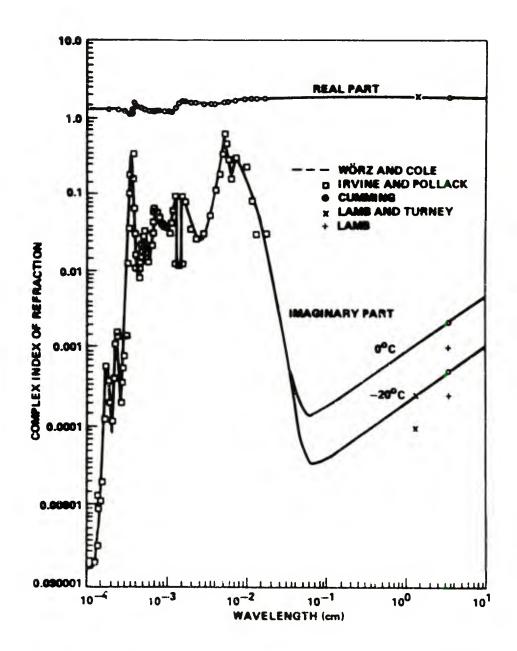


Fig. 65. Wavelength Dependence of the Real and Imaginary Parts of the Index of Refraction of Water (From Data in Ref. 84)

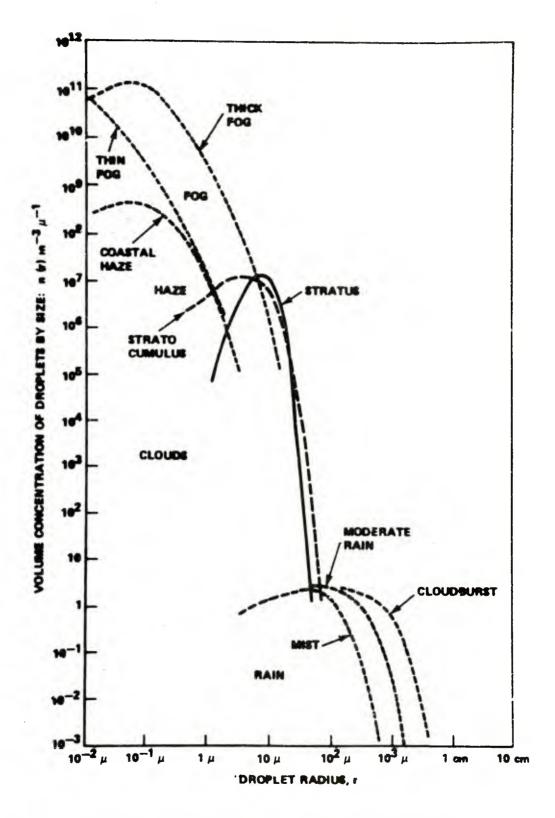


Fig. 66. Volume Concentration of Water Droplets by Size (Counted in 1-micron Intervals by Drop Radius.) (Data from Ref. 84)

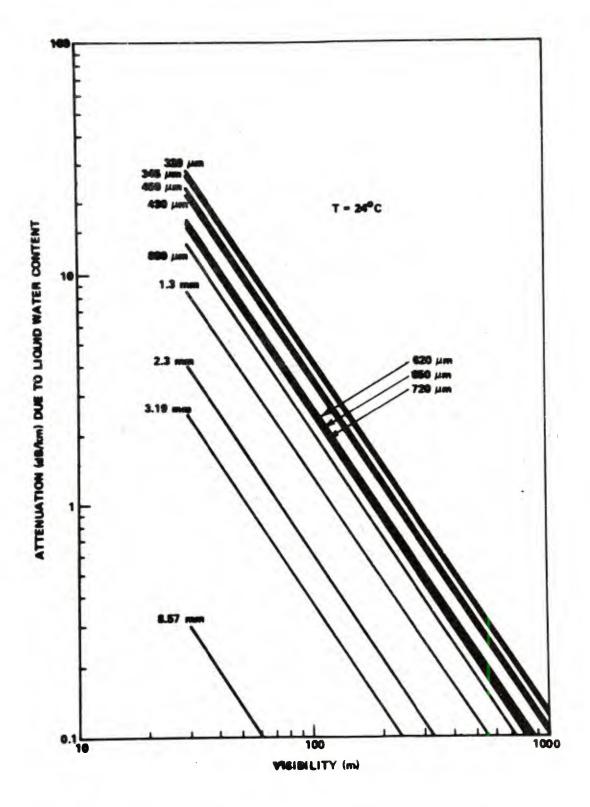


Fig. 67. Atmospheric Attenuation Due to Liquid Water Content Versus Visibility at a Temperature of 24°C and Wavelengths Between 320  $\mu m$  and 8.57 mm (Data from Ref. 84)

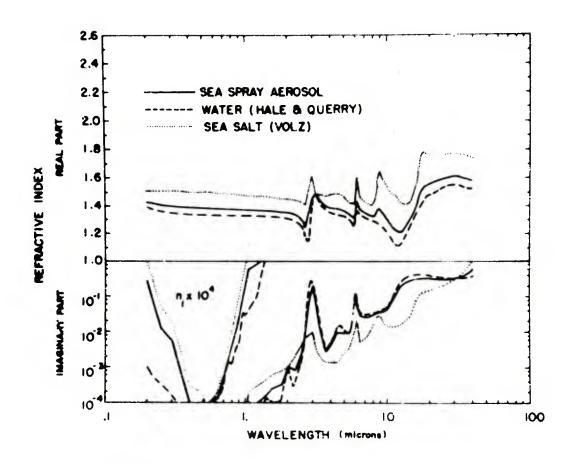


Fig. 68. Refractive Index of the Sea Spray Produced Aerosol at 80% Relative Humidity. Also shown are the Refractive Indices of Water and Sea Salt. (Data from Ref. 87)

### IV. SUMMARY OF DOCUMENTS SURVEYED IN THE CLASSIFIED LITERATURE

A review of the classified literature showed that all the physical properties of the atmosphere and other media, e.g., rain, aerosols, snow, and battlefield conditions, were treated in the unclassified section. The classified documents were effectively hardware related and no new physical properties of the atmosphere were discussed.

## V. RECOMMENDATIONS FOR FURTHER RESEARCH

Two of the most important attenuators of mm and sub mm radiation in the atmosphere are water vapor and oxygen. For the case of water vapor there are resonance frequency regions at approximately 1.3, 2.1, 3.2 and 8.6 mm where absorption is abnormally large. Much of the water vapor attenuation coefficient data currently available for the mm and sub mm wavelength range were measured or calculated over a decade ago. It appears that some new measurements would be useful for checking out the accuracy of band model calculations. The measurements need to consider the effects of temperature and pressure on the absorption cross section of water vapor. The Russians have pointed out the importance of considering dimer effects, where attenuation is proportional to the square of the humidity, when calculating the absorption cross section for wavelengths in the 1.15 to 1.55 mm band. Most investigators have used a Lorentz line profile when calculating the contribution to the absorption cross section from the wings of each line. It appears that use of other line profiles, such as the Van Vleck-Weiskopf model, would probably produce more accurate water vapor absorption cross section data in the mm and sub mm wavelength range than that now available. The line broadening produced by  $(N_2 - H_20)$ ,  $(O_2 - H_20)$  and  $(H_20 - H_20)$  collisions needs further investigation.

The absorption by oxygen in the mm and sub mm wavelength is usually considered to be fairly well known. Even so, the experimental and theoretical data now being used is over a decade old and a comparison of transmission calculations based on that data with measurements would be useful.

The index of refraction of liquid water at 20°C is fairly well known, but at other temperatures it is not well known. Thus, the transmission of mm and sub mm radiation through clouds and fogs containing

water droplets may be considered to be well known at 20° C but only at that temperature. A measurement program is needed to determine the temperature dependent parameters needed in the Debye equation.

There are a fair number of measurements of the attenuation and scattering coefficients for rain at frequencies of 15, 20, 30, 35 and 70 GHz, much fewer at frequencies of 94, 140, 240 and 300 GHz and none at frequencies above 320 GHz. The need to consider the effects of non-sphericity of rain drops, as suggested by Oguiche and discussed by Wiley <sup>69</sup>, when computing scattering, absorption and extinction coefficients and phase function data with the use of Mie theory should be studied.

Propagation of mm and sub mm radiation through snow has not received much attention. At frequencies less than 50 GHz snow is not as important a scatterer as rain, but for frequencies greater than 150 GHz, and especially for wet snow, it will scatter more than rain. Calculations of the scattering and attenuation characteristics of snow with the use of Mie theory needs to consider the fact that snow flakes are not spheres. A measurement program is also needed to obtain more accurate values of the index of refraction for both ice and snow in the mm and sub mm wavelength range. Measurements of the index of refraction of ice and snow need to be made as a function of temperature and, for the case of snow, as a function of the "wetness" of the snow.

Aerosol effects have not been seriously considered for mm and sub mm wavelengths since for normal atmospheric aerosol size distributions the particle size is small enough for Rayleigh scattering theory to be applicable. Aerosol effects for battlefield type dust, which contains a significant fraction of large particles, needs further investigation. Studies need to be carried out on the scattering and absorption by large aerosol particles with a core of one material and an outside shell of another material. The index of refraction of aerosols for mm and sub mm

wavelengths needs to be measured so as to provide data to be used in Mie theory calculations.

There is no information available on the index of refraction for battlefield dusts, battlefield generated smokes and exotic gases and the aerosols produced by vehicle engines. Although some information on combustion products were found in the literature, there is a need for a study to define the specific combustion products emitted by the engines of battlefield vehicles and to determine which are important absorbers and scatterers of mm and sub mm wavelength radiation. Of great importance is the need for data on the size distributions of the particles contained in battlefield generated dusts and smoke.

Some data are available on the transmission of mm and sub mm radiation through battlefield generated dust and smoke (see Section 2.7). More effort needs to be expended to develop better models of the time and spatial dependent variation of battlefield smoke and dust particle size distribution. Since the particle sizes that are important in Mie theory calculations are those with diameters greater than 0.06 times the wavelength, the need to treat these large particles as nonspherical particles in Mie theory should be investigated.

The exotic gases produced under battlefield conditions should be identified and the absorption lines for these gases should be tabulated to determine which of the gases would be important absorbers for mm and sub mm wavelength radiation.

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## APPENDIX A - BIBLIOGRAPHY

A bibliography of the unclassified unlimited and limited literature on the interaction phenomena occurring in the atmosphere for millemeter and submillemeter radiation is given in the Appendix.

To aid the user of this bibliography, a 7-digit identifier or index number, on the same theme as the Dewey Decimal classification or key-word description, is given to each bibliographical entry. This 7-digit index number has the following form:

The first digit of the identifier number, which is used to identify the materials discussed in the biographical entry. is assigned numbers as follows:

- 1) Water vapor
- 2) Rain and aqueous water
- 3) Snow
- 4) Clouds and Fog
- 5) Air
- 6) Oxygen, 0,
- 7) Ozone
- 8) Nitrogen and its compounds (include Organic Compounds)
- 9) Exotic gases and Hydrocarbons
- A) Smoke and Aerosols
- B) Dust and Solid material
- C) Hardware Discussions
- D) Plasmas

The material identifiers listed above were selected to satisfy the terms of the work statement of the contract; additional identifiers are

provided because of titles specifically on these topics that had been reviewed and were considered useful peripheral information in mm wave technology. If an article discusses more than one material, and one of the materials discussed is one of those called out in the contract, then the article is listed under the material category called out in the contract. To identify the mm wave spectral region, the second digit of this 7 "digit" identifier is used in the following fashion:

- 1) 10-30 GHz (3.33 cm 1 cm)
- 2) 30-100 GHz (1 cm 3.33 mm)
- 3) 100-300 GHz (3.33 mm 1 mm)
- 4) 300-1000 GHz (1mm 333 μm)
- 5) 1000 GHZ 3000 GHz (333 μm 100 μm)
- 6) Greater than 3000 GHz (wavelength less than 100  $\mu\text{m})$

For the third digit of the index number identifier, one of the following numbers for unclassified, unlimited distribution documents is used:

- 1) Experimental
- 2) Theory
- 3) Combination of Experimental and Theory

For limited distribution, unclassified documents, one of the following numbers for the third digit is used:

- 4) Experimental
- 5) Theory
- 6) Combination of Theory and Experimental

For confidential documents, the third digit was assigned as follows (to include the classification):

- Experimental
- 8) Theory

9) Combination of Theory and Experimental

For secret classified documents, the third digit is assigned as follows:

- A) Experimental
- B) Theory
- C) Combination of Theory and Experiment

To identify the specific technical area described in the bibliographical entry, such as transmission, reflection, etc., the fourth "digit" is used in the following way:

- 1) Transmission
- 2) Reflection
- 3) Cross Section
- 4) Backscatter
- 5) Dielectric
  - 6) Index of Refraction
  - 7) Emission

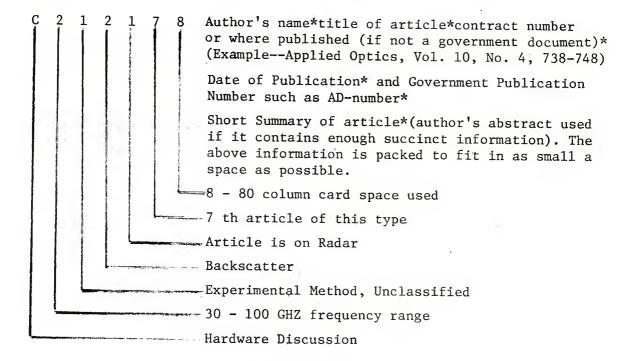
The fifth digit of the identifier number, which describes the project area described in the bibliographical entry, is assigned as follows:

- 1) Radar
- 2) Astronomy
- 3) Radiometry
- 4) Fourier Transform Spectrometer
- 5) Spectrometer and Michelson Interferometer
- 6) Remote Sensing
- 7) Communications
- 8) General Use
- 9) Obscurant
- A) Laser and Maser
- B) Missile Seeker

The sixth digit of the identifier number is used to indicate the number of articles in the bibliography on each title or technical area (1-9, A-Z). A computer code can be written to search on a file (tape or disc) where, with respect to an 80 column card, the first 7 columns would contain the 7 "digit" number. The last digit of the index number (the seventh) is used to designate the number of 80 column cards space in the file required to contain the subfile.

## A.1 Illustration of Indexing/Identifier Technique

Let us pick a number and see how it refers to the indexing system discussed above (Along with discussion on what is on a file):



To allow a computer to access the contents of the index card file on a disc or a tape, the information given after the 7 digit identifier must be spaced by a computer recognizable identifier, e.g., an asterisk. The end of the abstract will end uniformly by a double asterisk for an end of file identifier for each article file.

851781C\*WALKER, R.E.: AND HOCHHEIMER, B.Z.\*INVERSION-ROTATION EMISSION SPECTRUM OF THERMALLY-EXCITED NH3 IN THE 60-200 CM-1 REGION.\*JOURNAL OF MOLECULAR SPECTROSCOPY 34,500-515.\*1970\* NO #.\*THE INVERSION-ROTATION EMISSION SPECTRUM OF THERMALLY EXCITED NH3 IN THE 60-200 CM-1 REGION HAS BEEN MEASURED USING INTERFERENCE SPECTROSCOPY.INVERSION-ROTATION-FREQUENCY ASSIGNMENT, ASSOCIATED WITH THE V2,V4 AND 2V2 LOW LYING VIBRATIONAL LEVELS, ARE BASED EXTENSIVELY ON NEW I.R. ABSORPTION MEASUREMENTS.REFINEMENTS ARE MADE IN THE INVERSION-ROTATION MOLECULAR CONSTANTS FOR THE V2 VIBRATIONAL LEVEL, AND THE 2V2 INVERSION-ROTATION EMISSION SPECTRA IS EXTENDED.

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MICROMAVE ATIENUATION SETATISTICS, ON THE EARTH-SPACE PATH AT 13, 19, 480 300 AT 100 A

ISLAND, VA. USING A HIGH RESOLUTION S-BAND RADAR INTERFACED WITH A COMPUTER AND DIGITAL PROCESSING SYSTEM. FADE STATISTICS HAVE BEEN CALCULATED FOR VARIOUS PATH ANGLES AND SEVERAL FREQUENCIES BETWEEN 13 AND 100GHZ.\*\*

2211718\*SANDER, JOERG\*RAIN ATTENUATION OF MILLIMETER WAVES AND PROPAGATION, VOL. AP-23, NO. 2, 213-220\*MARCH 5, 1975\*

MEASUREMENTS OF RAINFALL ATTENUATION OF MWWAVES AT 5, 777, 3.3, AND 2 MM WAVELENGTH WERE CONDUCTED DURING 1969-1970. SIMULTANEOUSLY RECORDED METEOROLOGICAL QUANTITIES WERE THUS DETERMINED.

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2. 1618 SHEN, LIANG-CHI\*REMOTE PROBING OF ATMOSPHERE AND HIND VELOCITY BY MILLIMETER WAVES\*IEEE TRANSACTIONS ON ANTENDAM AND AND PROPAGATION, VOL. OF APT-18, NO. 4, 493-497\*JUY 1970\*

A TECHNIQUE IS DEVELOPED TO PROBE THE ATMOSPHERE TURRULENCE STRENGTH CN2 AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE SOURCE HER WITH THE TAKE AND STREAM AND THE SOURCE HER WITH THE TAKE ALONG THE PROPAGATION. EXPERING THE WIND VELOCITY ALONG A PATH USING MM MAYE AND THE SOURCE HER WITH THE AVERAGE CN2 AND WIND VELOCITY AND WIND VELOCITY. TO SOURCE HER WITH THE AVERAGE CN2 AND WIND VELOCITY. THE SOURCE HER WITH THE THE AVERAGE CN2 AND WIND VELOCITY. AND AND METEOR OF THE PROPAGATION OF AND WIND VELOCITY. AND AND METEOR OF THE PROPAGATION OF AND WIND VELOCITY. THE SOURCE HER WITH THE AVERAGE CN2 AND WIND VELOCITY. AND AND METEOR OF THE PROPAGATION OF THE PR

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URBAN CLIMATES WITH PARTICULAR APPLICATIONS TO THE LOS ANGELES BASIN\*JOURNAL OF THE ATMOSPHERIC SCIENCES, VOL. 34, 531-547\*MARCH 1977\*NO #\*A 1-DIMENSIONAL, TIME DEPENDENT MODITHE BOUNDARY LAYER HAS BEEN DEVELOPED TO STUDY THE EFFECT OF POLLUTANTS ON LOCAL METEOROLOGICAL VARIABLES. RADIATIVE TERMS FOR THEMODEL ARE COMPUTED USING A 4-STREAM DISCRETE ORDINATE METHOD, CONVECTION TERMS ARE PARAMETERIZED AT THE SURFACE USING TRANSFER COEFFICIENTS AND DYNAMICAL TERMS ARE PARAMETERIZED FROM AVAILABLE DATA. THE MODEL IS COMPARED METRICALLY FOR THE GREAT PLANE DATA WITH GOOD RESULTS. OPT BANDS ARE FROM THE UV AT .347 UM, THE WATER VAPOR LINE AT 330 CM-1.\*\* MODEL OF PÄRAMETERIZED FROM AVAILABLE UNITA WITH GOOD RESULTS. OPILUAL-IN METRICALLY FOR THE GREAT PLANE DATA WITH GOOD RESULTS. OPILUAL-IN METRICALLY FOR THE GREAT PLANE DATA WITH WATER VAPOR LINE AT 3350 (M-1.\*\*).

A13601A\*BORDIN, L.F.; KIRDYASKORI, K.P.; STAMANKIM, YU.P., AND CHUKHLANTSEV, A.A.\*ON THE APPLICATION OF MICROMAVE RADIOMETRY TO FOREST FIRE SURVEYS\*RADIO ENGINEERING AND ELECTRONICS PHYSICS 21.89-91\*SEPT 1976\*ON #\*STHE INTENSITY OF THE FLAME MICROWAVE RADIOMETRY OF OREST FIRE SURVEYS\*RADIO ENGINEERING AND ELECTRONICS PHYSICS 21.89-91\*SEPT 1976\*ON #\*STHE INTENSITY OF THE FLAME MICROWAVE FROM THE FOREST FIRE SURVEYS\*RADIO ENGINEERING AND ELECTRONICS PHYSICS 21.89-91\*SEPT 1976\*ON #\*STHE INTENSITY OF THE FLAME MICROWAVE RADIOMETRY OF DETECTION IN THE MICROWAVE RADIOMETERS IN THE FLAME AND THE TREE TOPS ON THE MICROWAVE RADIOMETERS IN THE SWOKE NEW PLUME AND THE POSSIBILITY OF DETECTING FOREST FIRES SOUCES USING AIRBORNE MM HAVE RADIOMETERS IN THE .8 AND 3.4 WAVELENGHT BANDS. THE .8 MM BAND NO DEFINITELY SHOWS THE FIRE ARE THEN THAN THE 3.4 MM BAND NO DEFINITELY SHOWS THE FIRE ARE THEN THAN THE 3.4 MM BAND RADIOMETERS. THE REMAINS OF TOWN AND THE MEGA - QEGAHERTZ FRENCH CY RANGES AND TOWN AND TOWN AND TOWN AND THE MEGA - QEGAHERTZ FRENCH CY RANGES AND TOWN AND TOWN AND THE MEGA - QEGAHERTZ FRENCH CY RANGES AND METHODS OF MEGALE AND THE 100 METAL OF THE MEGA - QEGAHERTZ FRENCH CY RANGES AND METHODS OF MEGALE AND THE 100 METAL OF THE MEGALE AND THE MEGALE AND THE 100 METAL OF THE MEGALE AND THE MEG OPTICAL-IR AND OTHER GASES.\*\*

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\*\*ATTENDATION ON THE REPORTED STREET RAPPON ON THE REPORTED RAPPON ON THE REPORT OF A 15 STREET RAPPON ON THE REPORT OF THE RE  ONLY THE COUPLING BETWEEN ADJACENT ROTATIONAL STATES IN MOLECULAR COLLING STORY, WE HAVE DEVISED AS SAMPLE MAPPROXIMATION METHOD FOR COMPUTING THE INTERFERENCE BETWEEN LINES BY METHOD FOR COMPUTING THE INTERFERENCE STATE OF THE INTERFERENCE ST POLYMERS. \*\* PARTICLES MITH COMPLEX INDEX OF REFRACTION. UVALUES OF THE SCATTERING CROSS SECTION AURILATIONS ASSUMED AMSPERS AND BAYES AND WAVELENGTROWN OF THE CALCULATIONS ASSUMED AMSPAPERS AND BARSBALL-ALMER, DOPP DISTRIBUTIONS, USING DROPLET DISTRIBUTIONS ASSUMED THAT THE SCATTERING CROSS SECTION MAY NOT BE CHARACTERIZED THAT THE SCATTERING CROSS SECTION MAY NOT BE CHARACTERIZED BY EVEN RATE ONLY.\*\*

2133810\*\*\*ILEY, P.H.\*\* THE INFLUENCE OF POLARIZATION ON MILLIMETER WAVE PROPAGATION THROUGH OF POLARIZATION ON THE WAVE PROPAGATION ON MILLIMETER WAVE PROPAGATION ON THE MOST ARE ALBERT AND A THEORET ICALL THE WAVE PROPAGATION ON THE WAVE ARE ALBERT ON THE WAVE PROPAGATION ON THE WAVE P

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111731E\*GORDY, NORMAN C.\*REMOTE SENSING OF ATMOSPHERIC WATER CONTENT FROM SATELLIES USING OF ATMOSPHERIC WATER CONTENT FROM SATELLIES USING THE CONTENT FROM SATELLIES OF A MILE STATE OF THE CONTENT FROM SATELLIES OF THE CONTENT

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RATE CONSTANTS OF ATMOSPHERICALLY IMPORTANT SPECIES. THE REACTIONS REPORTED ARE POSITIVE AND NEGATIVE ION CHARGE - TRANSFER (ELECTRON TRANSFER) WITH NEUTRALS, ION-ATOM-INTER-CHANGE REACTIONS (CHEMICAL REARRANGEMENTS) \_, AND 3-BODY ASSOCIATION REACTIONS.\*\*

C111119\*SKOLNIK, M.I.\*REVIEW OF CURRENT RADAR INTERESTS AND EXTENDING THE RADAR SPECT...\*NRL-M5/R-2869\*NO #\*AUG 1974\*AD-785-007\*THIS REPORT CONSISTS OF TWO PAPER THAT ARE CONCERNED WITH CURRENT RADAR INTEREST. IN ONE PAPER, THE VARIOUS MAJOR APPLICATIONS ARE DESCRIBED AND A LISTING OF CURRENT PROBLEM APPLICATIONS ARE DESCRIBED AND A LISTING OF CURRENT PROBLEM OF RADAR OUTSIDE THE NORMAL UWAVE BANDS TO INCLUDE THE REGION AND ONE END OF THE SPECTRUM AND MM WAVES AT THE OTHER END.\*\*

HF REGION AND ONE END OF THE SPECTRUM AND MM WAVES AT THE OTHER END.\*\*

252581A\*DEIRMENDJIAN, D.\*FOR INFRARED AND SUBMILLIMETER SCATTERING. I. THE OPTICAL CONSTANTS OF WATER, A SURVEY\*
NO #\*NO #\*FEB 1974\*AD-787 205\*THIS IIS A LITERATURE SURVEY OVER THE OPTICAL CONSTANTS OF LIQUID WATER FROM 15U TO 1000U IN 1974. HE CONCLUDES THAT THE CONSTANTS ARE FAIRLY WELL KNOWN IN THE ENTIRE RANGE UP TO MM WAVES.

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8411418\*AFSAR, M.N.; HONIJK, D.D.; PARSCHIER, W.F.; AND
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MICROWAVE THEORY AND TECHNIQUES. VOL.

MIT-25 NO. 6, 505-511\*JUNE 1977\*NO \*\*MEASUREMENTS OF THEE
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FOR RADIATION OF WAVE NUMBER 20 CM-2 TO 180 CM+1 LIQUID CELL

INTERFEROMETER.\*\*

921582F\*KEATZE, U.\*DIELECTRIC RELAXATION IN AQUEOUS SOLUTIONS
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921582F\*KEATZE, U.\*DIELECTRIC RELAXATION IN AQUEOUS SOLUTIONS
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TION PROCESSES 7, 71-85\*1975\*NO \*\*THE COMPLEX DIELECTRIC

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OF RESPANDING THE WALL TO THE SET OF THE SET N EXPERIMENTAL M WAVE AS A #\*NO #\*OCT ZENITH ATMOSPHERIC T NIRFI FROM 1960-1964 ARE GIVEN. MEASUREMENTS WERE CONDUCTED BY RADIO ASTRONOMICAL METHODS AT DIFFERENT HEIGHTS ABOVE SEA LEVEL, WHICH MADE IT POSSIBLE TO DETERMINE THE EFFECTIVE PATH FOR 02 AND WATER VAPOR OF THE ABMOSPHERE IN ABSORPTION. TOTAL ABSORPTION OF THE ATMOSPHERE FROM SEA LEVEL DURING ZENITH OBSERVATION IS GAMMA = 0.26+0.0065 P VAPOR, WHERE P = ABSOLUTE HUMIDITY IN THE SURFACE LAYER OF AIR. EFFECTIVE HEIGHTS OF 02 AND WATER VAPOR OF THE ATMOSPHERE RESPECTIVELY (4.3 + OR - .3) KM, AND (1.75 + OR - 0.1) KM. COEFFICIENTS OF ABSORPTION OF 02 AND WATER VAPOR AT SEA LEVEL ARE (0.21 + OR - .02) AND (.13 + OR - .02) DB/KM, RESPECTIVELY.\*\*
523133A\*WINKLER, LOUIS\*THE PENNSYLVANIA STATE UNIVERSITY RADIO ASTRONOMY OBSERVATOR\*DA-18-001-AMC-905(X)\*NO #\*NOV 1

COEFFICIENTS OF ABSORPTION OF 02 AND WATER VAPOR AT SEA LEVEL ARE (0.21 + 0R - .02) AND (.13 + 0R - .02) DB/KM, RESPECTIVELY.\*\*

23133-8-WINKLER, LOUIS\*THE PENNSYLVANIA STATE UNIVERSITY 1968\*
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FUIURE DEVELOPMENTS ON THE SUBJECT. 80 REFS.\*\*

5121710\*CHEVKIN, S.A. AND NAUMOV, A.P.\*PRPAGATION OF CENTIMETER, MILLIMETER, AND SUB MILLIMETER, NO OF CENTIMETER, MILLIMETER, MIND SUB MILLIMETER, NO OF CENTIMETER, MILLIMETER, MILLIMET

OF ZENITH ATTENUATION MEASUREMENTS OF THE ATMOSPHERE ON BOTH SIDES OF THE OXYGEN ABSORPTION SPECTRUM (48-72 GHZ) ELUCIDATES THE ABSORPTION CHARACTERISTICS OF THE 4 TO 6 MI WAVELENGTH BAND. WITH THE SUN AS A SOURCE, ZENITH ATTENUATION MEASUREMENTS WERE MADE AND USED AS A FUNCTION OF THE PRECIPITABLE WATER CONTENT OF THE ATMOSPHERE TO DETER MINE THE ZENITH ATTENUATION COEFFICIENTS OF PRECIPITABLE WATER. FROM THESE COEFFICIENT AND MEASUREMENTS OF THE TOTAL PRECIPITABLE WATER CONTENT IN THE ATMOSPHERE, THE OXYGEN COMPONENTS OF THE ZENITH ATTENUATION WERE DETERMENTED. TO DETER-MINED. \*\*

MINED.\*\*
C21171A\*COHN, MARVIN AND LITTLEPAGE, ROBERT S.\*IMPLICATIONS
OF MILLIMETER WAVE RESEARCH AND TECHNOLOGY ON NAVAL
PROBLEMS\*N00014-77-C-0166\*NO #\*JAN 1967\*AD-813 462\*THIS
TECHNICAL REPORT CONTAINS A SURVEY AND A CRITICAL ANALYSIS
OF THE EXISTING AND PROJECTED MM WAVELENGTH STATE OF THE
ART. SPECIFIC AREAS TREATED ARE PROPAGATION EFFECTS,
ANTENNAE, COMPONENTS, POWER SOURCES, AND RECEIVER
TECHNIQUES. AREAS WHERE FURTHER RESEARCH AND DEVELOPMENT
WOULD RESULT IN INCREASED PERFORMANCE HAVE BEEN POINTED ANALYSIS OF THE

OUT. \*\*
C13171C\*KEELTY,

WOULD RESULT IN INCREASED PERFORMANCE HAVE BEEN POINTED

C13171 C\*\* KEELTY, J.M. AND CRANE, R.A. \*\*MILLIMETER INVESTIGATIONS,

UT. \*\*\*

C13171 C\*\* KEELTY, J.M. AND CRANE, R.A. \*\*MILLIMETER INVESTIGATIONS,

CONTRACT PG 727001-1\*NO \*\*JAN 1969\*AD\*\*

CONTRACT PG 727001-1\*NO \*\*JAN 1969\*AD\*\*

CONTAINS SAMPLES OF THE COMPUTER ANALYSIS OF VARIOUS

PARAMETERS SALIENT TO THE DESCRIPTION OF SYSTEM PER
FORMANCE. THE VOLUME BEGINS WITH A DESCRIPTION OF THE

STRUCTURE OF THE COMPUTER PROGRAMS AND A SECTION EXPLAINING

THE MEANING OF SAMPLE PRINTOUTS. PRINT OUTS DETAILING THE

STRUCTURE OF SAMPLE PRINTOUTS. PRINT OUTS DETAILING THE

VARIATIONS FOR VARIOUS METEOROLOGICAL COONDITIONS AND A

SECTION DISCUSSINGTHE RESULTS OF A

SECTION DISCUSSINGTHE RESULTS OF A

SECTION DISCUSSINGTHE RESULTS OF A

FREEDRIT WORK ON PROPAGATION IN THE RADIO SPECTRUM FROM

10 TO 100 GHZ\*NO \*\*SUBJECT OF THE ATMOSPHERE AT FREE

13183A\*STEELE, F.K. AND VAN HORN.\*\*

STEELE AT FOR VAND \*\*JAN 1975\*COMM-75-10761\*REFERENCES

ARE PRESENTED ON THE SUBJECT OF THE ATMOSPHERE AT FREE

GENALT WORK ON RADIO PROPAGATION IN THE ATMOSPHERE AT FREE

WORK ON RADIO PROPAGATION THROUGH THE ATMOSPHERE AT FREE

SEPARATED INTO SIX MAJOR CATEGORIES COOKAGATION, THROUGH,

NON-TURB ULENT CLEARANCE, GENERAL COVERED REFERENTION

NON-TURB ULENT CLEARANCE, GAS STUDIES

SPECTROMETER FOR ATMOSPHERIC GAS STUDIES

NON-TURB ULENT CLEARANCE, THE INTO SPECTROMETER

WAVELERIES FROM ATMOSPHERIC GAS STUDIES

SPECTROMETER FOR ATMOSPHERIC COMPONITIONS

ATTER OF THE OWN AND A SEPECTRUM (OZ-MS). DISTRIBUTION

ATTER OF THE OWN AND A SEPECTRUM (OZ-MS). SPECTRUM (OZ-MS).

STRUCTURE OF THE OZ MS ABOUT 60 GHZ COMPOLICATES THE ANALYSIS. SPECIAL DIAGNOSTICS EVOLVED FROM THE DATA

FOR DEDUCING SPECTROSCOPIC PARAMETERS.\*\*

623171D+LIEBE, HANS J.\*STUDIES OF OXYGEN AND WATER VAPOR NICROWAVE SPECTRA UNDER SIMULATED AMMOSPHERIC CONDITIONS\*

MICROWAVE SPECTRA UNDER SIMULATED AMMOSPHERIC CONDITIONS\*

11096\*ATMOSPHERIC RADIO WAVE PROPAGATION IN THE 40-140-6HZ

BAND IS INFLUENCED BY THE UWAVE SPECTRUM OF O2 AND HERE

VAPOR. THIS REPORT TREATS THE COMPLIMENTARY SIDES OF PROVIDING MOLECULAR TRANSFER CHARACTERY

THE CONTROLLED LABORATORY EXPERIMENTS AND COMPUTER ANALYSIS PRESSURE SCANNING DIFFERENTIAL REFRACTOMETER THE VAPOR PROVIDING MOLECULAR TRANSFER CHARACTERS THE VAPOR THE VAPOR THE OZAND H20 SPECTRA WITH FREQUENCY, PRESSURE SCANNING DIFFERENTIAL REFRACTOMETER TO THE VAPOR THE OZAND H20 SPECTRA WITH FREQUENCY, PRESSURE AND H20 SPECTRA WITH FREQUENCY PRESSURE AND H20 SPECTRA WITH FREAD FROM H20 SPECTRA WITH FREAD FR OPERATED VARIABILITY RE, TEMPERA-INTO THREE MAIN CATEGORIES COVERING THE AREA OF PROPAGATION THROUGH NON-TURBULENT CLEAR ATMOSPHERE AND PRECIPI
TOTATION.\*\*

513181 \*THOMPSON, W.I.\*A REVIEW OF RADIOMETER MEASUREMENTS OF
ATMOSPHERIC ATTENUATION AT WAVELENGTHS FROM 75 CENTIMETERS
TO 2 MIGLINES-E29 (LITERATURE SEARCH)\*NASA-TN D-5087\*NO #\*
APR 1969\*N69-\*N69-\*PUBLISHED VALUE MEASUREMENTS
OF ABSORPTION AND EMISSION OF THE EARTH. ATMOSPHERE IN
THE WAVELENGTH RANGE FROM 75 CM (.4 GHZ) TO 2 MM (150 GHZ)
ARE PRESENTED. THE LITERATURE SEARCH DATA EMPHASIZE THE
WAVELENGTH RANGE FROM 75 CM (.4 GHZ) TO 2 MM (150 EW
ARE PRESENTED. THE LITERATURE SEARCH DATA EMPHASIZE THE
NEED FOR FURTHER THEORETICAL AND EXPERIMENTAL WORK IN THE
CALCULATION AND MEASUREMENT OF ATTENUATION IN

7337318\*NO 4ND EXPECTATION ATTENUATION IN
7337318\*NO #BESONANT LINE (APPROX 100 GHZ) WITH SUFFICIENT
AN OZONE RESONANT LINE (APPROX 100 GHZ) WITH SUFFICIENT
INTENSITY WHICH COULD BE DETECTED WITH A SIGNAL TO NOISE
RATES (FROM A SPACE-BORNE RADIOMETER) ADEQUATE TO ALLOW
RESOLUTION OF THE LINE PROFILE TO THE PRECISION REQUIRED
FOR THE INVERSION. A FURTHER STIPULATION WAS THAT THE
TECHNIQUES AND COMPONENTS INCORPORATED IN THE DESIGN OF
THE SATELLITE INSTRUMENT, OR NEAR, CURRENT STATE OF THE

1231619\*\*GAUJI, N.E. \*\*INTERACTION MODEL OF \*\*MICROPHAY VEO \*\*SAPOR OF \*\*AND ATMOSPHERIC VARIABLES\*\*CONTENDED \*\*AND \*\*AND ATMOSPHERIC VARIABLES\*\*CONTENDED \*\*AND \*\*AND ATMOSPHERIC VARIABLES\*\*CONTENDED \*\*AND \*\*AN

DETERMINATION BY MEANS OF A 22-COLOR MIECTLIDAR THERE AND A AREASONS ARE IMPORTANT FOR OF THE THE STATE OF A THE SERVICE SERVI

AND RADIATION OF THE ROUGH SURFACE OF THE SEA AND THE ICE COVER ARE INVESTIGATED AND THE CONTRAST IN RADIO BRIGHT-NESS TEMPERATURE OF THE ICE FIELD, THE ZONE OF CLOUD COVER, PRECIPITATION AND THE REGIONS OF REVERSED HUMIDITY ARE EVALUATED. THE POSSIBILITY OF USING RADIO EMISSION IS EVALUATED FROM THE VIEWPOINT OF SOLVING INVERSE PROBLEMS, I.E., SOUNDING OF THE ATMOSPHERE AND THE UNDERLYING SURFACE FROM AIRCRAFT.\*\*

EVALUATED. FROM THE VIEWPOINT OF SOLVING INVERSE PROBLEMS,
I.E., SOUNDING OF THE ATMOSPHERE AND THE UNDERLYING
SURFACE FROM AIRCRAFT.\*\*

SOUNDING WASA TITE -16930\*NO #\*JULY 1976\*N76-27449\*THIS IS

A LONG ARTICLE ON MICROWAVE REMOTE ENVIRONMENT
SOUNDING\*NASA TITE-16930\*NO #\*JULY 1976\*N76-27449\*THIS IS

A LONG ARTICLE ON MICROWAVE REMOTE SOUNDING - - MICROWAVE REMOTE SOUNDING \*NASA TITE -16930\*NO #\*JULY 1976\*N76-27449\*THIS IS

A LONG ARTICLE ON MICROWAVE REMOTE SOUNDING - - MICROWAVE - LENGTH REGIONS, ALTHOUGH THERE ARE DISCUSSIONS ABOUT MEASUREMENTS IN THE 3-3.2 CM RANGE IN THE ATMOSPHERE, SOIL, OIL SPILLS, ICE COVER. CALCULATIONS OF DIELECTRIC CONSTANTS OF SOILS ARE ALLUDED TO, IN THE 8.1 - 214 MM RANGE. THERE IS A 167-ELEMENT BIBLIOGRAPH IN DIELECTRIC RANGE. THERE IS A 167-ELEMENT BIBLIOGRAPH IN DIELECTRIC RANGE. THERE IS A 167-ELEMENT BIBLIOGRAPH IN DIELECTRIC RANGE. THERE SO NEW SECATTERING CORFECTION #\*AUGE 1975\*N76-27629\*ALGORYTHMS HAVE BEEN DEVELOPMENS TEMPERATURE AT 193 RAD SCAT (13.9 GHZ RADDIOMETER)

TEMPERATURE FOR SKYLAMB-5-ALTENUATION. THE SE ALGORYTHMS FOR THE EFFECTS OF CLOUD ATTENUATION. THE SE ALRIZED EXCESS BRIGHTNESS TEMPERATURE AT 50-DAY INCIDANT IN THE FOR I - ZONTALLY POLARIZED EXCESS BRIGHTNESS TEMPERATURE THEN DAY INCIDANT IN THE AND SOUND THE AND SCATTERING COEFFICIENT AT 50 DEG. FOR ANGLES VARIATION OF EMISSIVITY WITH SALINITY AND WATER AT MILLIMETER WAVE

210NS.\*\*

210NS.\*\*

211NS.\*\*

231581K\*BLUE, M.D.\*PERMITTIVITY OF WATER AT MILLIMETER WAVE

TIONS. ## 231581K\*BLUE, M.D.\*PERMITTIVITY OF WATER AT MILLIMETER LENGHTS\*N56-5082\*NO #\*AUG\_1976\*N76-30911\*THIS REPORT COVERS WORK PERFORMED ON THE PERMITTIVITY OF SEAWATE COVERS WORK PERFORMED ON THE PERMITTIVITY OF SEAWATER AND ICE AT 100 GHZ. MEASUREMENTS ON WATER WERE FROM 0 DEG C TO 50 DEG C; ON ICE, NEAR -10 DEG C. IN ADDITION, A SMALL NUMBER OF MEASUREMENTS WERE MADE ON REFLECTIVITY OF ABSORBER MATERIALS USED IN THE PROGRAM "RE-SEARCH ON MM WAVE TECHNIQUES." AT 103.86 GHZ, THE FOLLOW-ING RESULTS ARE GIVEN: FREE WATER: REFLECTIVITY - 0.392 + OR - .014; INDEX OF REFRACTION M = 3.24 - I 1.825: APPROPRIATE DIFLECTRIC CONSTANTS ARE: E' - IE" = 7.16 - I 11.825. FOR SEA WATER (.7N SOLAR OF NACL). R(SALT WATER)/R(FRESH WATER) = 1.0056 + OR - .010. FOR SALT WATER FROM THE GULF OF MEXICO, R(SALT WATER)/R(FRESH WATER)) = 1.004I.008. THUS, ONE CAN'T DETECT THE EFFECT OF SALT IN WATER AT 100 GHZ. FOR ICE AT 99 GHZ; R(!CE) = .0785 + OR - .0112; N = 1.78 + OR - .08; E = 3.17 + OR - .27. THE LITERATURE INDICATES NO ABSORPTION OR DISPERSION OF ICE IN MM-CM BANDS.\*\* SEAWATER

ICE IN MM-CM E 212371M\*MAWIRA, 2371M\*MAWIRA, A. AND DICK, J.\*DEPOLARTZATION BY RASOME RELATED THERMAL EMISSION CONSIDERATIONS\*NO #\* RAIN.

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FINDHOUSE AND THE PROPERTY OF 
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B612618*RAO, N.C.*EVALUATION OF INDEX PROPERTIES OF NATURAL FORMATION BY POLARIBETER STORES OF NATURAL ADDO 2014 THE DEPENDENCE OF STHE POLARIZATION OF RADIOTION OF REPORT 1974 ADDO 2014 THE DEPENDENCE OF STHE POLARIZATION OF RADIOTION OF
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SCATTER FROM A 70-GHZ RADAR\*BR L-MR-2467\*NO. #\*MAR 1975\*AD1009 699\*A MATHEMATICAD TO PREDICT THE COMPUTER STORY
THAT HE ADDRESS OF THE THAT HE ADDRESS OF THE CALL THE COMPUTER STORY
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FOR THE GENERAL MUTUAL COHERENCE FUNCTION IS DERIVED,
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LENGTHS \*\* A BLACKENIAN POWDER IS FOUND TO BE FARRED TO BE STANDED TO BE REFERENCES. \*\* MENTS\*NO #\*ADV. MOL. RELAXATION PROCESSES, VOL. 7, 113-120\*
1975\*NO #\*OPTICAL CONSTANTS MEASURED BY THE ATTENUATED
TOTAL REFLECTION (ATR) TECHNIQUE FOR MEDIUM INTENSITY
ABSORPTION OF A WIDE VARIETY OF LIQUIDS WERE USED TO TEST
THE APPLICABILITY OF THE VAN VLECK-WERSSKOPFBOND SHAPE
MODEL. THIS MODEL YIELDS TWO PARAMETER CHARACTERISTICS
OF A PARTICULAR BOND, THE INTEGRATED BAND INTENSITY
CORRECTED FOR THE BULK DIELECTRIC EFFECT AND A DAMPING
CONSTANT, RELATED TO THE MEAN COLLISION OR RELAXATION

6221811\*LIEBE, H.J. AND WELCH, W.M.\*MOLEGULAR ATTENUATION AND PHASE PISPERSION BETWEEN 40 AND 140 GHZ FOR PATH MODELS FROM DIFFERENT ALTITUDES\*NO #\*\*SOFTICE OF TELECOMMUNICATIONS, N.B.S. OT REPORT 73-10\*MAY 1973\*NO #\*RADIO WAVE PROPAGATION IN THE 40 - 140 GHZ BAND THROUGH THE FIRST 100 KM OF THE ATMOSPHERE I STRONGLY INFLUENCED BY THE MICROWAVE SPECTRUM OF OXYGEN (02-MS). A UNIFIED TREATMENT OF MOLECULAR ATTENUATION AND PHASE DISPERSION IS FORMULATED. RESULT THE MOLECULAR PHYSICS ARE TRANSLATED INTO FREQUENCY, LESS OF A COMPLEX REFACLE ATTENUATION AND PHASE DISPERSION IS FORMULATED BY COMPUEX REFACLES OF A COMPLEX REFACLES OF A CO L.V. #

FEBO30 (WITH GA+3), ARE GIVEN, AND CORRELATION IS

EXCELLENT.\*\*

133182L\*KUKIN, L.M.; NOZDRIN, YU.N.; RYADOV, V.YA;

FEDOSEYEV, L.I.; AND FURASHOV. N.I.\*DETERMINATION OF THE CONTRIBUTION OF WATER VAPOR MONOMERS AND DIMERS TO ATMOSPHERIC ABSORPTION FROM MEASUREMENT DATA IN THE LAMBDA = 1,15-1.55 MM BAND\*NO #\*RADIO ENGINEERING AND ELECTRONIC PHYSICS, VOL. 20, NO. 10, 7-13\*OCT 1975\*

NO #\*THE COMPONENT OF THE WATER VAPOR ABSORPTION COEFFICIENT THAT ARE LINEARLY AND QUADRATICALLY DEPENDENT ON THE ABSOLUTE HUMIDITY OF THE AIR ARE DETERMINED FROM MEASUREMENTS OF THE DEPENDENCE OF RECEIVED RADIATION ON THE LATTER. THE LINEAR COMPONENT TOGETHER WITH A CERTAIN PORTION OF THE QUADRATIC ARE TAKEN INTO CONSIDERATION THE SELF BROADENING OF THE LINES OF THE H2O MONOMERS IS IDENTIFIED WITH THE ABSORPTION COEFFICIENT OF THE MONOMERS: THE REST OF THE QUADRATIC COMPONENT IS IDENTIFIED WITH THE ABSORPTION COEFFICIENT OF THE MONOMERS: THE REST OF THE QUADRATIC COMPONENT IS IDENTIFIED WITH THE ABSORPTION COEFFICIENT OF THE DIMENS. THE REST OF THE QUADRATIC COMPONENT IS IDENTIFIED WITH THE ABSORPTION COEFFICIENT OF THE DIMENS. THIS PAPER CONTAINS THE RESULTS OF TWO INDENPENDENT EXPERIMENTS, PRESENTED AT THE RUSSIAN (ALL-UNION)

SYMPOSIUM ON THE PROPAGATION OF SUB MM AND MM WAVES
IN THE ATMOSPHERE IN 1974. THERE ARE 41 REFERENCES.\*\*
211817\*GORDY, WALTER; SMITH, WM. V.; AND TRAMBANLO, RALPH. F.\*
MICROWAVE SPECTROSCOPY\*NO #\*JOHN WILEY\*1953\*NO #\*THIS IS
AN EARLY TEXTBOOK ON MICROWAVE SPECTROSCOPY; A LOT OF THE
RESONANCE AND ABSORPTION LINES (IN THE 30-300 GHZ) OF
BARE ATMOSPHERE CONSTITUENTS WERE DISCOVERED BY USE OF
TECHNIQUES DESCRIBED IN THE BOOK. IT IS A STANDARD 5211817 GORDY, TECHNIQUES DESCRIBED IN THE BOOK. 11 15 A STANDARD

REFERENCE.\*\*

521781C\*WACKER, PAUL F.; CORD, MARIAN S., ET AL.\*SPECTRAL

TABLES, VOL. III. POLYATOMIC MOLECULES WITH INTERNAL ROTA

TION\*NO #\*N.B.S. MONOGRAPH 70, VOL. III\*JUNE 1969\*NO #\*

THIS IS A PART OF THE 5-VOLUME NBS MONOGRAPH SERIES ON

MICROWAVE SPECTRAL TABLES. THESE ARE OF VALUE FOR DETER
MINING CHEMICAL CONSTITUENCY OF A SPECIFIC MOLECULAR

SPECIES -- SUCH AS OIL VAPORS, COMBUSTION PRODUCTS -
IN THE SPECTRAL REGION FOR 5 GHZ TO PAST 50 GHZ. OTHER

VOLUMES IN THIS NBS TABLES SERIES ARE: I. DISTANCE MOLE
CULES; II. LINE STRENGTHS OF ASYMMETRIC ROTATIONS; IV.

POLYATOMIC MOLECULES WITHOUT INTERNAL ROTATION; V. SPECTR

INE LISTING.\*\* ROTA-VULUMES; IN LHIS NEWS MITHOUT INTERNAL ROTATIONS; SPECTRAL

CULES; IL LINE STREEM WITHOUT INTERNAL ROTATIONS; SPECTRAL

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D.H.: PUPLET, SURREMENDS, ATM.

PUPLET, SURREMENDS, ATM.

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INCREASED PENEIRATION POWER RELATIVE TO MORE CEXTREMELY INCREASED PENEIRATION POWER RELATIVE TO MORE CEXTREMELY INTO MALE FIR SPECTROMETERS FROM CONVENIENT SERVER FROM CONVENIENT SERV

CULATED. 57 REFS.\*\*

511172 \*\*IPPOLITO, L.J.\*\*TWENTY AND THIRTY GHZ MILLIMETER WAVE EXPERIMENTS LITE AND THIRTY GHZ MILLIMETER APPLICATIONS TECHNOLOGY SATELLITE GOATS APRIL 1976\*N76-2242\*THE APPLICATIONS TECHNOLOGY SATELLITE GOATS APRIL 1976\*N76-2242\*THE APPLICATIONS TECHNOLOGY SATELLITE GOATS APPLICATIONS TECHNOLOGY SATELLITE GOATS APPLICATIONS TECHNOLOGY SATELLITE GOATS APPLICATIONS TECHNOLOGY SATELLITE APPLICATIONS THE FIRST DIRECT MEASUREMENTS OF 20 AND 30 GHZ EARTH-SPACE LINKS FROM AN ORBITING SATELLITE. STUDIES AT 11 LOCTIONS IN THE CONTINENTAL U.S. WERE DIRECTED AT AN EVALUATION OF, SITE DIVERSITY, COHERENCE BANDWIDTH, AND ANALOG AND DIGITAL COMMUNICATIONS TECHNIQUES. IN ADDITION TO DIRECT MEASUREMENTS WITH RADARS, RAIN GAUGES, AND RADIOMETERS WERE DEVELOPED AND COMPARED WITH THE DIRECTLY MEASURED ATTENUATION. THIS REPORT CONTAINS OF THE ATS-6 MM WAVE EXPERIMENT FROM THE MAJOR PERLICOMPUTING ORGANIZATIONS.\*\*

132181ATZRAZHEVSKIY, A.YU.\*METHOD OF CALCULATING THE JAMO-PHYSICS. SPHERIC WATER ABSORPTION OF MALUATION OF SEMILLIF. SPHERIC WATER AND SHAPLICS. THE SPECTRAL REGION. THE SPECTRAL REGION. THE SPECTRAL REGION. THE SPECTRAL REGION. THE SMALL EFFECTS. VOL. 21, NO. 5, 31-36\*MAY 1976\*NO #\*\*A THOO OF SEMILLIF. THE SPECTRAL REGION. THE SMALL EFFECTS. THE DIMERS OF WAPOR ABSORPTION OF MATER IN DB/KM VS WAVE NUMBER, THE BASORPTION OF WATER INCLUDED. THE SMALL EFFECTS. THE SPECTRAL REGION. THE SPECTRAL REGION. THE SPECTRAL REGION. THE SMALL EFFECTS. THE DIMERS OF WATER IS NOT INCLUDED. THE SMALL EFFECTS. THE DIMERS OF WATER IS NOT INCLUDED. THE SMALL EFFECTS. THE SPECTRAL REGION. THE SPECTRAL REGI THE EMPIRICAL FORMULA AGREES RATHER CLOSELY WITH EXPERI
MENT.\*\*

B11411N\*WANG, R.T. AND GREENBERG, J.M.\*SCATTERING BY
SPHERES WITH NONISOTROPIC REFRACTIVE INDICES\*NO #\*APPLIED
OPTICS, VOL. 15, NO. 5, 1212-1217\*MAY 1976\*NO #\*THIS
ARTICLE COVERS X-BAND SCATTERING OFF OF TWO SETS OF
ARTIFICIAL ANISOTROPIC DIELECTRIC SPHERES MADE OF LAYERS
OF CARBON PAPER, ROYAL GRAY PAPER AND PRESSURE. OANISOTROPIC DIELECTRIC SPHERES MADE OF LAYERS
OF CARBON OF THE SECOND GROUP WERE PREPARED FROM ALTERNOM
TOGETHER BY THE APPLICATION OF HEAT AND PRESSURE. OANISOTROPIC MEDIA OF THE SECOND GROUP WERE PREPARED FROM ALTERNOM
NATE LAYERS OF EXPANDED POLYSTYS NEW EACH
NATE LAYERS OF EXPANDED POLYSTYS NEW EACH
CALLED TELEDELTO. THREE TARGETS IN THE SIZE RANGE CASH
TYPE OF ANISOTROPY. THE PRINCIPLE REFRACTIVE INDICES MAND
LEX E KN LE 5.68, A = RADIUS WERL REFRACTIVE INDICES MAND
HO OF THE INCIDENT WAVE RESPECTIVELY, WERE MEASURED FOR EACH
GROUP. RESULTS SHOW THAT HELD THE SPECISOR REACH
GROUP. RESULTS SHOW THAT HELD FORGED OR IENTATION IS
A GOOD APPROXIMATION FOR ANISOTROPIC SPHERES IN THE AGREEMENT
HAS DEFRACTIVE INDEX AT EACH FORGED RESSIVELY
TO THE POLARIZATION, FOR WHICH CASE THE MOST ARECES
ONE GOES TOWARD OTHER PRINCIPLE DIRECTIONS.\*\*

542121D\*TRAUB WESLEY A. AND STIER, MARK THEORETIC AL
ATMOSPHERIC TRANSMISSION IN THE MID AND FAR INFRARED
AT FOUR ALTITUDES\*NO #\*APPLIED OPTICS, VOL. 15, NO. 2,
364-377\*FEB 1976\*NO #\*THE IR TRANSMISSION FOR THE TRANSMISSION 41 KM (10-1000 UM). BOTH HIGH RESOLUTION SPECTRA (.05 CM-1)
AND BROADBAND AVERAGES ARE SHOWN. THE MODEL ATMOSPHERE
USED IS A SINGLE LAYER CARTER GODSON APPROXIMATION WITH
THE COLUMN ABUNDACES GIVEN ACCORDING TO ALURENTZIAN
ABSORPTION LINE PROFILE IS A CONVOLUTION OF A LORENTZIAN
AND A GAUSSIAN. THERE ARE 23 REFERENCES TO SOURCE
ARTICLES IN ATMOSPHERIC LIGHT TRANSMISSION. \*\*
111611\*UNGBOTHEM, RICHARDA L.\*A FEASIBLITY POPE A
MICROWAVE WATER VAPOR MEASUREMENT FROM A SPACE PROBE ALONG
AN OCCULTATION PATH-NO #\*PENNSYLVANIA STATE UNIVERSITY\*
APRIL 1975\*N75-29603\*THY OF USING A MM WAVE RADIOMETER TO
MICROWAVE WATER VAPOR CONTENT ALONG ITS LIZE THE WATER TO
MEASURE THE WATER VAPOR CONTENT ALONG ITS LIZE THE RESONANT H20 CROSS SECTIONS ARE PRESENTED, AND UPSINSTO —
MICROWAVE THE WATER VAPOR CONTENT ALONG ITS LIZE THE RESONANT H20 CROSS SECTIONS ARE PRESENTED, AND UPSINSTO —
MODEL THE ATMOSPHERIC WATER VAPOR CONTENT ALONG ITS LIZE THE WATER VAPOR COMPANDED TO PATH-S T 19 DEG C. THE O IS DISCUSSED.\*\* 5311318\*GOLDSMITH, IS DISCUSSED.\*\*

5311318\*GOLDSMITH, PAUL F.; PLAMBECK, RICHARD L.; AND CHIAD, RAYMOND L.\*MEASUREMENT OF ATMOSPHERIC ATTENUATION AT 1.3 AND 0.87 MM WITH AN HARMONIC MIXING RADIOMETER\*NO #\* IEEE MT-22, NO. 2, 1115-1116\*DEC 1974\*NO #\*THE ATMOSPHERIC ATTENUATION AT 1.3 AND 0.87 MM WAS MEASURED ABOVE M + THE MEASURED VALUE OF THE ZENITH ATTENUATION VARIED FROM 1 TO 5 DB AT 1.3 MM OVER THIS 5-DAY PERIOD AND WAS 2.5 DB AT 0.87 MM ON DEC 9, 1973. THE MEASURED VALUE OF THE ZENITH ATTENUATION VARIED FROM 1 TO 5 DB AT 1.3 MM OVER THIS 5-DAY PERIOD AND WAS 2.5 DB AT 0.87 MM ON DEC 9, 1973. THE TOTAL BEAMWIDTH OF THE FIGURATION WAS MEASURED TO BE 3' AT 1.3 MM.\*\*

B137618\*KONG, J.A., EDITOR\*THEORY OF PASSIVE REMOTE SENSING WITH MICROWAVES, FINAL REPORT\*CONTACT NO. 953524\*NO #\* JULY 1975\*N76-18629\*THIS IS A COLLECTION OF PAPERS ON #\* JULY 1975\*N76-18629\*THIS IS A COLLECTION OF PAPERS ON REMOTE SENSING OF THE EARTH BY MICROWAVES IN THE FRE-QUENCY RANGE 1.4-37 GHZ. KONG 'S ARTICLE TREATS THE FOLLOWING TOPICS: STRATIFIED MEDIA WITH NOTH TURE DISTRIBUTION, 2 LAYER RANDOMMEDIA WITH NON-UNIFORM TEMPERATURE DISTRIBUTION, AND STRATIFIED MEDIA WITH NON-UNIFORM TEMPERATURE DISTRIBUTION. REPORTS/THESIS

BY STUDENTS ARE IN APPENDIGES TO THIS MAIN REPORT. \*\*

5111713G\*\*HODGE\*\*, DR.; THIS MOPE AT TO THE STATE OF T

TION.\*\*

112181K\*AGANBEKYAN, K.A.; ZRAZHEVSKIY, A.YU.; AND MOLINHIN,
V.G.\*TEMPERATURE DEPENDENCE OF THE ABSORPTION OF RADIO
WAVES BY ATMOSPHERIC WATER VAPOR AT THE 10 CM-0.27 MM
WAVELENGTHS\*NO #\*RADIO ENGINEERING AND ELECTRONIC PHYSICS
20, NO. 11\*NOV 1975\*NO #\*THE ABSORPTION COEFFICIENTS
IN THE .398-13.5 MM WAVELENGTH REGION WATER VAPOR ARE
CALCULATED FOR CONSTANT AIR PRESSURE AND RELATIVE WATER
VAPOR CONCENTRATION FOR TEMPERATURES OF 173-373 DEG K.
FROM THE RESULTS OF THIS CALCULATION, THE TEMPERATURE
IN THE CM, MM AND SUB MM BANDS, AND CAN BE REPRESNIED IN
THE FORM GAMMA IS PROPORTIONAL TO T-N1. THE JEMPERATURE
IN THE CM, MM AND SUB MM BANDS, AND CAN BE REPRESNIED IN
THE FORM GAMMA IS PROPORTIONAL TO T-N1. THE JEMPERATURE
COEFFICIENT NI LIES WITHIN THE INTERVAL FROM 3.22 TO 4
IN THE TRANSMISSION WINDOWS, AND DECREASES WELL THE CALCULATION AGGREES WELL THE CALCULATION IN THE JEMPERATURE
ABSORPTION LINES. THE PRINCIPAL INACCURACY IN THE CALCULATION IS DUE TO THE INDETERMINING OF THE 1/2 WIDTH OF THE
ABSORPTION LINES, FOR RADIATION IN THE .398 MM TO 13.5 MM
ASSORPTION LINES, FOR RADIATION IN THE .398 MM TO 13.5 TION. \*\* PHYSICS,

LATTON IS DUE TO THE INDETERMINING OF THE 1/2 WIDTH OF THE ARSORPTION LINES, FOR RADIATION IN THE 13.98 MM TO 13.5 MM

ARSORPTION LINES, FOR RADIATION IN THE 13.98 MM TO 13.5 MM

6221714\*\*LEBE, HANS, FOR RADIATION IN THE 13.88 MICROWAY

OF AIR BETWEEN 40 AND 140 GHZ\*NO #\*IEEE TARANS MICROWAY

AD-A012 256\*RADIO WAVE PROPAGATION IN THE 40-140 GHZ BAND

THRU THE FIRST 100 KM OF THE CLEAR ATTENUATION AND

MOLECULAR PHOSOR 100 WAVE PROPAGATION IN THE 18 NWALER

YAPOR A UNIFIED TREATMENT OF MOLECULAR ATTENUATION AND

PHASE DISPERSION IS FORMULATED WHENTO FREQUENCY, PRESSURE

5321884 HARRIST, J.E.\*ATMOSPHERIC TRANSMISSION IN SEVERAL

AND TEMPERATURE DEPENDENCES.\*\*

SUBMILLIMETER WINDOWS\*NO #\*INFRARED PHYSICS. VOL. 116, 483-4851976\*\*

SUBMILLIMETER WINDOWS\*NO #\*INFRARED PHYSICS. VOL. 116, 483-4851976\*\*

SUBMILLIMETER WINDOWS\*NO #\*INFRARED PHYSICS. VOL. 116, 483-4851976\*\*

SUBMILLIMETER WINDOWS\*NO #\*INFRARED PHENDOMICAL AND ATMO
OF THE TRANSMISSION IN SEVERAL ASTRONOMICAL AND ATMO
SPHERIC EXPERIMENTS. THE TRANSMITT ANCE AT A WAVENUMBERNO PHENDENCY FREEDY ATTON OF THE WATER

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YAPOR CASES ARISING IN PRACTICION THE WATER

SAND THE ATMOSPHERE, IN A HEIGHT HIN THE WATER

1421218\*RIGHINI, G. AND SIMON, M.\*EVINCTION IN THE SUB
WILLIMETER ATMOSPHERE, IN A HEIGHT HIN THE WATER

1421218\*RIGHINI, G. AND SIMON, M.\*EVINCTION IN THE WATER

1421218\*RIGHINI, G. AND SIMON, M.\*EVINCTION THE EXTINCTION COEMOLOGY

MAY BE APPROXIMATED BY THE FUNCTION EXPECTIVE ABSORPTION, MODELLA APPROXIMATED AND THE EXTINCTION OF MODEL

B.A.; KLOKKO, V.V.; KHOKHLACHEZE, V.V A.G. THEORETICAL AND EXPERIMENTAL INV COMPLEX DIELECTRIC CONSTANT OF GROUND B33561N#RED•KIN, AND BABUSHKIN, GATIONS OF THE INVESTI- IN THE USW BAND (3 CM)\*NO #\*RADIO ENGINEERING AND ELECTRONIC PHYSICS VOL. 20, NO 1, 1111112\*JAN 1975\*NO #\*
THE INVESTIGATIONS CONDUCTED BY USINDICATED THAT THE
COMPLEX DIELECTRIC OF THE EMBOUND EXPERIENCES LARGE
CHANGES WITH HUMIDITY, TEMPERATURE AND SIGNAL FREQUENCY.
THE RESULTS HAVE AS SIMPLE EXPLANATION IF THE GROUND IS
REGARRED AS A COMPLEX DIELECTRIC THAT CONSISTS OF DRY
EARTH AND WATER THAT CONTAINS A MIXTURE OF DISSOLVED
SALTS. THE DIELECTRIC CONSTANT OF FREQUENCY AND THE
DIELECTRIC PROPERTIES OF WATER ARE DESCRIBED BY
ASSUMED AS BEING READ AND INTERPRIPED FOR THE THE TOP BY
ERLAXATION FORMULA, WITH A VECTOR SALTS. THE THE ADEBYCE
CONDUCT TYPE THE READING FOR AND THE READING OF THE FROM THE PROPERTY OF THE FROM THE

SPACE LINK OPERATING ABOVE 10 GHZ. RELATED MEASUREMEN PERFORMED AS A PART OF THIS EXPERIMENT INCLUDED THE DEMINATION OF THE CORRELATION BETWEEN RADIOMETRIC TEMPER TURE AND ATTENUATION ALONG THE EARTH-SPACE PROPAGATION RELATED MEASUREMENTS THE DETER-PERFORMEN AS APPART OF THIS EXPERIMENT INCLUDED THE DETERMINATION OF THE CORRELATION BETHEEN RADIOMETRIC TERPORA

TIME AND ATTENUATION ALONG THE EARTH-SPACE
PROPAGATION AND
PATH-3\*

622181C\*\*LIEBE, H. J. AND WELSH, W.M. \*MOLECULAR ATTENUATION AND
PHASE DISPERSION BETWEEN 40. AND 140 GETZ FOR PATH MODELS
FROM DIFFERENT ALTITUDES\*0.I. REPORT 73-10\*NO #\*MAY 1973\*
N.74-25886\*RADIO MAVE PROPAGATION IN THE 40-10\*NO #\*MAY 1973\*
N.74-25886\*RADIO MAVE PROPAGATION IN THE 40-10\*NO #\*MAY 1973\*
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11 NO \*\*\*MAY 1970\*\*N74-21804\*\*THIS IS A FINAL REPORT \*40 NO A 2-1/2
YEAR GRANT; THO LINES OF RESEARCH WERE PURSUES: 1)

MICROWAVE CONDUCTIVITY OF SLIGHTLY OF SLIGHTLY TO SAVE SURFACE OF THE NOTICE OF THE NOT BAND THROUGH GERMAN) \*

TERING FROM THE SEAS. MICROWAVE RADIOMETRY YEQUATIONS SAFETAL CLEAR TO THE SEAS. MICROWAVE RADIOMETRY YEQUATIONS SAFETAL CLEAR TO THE SEAS. MICROWAVE RADIOMETRY YEQUATIONS SAFETAL CLEAR TO THE SEAS THE

RADIATION, THE MAY BE AND STORE OF THE CONSENSATION OF THE STORE OF TH

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FINITE OVER THE ENTIRE DOMAIN OF ELEVATION ANGLE. AND ACCURATE OVER THE ENTIRE DOMAIN OF PRESSURE, THEMES OF EACH OF EACH OF EACH OF PRESSURE, THEMES OF EACH ATTENUATION STATISTICS IN THE ABSENCE OF DIRECT SATELLITE SIGNAL MEASUREMENTS.\*\*

C215417\*BERTOLINE, F; COTTANI, G. AND ROGAI, S\*COMPLEX DIELECTRON CONSTANT MEASUREMENTS IN THE FIELD OF MM WAVES (IN ITALIAN)\*NO \*\*FONDAZIONE UGO BARDONI\*MAY 24 1976\*N77-25376\*

THE COMPLEX DIELECTRIC CONSTANT OF A PLASTIC BICC WAS MEASURED FROM 40-50 GHZ IN A CIRCULAR CAVITY REFLECOMETER USING A BWV AS A POWER SOURCE. THE REASON FOR THIS WORK WAS TO PROVIDE A BASIS FOR DESIGN OF HIGHER (THAN 30 GHZ) FREQUENCY DIELECTRIC IN CAVITY MEASUREMENT HARDWARE.\*\*

C13181D\*THOMAS,J., M.C.; OTT, R.H.; AND VIOLETTE; E.J.\*

REPORT ON 1976 MM WAVE CONFERENCE\*NO \*\*OFFICE OF TELE-COMMUNICATIONS, U.S. DEPARTMENT OF COMMERCE, DENVER\*SEPT 1976\*PB-258 576\*TITLE AND SPEAKERS ONLY WERE GIVEN; USES OF

DISTORTION CORRECTIONS INTO CONSIDERATION.

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ANON-22 AND THE CORRECTION CALLED K6, 10S CALCULATED FOR COMPARED WITH CORRESON CALCED K6, 10S CALCULATED FOR COMPARED WITH COMPARED W

SYSTEMS EMPLOYING ORTHOGONAL TYPE THE PROPERTY OF THE ALTHONORY DISSEMBLY OF THE PROPERTY OF T

WAVE THEORY AND TECHNIQUES. VOL. MIT-25, NG. 6, 4844-488\*

JUNE 1977\*NO #\*\* THE RESULTS OF CALCULATION OF ANTENNA VIEWED

TEMPERATURE AT ZENITH, BOTH WITH AND HITHOUT THE SUNY THE SON OF ANTENNA VIEWED

AS A SOURCE, ARE GIVEN HORIZON AL PATH AND TOTAL ZENITH THESE

CALCULATIONS WAS MADE OVER THE FREQUENCY BOAD TO GAZ,

USING DATA FROM THE 24-WATER ABSORPHOR LINES BETWEEN 150ED,

WITH THE BARRETT AND CHUNG LINE WIDTH PARAMETER \*\*\*

14 ADIMER 87 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER SOVELET BRAND SECTRUM OF A DIMER 88 AND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A LINE SECTOR SECTRUM OF A DIMER 88 AS 39 \*\*MART NO \*\*\*SOVELET BRAND SECTRUM OF A LINE SECTOR SECTION OF A DIMER 88 AND SECTRUM OF A LINE SECTOR SECTION OF A DIMER 88 AND SECTRUM OF A LINE SECTOR SECTION OF A DIMER 88 AND SECTRUM OF A LINE SECTION OF A DIMER SECTION OF A SECTIO REAL SPEED.\*\*
2211818\*MINK, J
MENTS OF MILL
REPORT NO. 43 REAL SPEED.\*\*
11818\*MINK, J.W.\*RAIN-ATTENUATION AND SIDE-SCATTER MEASUREMENTS OF MILLIMETER WAVES OVER SHORT PATHS\*NO \*\*ECOM
REPORT NO. 4327\*JUNE 1975\*AD-A012 167\*RESULTS OF RAIN
ATTENUATION AND SIDE SCATTER MEASUREMENTS AT MM WAVELENGTHS
ARE PRESENTED THAT HAVE BEEN OBTAINED WITH A SHUTTLE PULSE
TECHNIQUE. THIS REQUIRES A PATH LENGTH THROUGH RAIN OF
ONLY A FEW METERS SO THAT RAINFALL RATE AND DROP SIZE DISTRIBUTION CAN BE CONSIDERED UNIFORM ALONG THIS PATH.\*\*

212182G\*DEIRMENDJIAN, D.\*FOR INFRARED AND SUBMILLIMETER
SCATTERING. II. ATTENUATION BY CLOUDS AND RAIN\*CONTRACT PART
F44620-C-0011\*NO #\*FEB 1975\*AD-A011 644\*IN THIS SECOND PART
OF OUR STUDY ON FAR IR AND SUB MM ATMOSPHERIC SCATTERING
EFFECTS, WE USE THE OPTICAL CONSTANTS SURVEYED IN THE FIRST
COEFFICIENTS OVER THE WAVELENGTH RANGE 12 UM TO 2.0 CM.
FOR THIS OVER THE WAVELENGTH RANGE 12 UM TO 2.0 CM.
FOR THIS PURPOSE, WE SET UP NEW ANALYTIC DROP SIZE DISAND
FOR THIS PURPOSE, WE SET UP NEW ANALYTIC DROP SIZE DISAND
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RAIN CORRESPONDING TO RAIN OF 10 AND 50 MM/HR. BY THE
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PROPAGATION. \*\*

B61481F\*\*ARONSON, J.R.; EMSHE, A.G.; AND SIRRONG, P.F.\*\*IHEORY OF ABSORPTION AND SCATTERING #Y LOSSY 19 TIELECTRIC PARTICLES \*\*
CONTRACT NO 3-44.022-121\*\*NO #\*\*JULY 19.75\*\*ED -2446 965\*\*HILLS
CONTRACT NO 10.40\*\*CD -40.00\*\*CD -40.00\*\*C SNOW. BUT LIMITED OCCURRENCE OF MAINTALL BOND.

PERIOD.\*\*

141151C\*LIN, B.J.\*ABSORPTION IN THE SUBMILLIMETER RANGE\*NSG74-60\*NO #\*DEC 15, 1965\*N66-16704\*WATER VAPOR ABSORPTION
IS THE MOST INTENSE ABSORPTION IN THE SUB MM REGION. WITH A
NEW SPECTROMETER, THE MICHELSON TYPE INTERFEROMETER, INVESTIGATIONS OF ABSORPTION CAN BE EXTENDED TO A LOWER FREQUENCY
RANGE WITH BETTER RESOLUTION AND ACCURACY. AN EXPERIMENTAL
SETUP IS DESCRIBED WHICH MEASURES THE WATER VAPOR ABSORPTION
FROM V = 10 CM-1 TO V = 200 CM-1 (.1 CM = 1 MM TO .05 MM)
AT A PATHLENGTH OF 200 FT AND PRESSURES OF 4.4 MM HG AND 1.1
MM HG. THEORIES OF THE WATER VAPOR ROTATIONAL LINE POSITIONS ARE REVIEWED. A NEWLY CONSTRICTED HIGH TEMPERATURE INVESTI -

SUB MM SOURCE IS ALSO DESCRIBED: \*\*

7231315\*CATOR, WILLIAM M. \*ABSORPTION AND EMISSION IN THE
8-MM REGION BY JOZONE IN THE YEAR ATMOSPHERE\*\*NONR - 222

OF SOLAR RASIATION AND THE MAY 1967\*AD 652-575\*THE ABSORPTION
OF SOLAR RASIATION AND THE WILLIAM OF THE ATMOSPHERE ABSORPTION
OF SOLAR RASIATION AND THE WILLIAM OF THE ATMOSPHERE ABSORPTION
OF SOLAR RASIATION AND THE WILLIAM OF THE ATMOSPHERE ABSORPTION
MAY. THE MEASURE AT 30.6, MAY 1967\*AD 67 THE ATMOSPHERE
LINES OF OZONE AT 30.6, MAY 1968.
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DEVELOPMENT OF A FREQUENCY SENTENCE WILLIAM OF THE ADDITION OF THE ATMOSPHERE ATMOSPHERE WILLIAM OF THE SOLUTION OF THE RADIATIVE THE CONTROL OF THE SOLUTION OF THE RADIATIVE THE SOLUTION OF THE RADIATIVE THE WILLIAM OF THE SOLUTION OF THE RADIATIVE THE WILLIAM OF THE WILL 812\* TION CURVE FOR THE RADIOMETER. THE BEST VALUE WAS
5.2 DEG K.\*\*
C317317\*STACEY, J.\*ELECTRONICS RESEARCH PROGRAM. RESEARCH AND
EXPERIMENTATION ON SPACE APPLICATIONS OF MILLIMETER WAVES:
REPORT NO. TDR-169(3250-41)-1\*CONTRACT NO.AF 04(695)-169\*
NO #\*21 MAY 1963\*AD-609 594\*THIS IS A PROGRESS REPORT IN
THE PLANNING AND DEVELOPMENT OF A 3.2 MM WAVELENGTH OBSERVATORY. A DESCRIPTION OF THE INSTRUMENTATION IS GIVEN AND
OBSERVATIONAL GOALS ARE OUTLINED.\*\*
511731D\*WULFSBERG, K.N.\*APPARENT SKY TEMPERATURES AT MILLIMETER WAVE FREQUENCIES: AFCRL-64-570\*NO #\*NO #\*JULY 1964\*
A\*605 813\*MEASUREMENTS OF APPARENT SKY TEMPERATURES TAKEN
OVER A ONE-YEAR PERIOD AT 15-17 AND 33 GHZ ARE SUMMARIZED.
SKY TEMPERATURE PROFILES FOR VARIOUS METEOROLOGICAL CON+
DITIONS ARE PRESENTED AS WELL AS CURVES SHOWING THE PER-

CENTAGE TIME DISTRIBUTION FOR VARIOUS ZENITH ANGLES. SUCFACTORS AS ABSORPTION AND RADIATION BY OXYGEN AND WATER VAPOR, EXTRAPOLATION OF THE DATA TO OTHER GEOGRAPHICAL AREAS, AND THE RELATION BETWEEN TOTAL ATTENUATION OF THE ATMOSPHERE AND SKY TEMPERATURE ARE DISCUSSED. A DESCRIPTION OF THE RADIOMETERS AND THE CALIBRATION TECHNIQUES ARE DISCUSSED. SUCH

TION OF THE RADIOMETERS AND THE CALIBRATION TECHNIQUES ARE INCLUDED.\*\*

6216810\*SNAY, R.J.\*MICROWAVE PORTION OF THE OXYGEN LINES REFRACTOMETER\*CONTRACT NO. AF 19-6285-165\*ESD+TR-66-65\*JUNE 1966\*AD-635 048\*A MICROWAVE SUBSYSTEM WAS INSTALLED IN THE MITRE CORP'S REFRACTOMETER VANS AS AN INTEGRAL PART OF THE OXYGEN LINES REFRACTOMETER. IN OPERATION, TWO COHERENT FREQUENCIES, 45 AND 90 GHZ, ARE TRANSMITTED OVER A 23 KM PATH, AND THE CHANGE IN DIFFERENTIAL PHASE SHIFT IS MEA-SURED AT THE RECEIVER. THIS CHANGE IS AN INDUCTION OF THE REFRACTIVE QUALITIES OF THE ACHIONSPHERE OVER THE PATH. THIE EQUIPMENT WAS TESTED AT A FIELD SITE ON THE LAKE WINNEPETIONS FOR IMPROVING SYSTEM SENSITIVITY AND STABILITY ARE GIVEN.\*\*

TIONS FOR IMPROVING SYSTEM SENSITIVITY AND STABILITY ARE GIVEN.\*\*

5215817\*LONG, M.W.\*SUBMILLIMETER WAVES AND ASTROPHYSICS AT OUEEN MARY COLLEGE\*NO #\*ORNL-20-66\*JUNE 1966\*AD-485 456\*
THIS REPORT IS ON THE RESEARCH CAPABILITIES OF QUEEN MARY COLLEGE, A SCHOOL OF THE UNIVERSITIES OF LONDON IN THE AREA OF SUB MM RESEARCH. THEY DISCUSS THE KINDS OF SUB MM RESEARCH GOING ON (CA 1965) AND THE INSTRUMENTATION BEING USED.\*\*

5311818\*HOFFMAN, L.A. AND WINTROUB, M.J.\*PROPAGATION FACTORS AT 3.2 MILLIMETERS\*CONTRACT NO. AF 04(695)-469\*NO #\*

TRIBUTE FROM 1 TO OVER 100 DEG K TO THE APPARENT SKY TEMPERATURE. SCATTERING FROM CLOUD DROPLETS IS OF NEGLIGIBLE
IMPORTANCE OVER THE FREQUENCY RANGE CONSIDERED. A CLOUD
DROPLET SIZE DISTRIBUTION OF THE FORM AR(SIXTH POWER)EXP
(-BR) IS USED IN THE CALCULATIONS, THE DROPLET RADIUS IS
CRITICAL BECAUSE OF THE R(CUBE) AND R(SIXTH POWER) VARIATION RESPECTIVE IN THE ABSORPTION AND SCATTERING CROSS
SECTIONS.\*\* THE INTERESPONDED TO SERVICE STATE OF THE PROPERTY OF THE PROPERTY OF THE RESIDENCE OF THE 227-234\*1972\*NO #\*THIS IS A GENERAL, THEORETICAL DISCUSSIO ON A NEW LOOK AT RELAXATION PROCESSES, WHICH EXIST IN MATERIAL MEDIA AS ACOUSTIC, ELASTIC, DIELECTRIC, MAG-NETOACOUSTIC ETC. PHENOMENA. ALL OF THESE ARE "EFFECTS" WHICH OCCUR AS A RESULT OF AN EXTERNAL FIELD ON A MEDIA, WHETHER IT IS A STRAIN, ELECTRIC, MAGNETIC...ETC. THESE EFFECTS "FOLLOW" THE CAUSES IN THE CONSTITUTIVE EQUATIONS; FOR EXAMPLE, IN THE CASE OF A DIELECTRIC THE DISPLACEMENT D(W) = E(IW)E(W), WITH E(IW) THE COMPLEX DIELECTRIC "CONSTANT" AND E(W) THE CAUSATIVE FIELD.\*\* THEORETICAL DISCUSSION

C417A27\*GALLAGHER, J.J.; STRAUCH, R.G.; CUPP, R.E.\*EXCITATION AND DETECTION TECHNIQUES FOR MM WAVES\*OR3821\*MARCH 1964 \*AD434001\*THE OBJECT OF THIS CONTRACT IS TO INVESTIGATE THE EXCITATION AND DETECTION TECHNIQUES FOR MOLECULAR MM WAVE TRANSITIONS WHICH CAN BE USED TO DEVELOP A FREQUENCY STANDARD OPERATING IN THE REGION OF 1 MM. DURING THE PAST QUARTER, H2S ELECTRIC RESONANCE HAS BEEN OBSERVED\*\*

OPERATING IN THE REGION OF 1 MM. DURING THE PAST QUARTER,
H2S ELECTRIC RESONANCE HAS BEEN OBSERVED\*\*

D217A1C\*NO NAME\*MM WAVE AMP^IFICATION BY RESONANCE
SATURATION IN GASES\*CONTRACT NO. AF 30(602)2744\*RADC\*TDR\*
G3-562\*MAR 1964\*AD-434 764\*THE POWER STURATED RESONANCE
ABSORPTION OF A GAS (HCN) HAS BEEN OBSERVED\*\*
A GAIN OF 20 DB WAS OBTAINED WITH A GAIN OF BUTTON OBSERVED\*\*
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BAND IN SEA 9 (1076) AND FRESH WATER TIGE AND SNOWS NO # #18 40 0 MF IZI-
BOYO-601 TEST OF THE ATTENUATION OF RADIO WAYES IN THE 30 0 MF IZI-
BOYO-601 TEST OF THE ATTENUATION OF RADIO WAYES AND WAYES THE STATE OF T
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KURPNOV, A.F.; AND SHAPIN, S.M. SUBMILLIMETERS WAVE SPECTRUM AND MOLECULAR CONSTANTS 105 148819 Beans ## WAVE SPECTRUM WAVE SPECTRUM SPECTRUM CONSTANTS 105 148819 Beans ## WAVE SPECTRUM WAVE SPECTRUM S

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ZATION MEASUREMENTS. \*\*
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CONSTANTS OF METAL OXIDES IN THE 859-861-8ARRIL 1976-8008 #\*
APPLS ART ICLES; METAL OXIDES IN 144.859-861-8ARRIL 1976-8008 #\*
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HEAD OPPICS, PORTS ON THE 600 X11 E. NO CRYSTALLINE
FOR LUCALOX, SINTERED OXIDES, IN THE 600 X11 E. 100 X11

MANIUM ARE SUGGESTED FOR USE AS FAR IR MEASUREMENTS, FOR HAVENUMBERS MITS OF STREET OF

AND

AND REFLECTION MEASUREMENTS ARE TABULATED FOR VARIOUS SNOW DENSITIES COVERING THE RANGE 32-39 GHZ. RESULTS SHOW THAT ...

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APPACKED SNOW AND SNOW ENABLED SNOW AND SNOW

SYNCHRONOUS COMMUNICATION SATELLITE, IN THE 15-35 GHZ

BAND.\*\*

212173A\*SMITH, IRA, EDITOR\*FINAL REPORT, VOLUME II, FOR MM
COMMUNICATION PROPAGATION PROGRAM (1 NOV 1964 - 1 NOV 1965)\*CONTRACT NO. NASS-9523\*NASA CR-76095\*NOV 1964\*N66-30164\*THIS DOCUMENT IS VOLUME II OF THE FINAL REPORT FOR THE MM COMMUNICATION PROGRAM BEING PERFORMED TO STUDY THE REQUIREMENTS FOR THE DESIGN OF EXPERIMENTS TO DETERMINE THE EFFECTS OF THE PROPAGATION MEDIUM ON MM SPACE-EARTH PATHS, FOR BOTH LOW ALTITUDES (200 NM) MEDIUM ALTITUDE (6000 NM) AND SYNCHRONOUS ALTITUDE (22,300 NM) SATELLITES.\*\*

5611211\*FAZIO, G.\*A 102-CM BALLOON-BORNE TELESCOPE FOR FAR IR ASTRONOMY\*NO #\*OPTICAL ENGINEERING, VOL. 16, NO. 6, 551-557(NGR22-007-270\*NOV-DEC 1977\*NO #\*THE CENTER FOR ASTROPHYSICS - UNIVERSITY OF ARIZONA. BALLOON-BORNE INSTRUCTION OF THE PROPAGATION MAPPING OF FAR IR ASTROPHYSICS - UNIVERSITY OF ARIZONA. BALLOON-BORNE FORM PHOTOMETRY AND HIGH RESOLUTION MAPPING OF FAR IR AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED A TOTAL OF 10 NOW BEEN FLOWN AND SUCCESSFULLY RECOVERED AND SUCCESSFULLY RECOVERED AND SUCCESSFULLY RECOVERED AND

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FRACTIVE INDEX, PARTICLE SIZE DISTRIBUTIONS, HUMIDITY
EFFECTS - DATA TO 32 UM, LOW SPECTRAL RESOLUTION PROPAGA1100 (RUMTRAN), AND GLASER TRANSMISSION RESOLUTION RESOLUTION

53811 \* VOGEL , WOLFHARD \* SCATTERING INTENSITY PLOTS AND TRANS MISSION COEFFICIENTS FOR MM WAVE PROPAGATION THROUGH RAIN \* CONTRACT NO. F33615-71-C-1203 AFAL-TR-71-345 \* DEC 1971 \* AD-890 408L \* THIS REPORT PRESENTS THE RESULTS OF COMPUTER

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PATH LOSS WAS 70 DB MORE THAN IS REQUIRED TO HAVE A READABLE SIGNAL . CONCLUSION: 1) REPORT A HOAX OR 2) CONDITIONS

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SOL STRUCTURE AND THE OPTICAL PROPERTIES ARE POINTED OUT.
CONCLUSIONS ARE PRESENTED ON THE POSSIBLITY OF INVESTIGATING THE AROSOL STRUCTURES BY MEANS OF EXPERIMENTAL EXTINCTION OF BACKSTATIC PROPERTIES ARE POINTED ON THE POSSIBLITY OF INVESTIGATION AND INTERPRETATION OF BACKSTATIC PROPERTIES ARE POINTED ON THE POSSIBLITY OF INVESTIGATION AND INTERPRETATION OF BACKSTATIC PROPERTIES ARE POSSIBLITY OF SAME AND THE POSSIBLITY

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C361B1B\*WERNER, B; BELANGER, B.; DOMIZIO, R.D.; AND SMITH, P. MILLIMETER SEMIACTIVE GUIDANCE SYSTEM\*NO #\*NOV 1976\*AD-B017

829L\*THE CONCEPT INVOLVES THE USE OF A MM ILLUMINATING A MOUNTED ON AN RPV AIRCRAFT ON THE GROUND, ILLUMINATING A GROUND VEHICLE SEEKER TARGET, AND A SEEKER MOUNTED IN A PROJECTILE OR SIMILAR WEAPON AND GUIDING THE WEAPON TO THE ILLUMINATED TARGET. TRADEOFF STUDIES WERE CONDUCTED TO DETERMINE THE OPTIMUM ILLUMINATOR WAVEFORM AND OPTIMUM SEEKER DESIGN. ANALYSIS OF DETECTION CAPABILITIES AND TRACKING ACCURACY WERE PERFORMED FOR BOTH CLEAR WEATHER AND ADVERSE WEATHER CONDITIONS.\*\*

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